

HR 2452

-0032 ± 9.0
-0044
-034

47703 6 38.3 + 35 59 6.3 F5 + 8638

8724 A

F8H 65.00

4337

16.286 1909.0 + 85 58 50.08 1505.5

$$\frac{13}{417}$$

~~0040~~ -029 →

-048 -029

$$\frac{1.10}{5.118}$$

$$\begin{array}{r} 35.42 \\ 40 \overline{) 788} \\ \underline{76} \phant{4} \\ 28 \phant{8} \\ \underline{28} \phant{0} \\ 8 \phant{0} \\ \underline{8} \phant{0} \\ 0 \phant{0} \end{array}$$

$$\begin{array}{r} 12.13 \ 1924.5 \\ 19.68 \phant{0} \\ \underline{5} \phant{2.62} \phant{6} \\ -2 \phant{31} \\ \hline 50 \phant{39} \\ \underline{50} \phant{15} \\ 18.2 \phant{0} \end{array}$$

$$\begin{array}{r} 545 \\ 27.2 \\ \hline 21.4 \end{array}$$

$$\begin{array}{r} 13 \phant{1} \\ 40 \overline{) 401} \\ \underline{40} \phant{0} \\ 1 \phant{0} \\ \underline{1} \phant{0} \\ 0 \phant{0} \end{array}$$

$$\begin{array}{r} 50.10 \ 1930.0 \\ \underline{50} \phant{15} \\ 18.2 \phant{0} \end{array}$$

$$\begin{array}{r} 16.38 \\ 37 \\ \hline 41 \end{array}$$

$$\begin{array}{r} 50.42 \\ \underline{50} \phant{15} \\ 18.2 \phant{0} \end{array}$$

30pp.

30 pm.

-048-029

186.3

-205	-108	972	+0473	+0148	+0621 ¹⁵⁶³	+1.9	+83.9	+85.8
-409	90	013	+0931	-1251	-0330 ⁶⁰	-4.0	+1.1	0.6
876	358	234	-2016	-0547	-2563 ⁷⁶⁹	-7.7	+20.2	+12.5

55 Ann

6 39.4 44 34

-73.16

47914

5.02 + 1.48 + 1.83 + 1.51 + 1.2

-75.86 (3)

GC875-1

47.1

-69.30 (4)

W4353

3.2

→ 7.30

Y1561

47.6

F41401518

948

12 52

1722.8

1516

-041 -03260

18040

5039

64

-56 -20 -55 .087

-218 -244 944

-407 902 -144

887 352257

+0424 +0379

+0790 -1370

-1720 -0535

+0801 +6.4

-0580

-2255

69.0

+10.3

-21.7

18.1 15.6 A(28)

79

+4.6

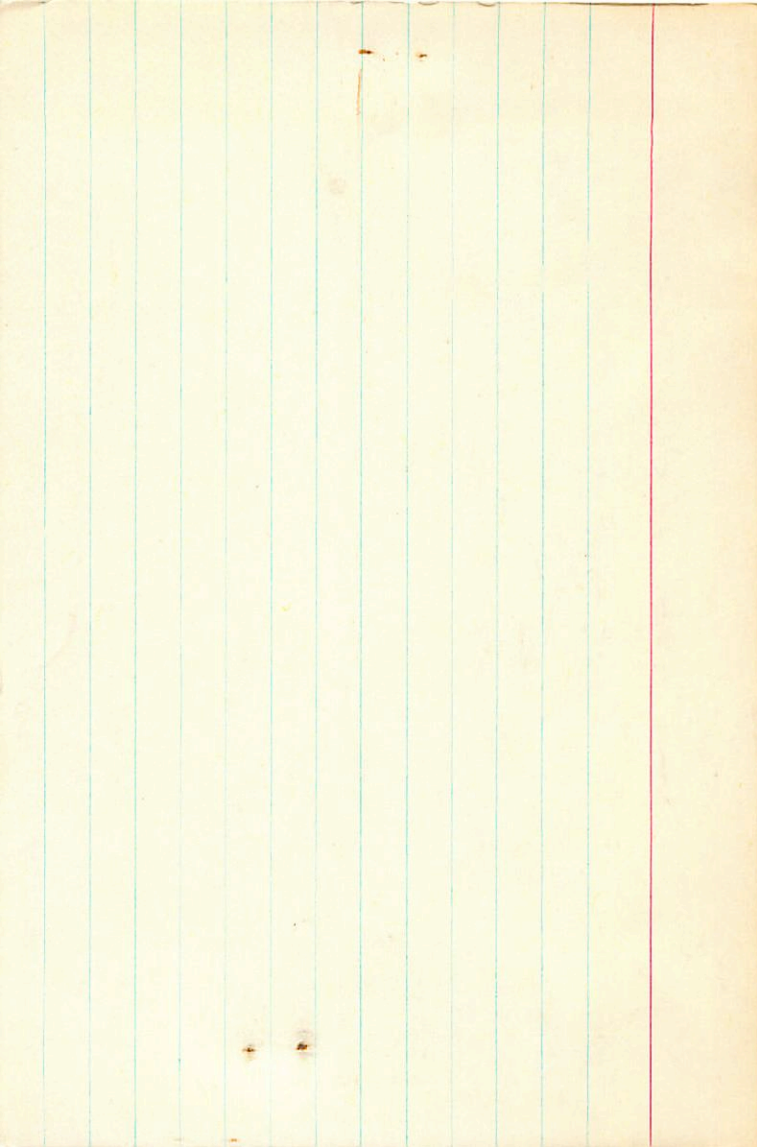
-18.1

15.6

-62.6

-14.9

-398



HR244

6 39.8 + 37 12 6.11 120

48073

+039-045 62

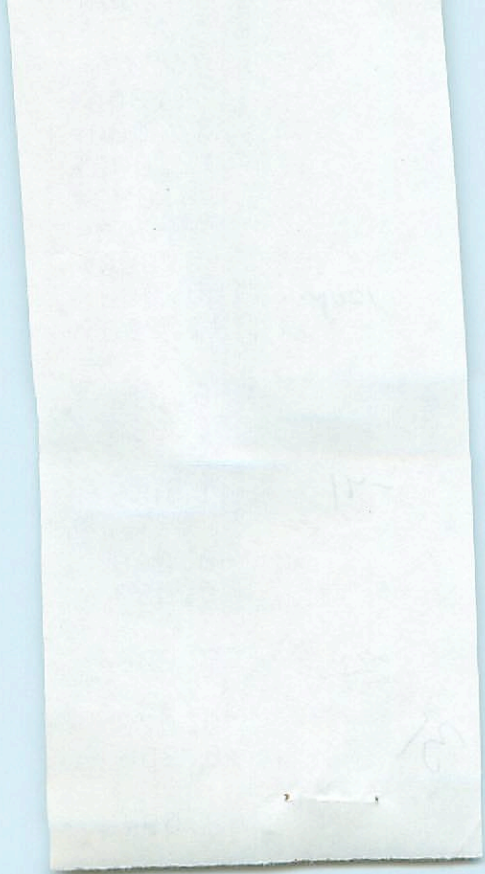
1
0

- 4/2

+038

...

31



10.000*

6.000*
39.800*
37.000*
12.000*
0.038*
-0.045*
5.000*

120p.

100.000
-41.200

-0.012
0.968

-41

-41.059

-0.268
0.029

-22

-28.006

31

0.077
0.250

~~11.41~~

-2.594

48381 6 39.9 -33 25 NOIB +34.5-46

FD 883

133/1276

8.48 +1.05 (2.08)

+40.20

$-0.27 + 0.20$ CP \rightarrow

6.650
-33.400
-32.000
20.000
6.000
158
39.500

-0.214
0.871
0.442
109.641
34.854

-0.409
0.331
-0.850
83.249
-20.384

0.887
0.363
-0.286
-77.916
-23.633

32

HP2413 . 6 40.2 153 21 6.23 100

+055 -181 GL

- 1 0

+18586

+054

33

2471 HR 6 40.6 -22 24 6.22 +36

+43.5 (3)

6.22 202 160 672 2.717 4.1

B 837 403 214 303 255 (

-088 1076

|

4

34

8.650
-22.400
-92.000
76.000
4.100
66
0.000

-0.214
0.771
0.601
363.778
24.035

-0.409
0.000
0.771
600.000
22.500

0.000
0.000
0.000
0.000
0.000
0.000

34

61
284

6 40.9 5.04 9

2423

2789 11.504 6876

8884

102

136

284

358

4884

252

0414

7414

5

74404 04.2

260

AND K11N-040

H-810 HISSON

00032

1410

2334 414

459a

~~1100~~

~~4000~~

~~2400~~

~~2510~~

2410

-6002-0111 W₀50

-60014-0156

110-0114

-6100

910-0110

1881

202

1411

488

694

(28)

4pm
M₀ = M₀ 0000

8.35

-6045

20016
-18

35



2473.000*

6.000*

40.960*

25.000*

12.000*

-0.001*

-0.014*

7.000*

8.1

421

251.109

9.900

-0.004

0.972

48

0.607

-0.058

-0.163

-25

-16.129

35

-0.033

0.168

-12

-6.561

12 Lys

1482470

6 41.8 +59 30 -40

9.5 "

down 12 in 5.0.16.22"

-021-00466

||

983-152-862 508-021-004-4-003-3.5-095
020003004001050 033-2.0+0.4-2.0

49.4+1.1-13.0

13 days

48432 6 42.6 +57 13 5.5966 +19.0a

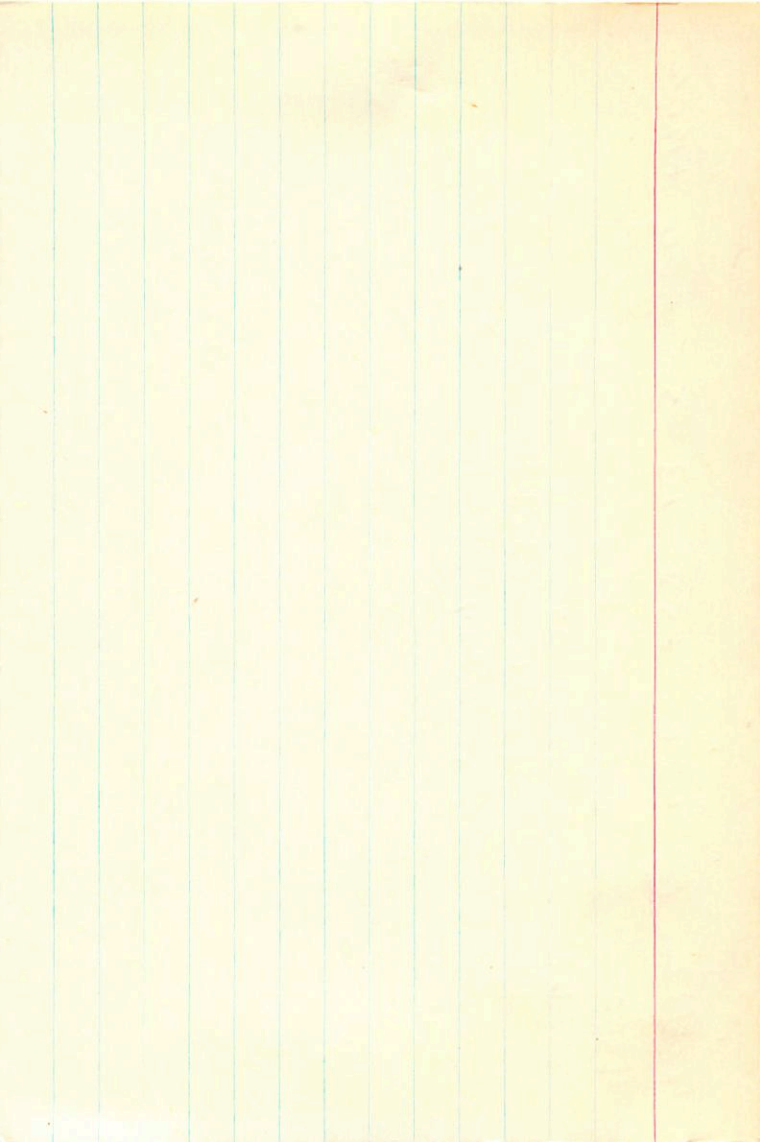
4390

8826

25

+0026 -038N30

+0026 ±2.4-041 ±1.866 → N30



452676 6m=02 6 44.0 +55 46 dP6-d15

HR240H
0208070

11.5
14.5
+5.5

107

2nd
2nd

.314 .167 .432 20 506 2.640PC+

318

[M1] 223 +10

[C1] 369 +28
+34
+38

-236	-026	872	-067	+2110	+1434
-355	462	317	-1123	-4249	-5372
598	270	373	2525	-1331	+1154

+8.1
+2.9
+3.8

36

+9.3
" "
" "
+100-104

RAD. VEL. : 0.000
 MODULUS : 31
 DISTANCE : 2.450
 PM. DEC. : -102.000
 PM. R.A. : 107.000
 DEC. : 55.750
 R.A. : 4.750

U : 4.263
 Ub : 137.235
 d3 (U) : 0.874
 d2 (U) : -0.422
 d1 (U) : -0.236

V : -16.321
 Vb : -500.484
 d3 (V) : 0.813
 d2 (V) : 0.864
 d1 (V) : -0.395

W : 3.782
 Wb : 121.265
 d3 (W) : 0.372
 d2 (W) : 0.272
 d1 (W) : 0.888

10
 10

R.A. : 6.750
DEC. : 55.750
PM. R.A. : 107.000
PM. DEC. : -102.000
DISTANCE : 2.450
MODULUS : 31
RAD. VEL. : 0.000

q1 (U) : -0.236
q2 (U) : -0.425
q3 (U) : 0.874
dU : 137.935
U : 4.263

q1 (V) : -0.395
q2 (V) : 0.864
q3 (V) : 0.313
dV : -530.404
V : -16.391

q1 (W) : 0.888
q2 (W) : 0.272
q3 (W) : 0.372
dW : 121.965
W : 3.769

30

49048 6 43.7 -0019±5.4 -018±4.9
-0013 -14 45 -008
51.3 42 -18.88

4401

8852 42.557 19163 -14 44 30.37 1944

064

+64

43.021

29.73

34.773

56.47

5.198

-32.58

42.972

996

29.05

+23

-025

-1.22

998

19.3

30.27

973

29.91

+44

42.594

29.18

29.81

43.002

1686

30.22

42.946

35.6

+32

42.946

1535.24

29.90

42.946

1686

29.98

42.946

35.6

30.03

42.946

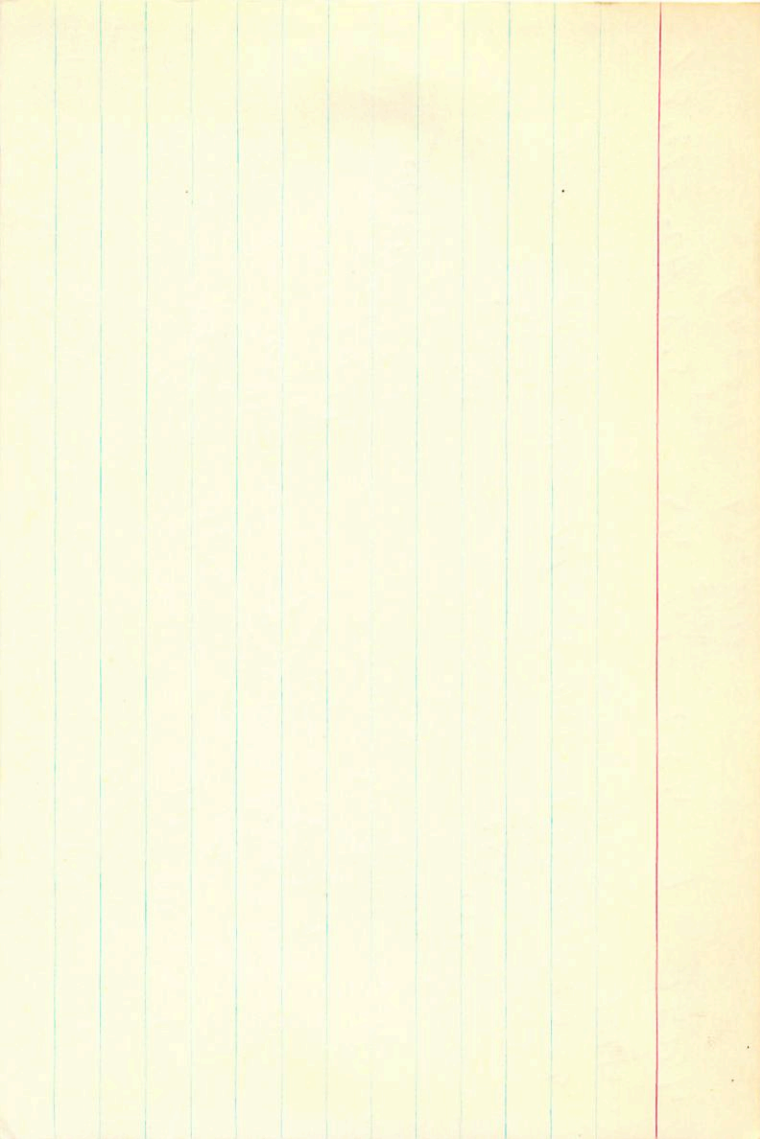
21.2

1533.07

42.946

21.2

30.03



50

6 43.7

+58

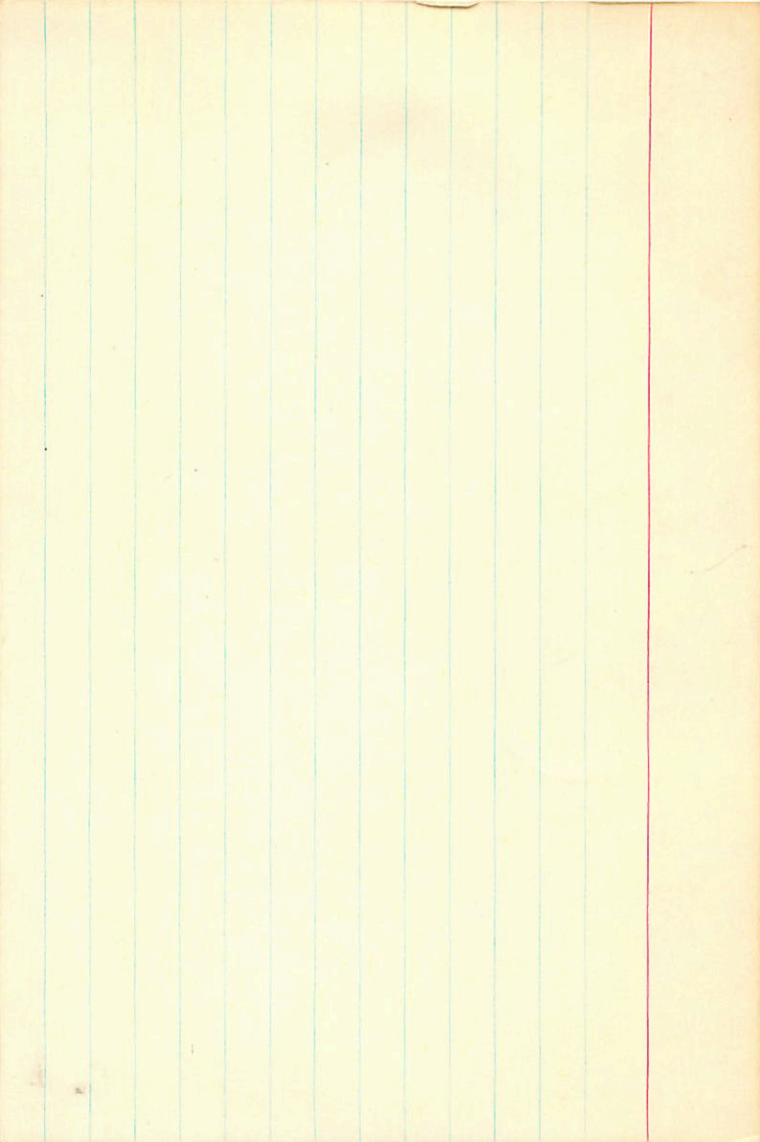
41

3W

+189C

W 4400

10.0



W 443

6 44.3 +37 36

WA +80d Md(2)

Hr 3

DA

W1579

12.03 -0.06 -0.90

+64
194

P_c +85 616pp

π_g 0.068

62M(8)
547k(10)
39u(8)
650(7)
059±5

-0.15 -0.93

-0.21 -0.91

-214±3 -932±5V

$\theta_0 = 190$

$\mu = 0.95'$

$\theta_c = 187$

981 -132 610 792 -0.21 -0.91 +75 -355 +52 -3.416
206 524 040 607 .474 2.767 +67 -13 +66

-6 +107 +2 068

[+94 -50 -11]

HR 2449

ADG 5447

44059

-0018 -0482 ZL

+0021 -0470

+0005 -0451

+0071

+0075

6 44.5 +18 15-

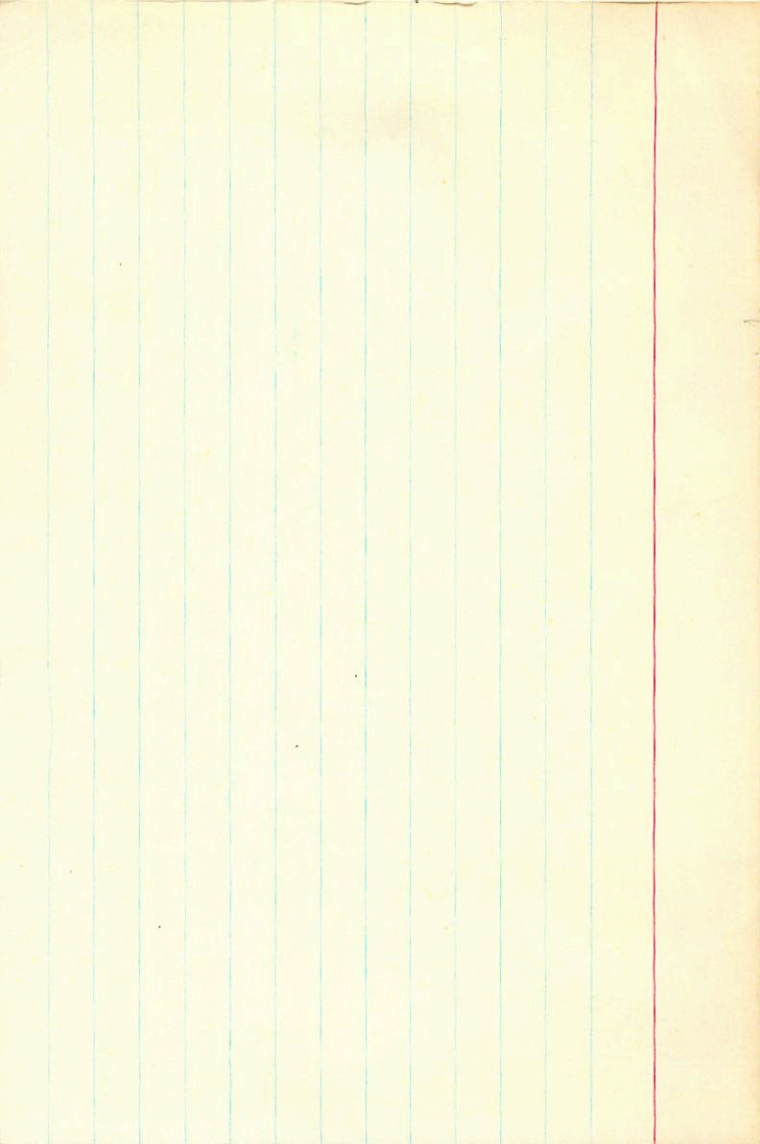
+1216 ⓑ

.0092

000 -044 +1

+116 +42

+16 ⓐ



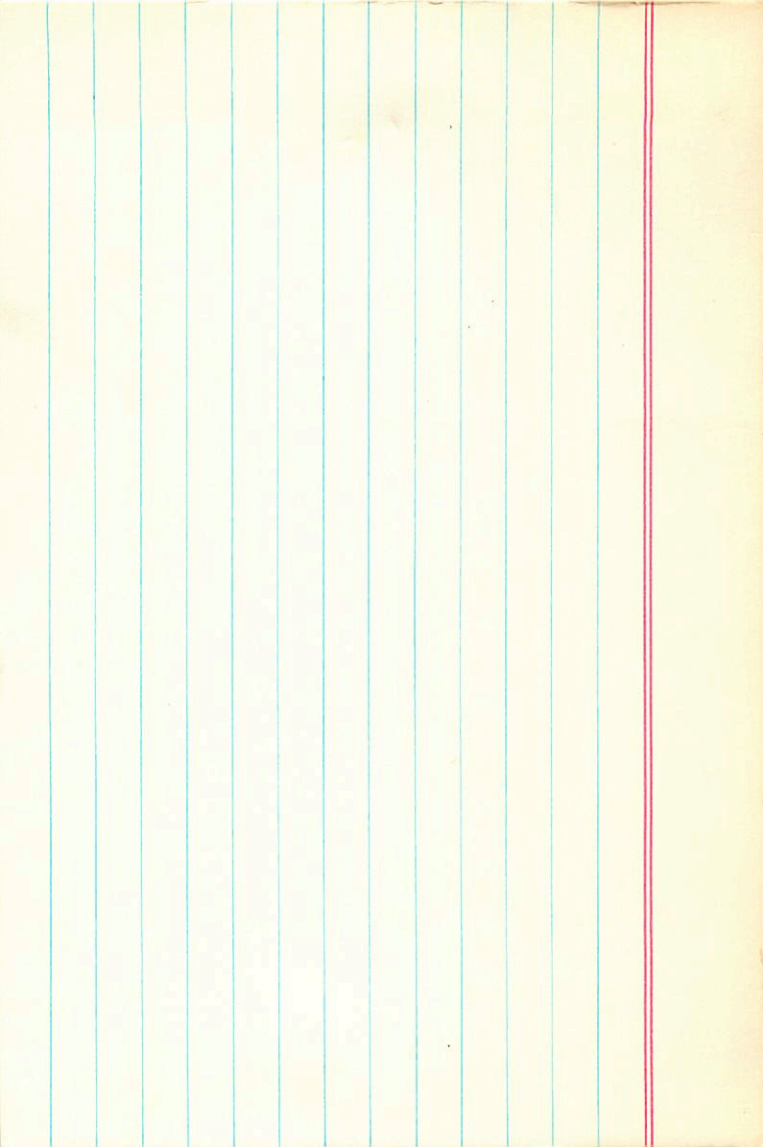
49614 6 45.4 -47 45 -9.8.56

FD 1148

6.94 + 1.40 (2.46) N3 III

6.9 } 26"
11.0 }

+0.0002 +0.013 N30
-0.0004 +0.001 GC →
-0.0001 +0.007



2514 -12.5 to 14.1 36 round
6.45.7

-1 16 -142 (3)
5.71 +4

49437 (32617)

46.921 8.4 -0028 347 -041 54.4
-0026 -040 42.23 9.8

1.1386 ~~27.44~~

116
42.047
-0027
-0024
-035 1.65
-039

66.8903

40.58

46.944 40.29 42.07
+17
961
+29
46.78

72620 4920 } 0546
-0117
-2.9
0190

46.878 65.43 42.59 -0026 -0089
+17
855
-11
42.70
-00081 -0397

-11.6 3.40 70.56

27.74 34.38 46.970
24.95 0.17
+28
844

-0421
-040 -039
42.93
0

531

5.75

177

174

716

2.948

(232)

214

(68)

641

2.62
24

(+2.33)

186

49435 6 45.8 -01 46 7.4 g/k⁵ +71.37

-701387

125 π +75.8 256.

4430 7.60 +1.48 +1.35 1.05

-0011 +0.24 Capes 25

$$\begin{array}{r} -012 +0037 \\ -3 +2 \\ \hline -015 +005 \\ -016 +024 \end{array}$$

R. 6.66 ①

8.25 pr. / 100 pr

$$\begin{array}{r} -015 +0057 \rightarrow GL \\ -016 +024 \rightarrow \end{array}$$

+91.8 +.7

$$\begin{array}{r} -0155 +015 \\ -0192 +014 \end{array}$$

+8.5 +11 ms

7.59 +1.51 +1.82 ③
6.74 +0.64 ②

-017 +014

-6.7 -1

6.48 55
593

636
5.5
7.9
④

12401357

37



49435.000*

6.000*

45.800*

-1.000*

-46.000*

-17

114

8.4

49435.000*

6.000*

45.800*

-1.000*

-46.000*

-0.017*

478.400*

73.600

0.05

0.000*

-0.500*

12.547

-0.015

-0.027

-9.156

3

$$\begin{array}{r}
 42176 \quad 2907 \quad 5438 \\
 + 40 \\
 \hline
 216 \\
 \hline
 -1 \\
 \hline
 .37
 \end{array}$$

$$\begin{array}{r}
 42169 \\
 \hline
 197 \\
 \hline
 42158 \\
 \hline
 187 \\
 \hline
 4438 \\
 \hline
 -14 \\
 \hline
 4424
 \end{array}$$

$$\begin{array}{r}
 42169 \\
 \hline
 197 \\
 \hline
 42158 \\
 \hline
 187 \\
 \hline
 4438 \\
 \hline
 -14 \\
 \hline
 4424
 \end{array}$$

$$\begin{array}{r}
 42169 \\
 \hline
 197 \\
 \hline
 42158 \\
 \hline
 187 \\
 \hline
 4438 \\
 \hline
 -14 \\
 \hline
 4424
 \end{array}$$

$$\begin{array}{r}
 42169 \\
 \hline
 197 \\
 \hline
 42158 \\
 \hline
 187 \\
 \hline
 4438 \\
 \hline
 -14 \\
 \hline
 4424
 \end{array}$$

$$\begin{array}{r}
 -1008 \\
 -1002 \\
 \hline
 -2010
 \end{array}$$

845

HR2512

6 46.4 + 32 39 5719104

039-0436C

1

040

-140

38



2512.000*

6.000*

46.400*

32.000*

10.000*

GRV 574 -02758.1

RX Year

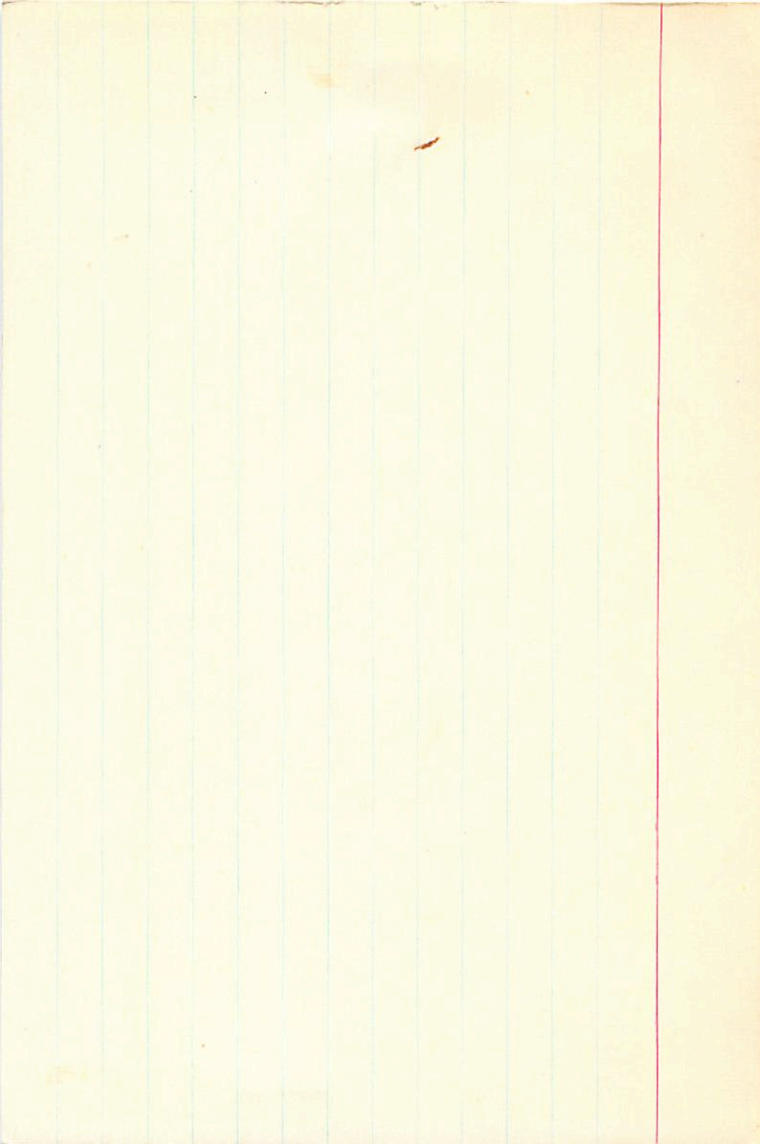
6 46.9 +33 18 8.6 A2 +33.58

4521

+19 Audit

4439

48. 55.03 | 1516.7 +33 17 51.10 1516.6



6 468 +60 22 -636 5499a

-63.6 ⑤

7000 024.00 +165 +108

335

34

5

-636



39

RAD. VEL. : -93.900
 MODULUS : 100
 DISTANCE : 5.000
 PM. DEC. : 38.000
 PM. R.A. : 335.000
 DEC. : 48.400
 R.A. : 2.800

p1 (U) : -0.247
 p2 (U) : -0.491
 p3 (U) : 0.832
 p4 : -282.214
 U : -81.342

p1 (V) : -0.388
 p2 (V) : 0.848
 p3 (V) : 0.379
 p4 : -123.303
 U : -32.420

p1 (W) : 0.888
 p2 (W) : 0.231
 p3 (W) : 0.398
 p4 : 237.882
 W : 48.481

R.A. : 6.800
DEC. : 60.400
PM. R.A. : 335.000
PM. DEC. : 38.000
DISTANCE : 5.000
MODULUS : 100
RAD. VEL. : -63.600

q1 (U) : -0.247
q2 (U) : -0.491
q3 (U) : 0.835
dU : -282.214
U : -81.342

q1 (V) : -0.388
q2 (V) : 0.840
q3 (V) : 0.379
dV : -153.303
V : -39.450

q1 (W) : 0.888
q2 (W) : 0.231
q3 (W) : 0.398
dW : 737.885
W : 48.461

39

33 Rev
49606

6 47.0 +16 16 5.7 B9 +12.86

4440

5.69-14-53 B8 14

8927

34

4030

-0014 -009 N30

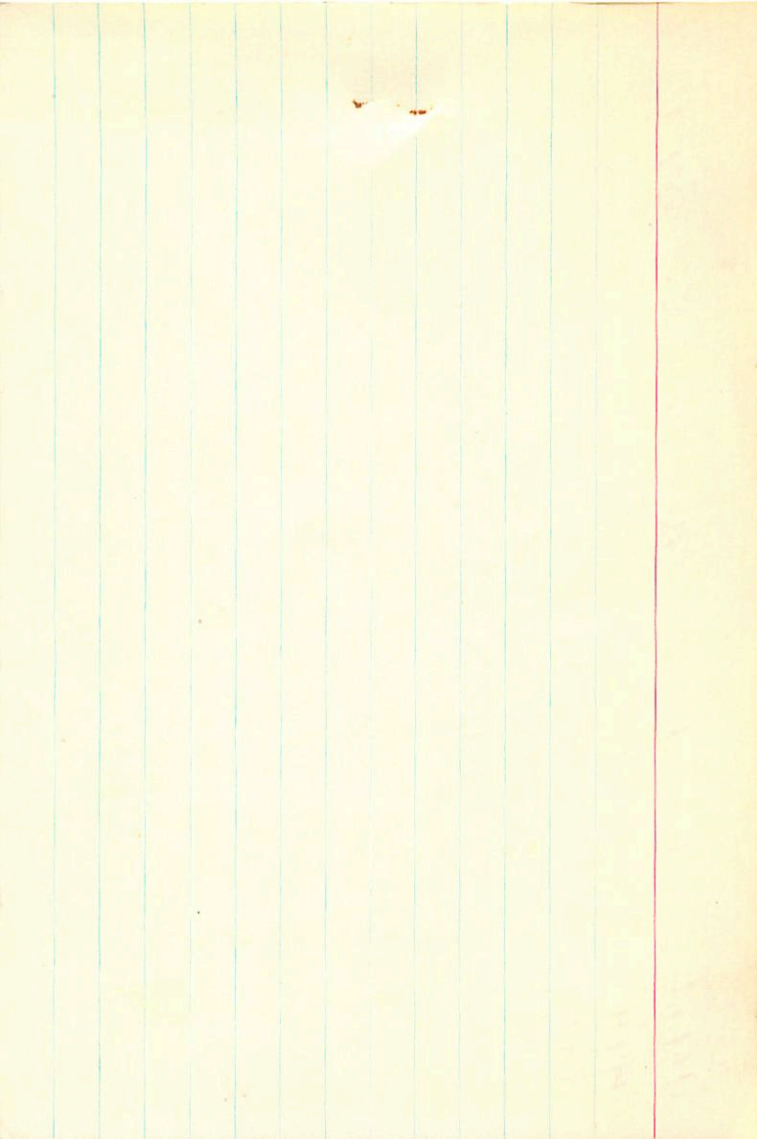
-0013 ± 2.3 -013 ± 2.0 Bc → N30

-00135 -010

-0195

-019

016.7 0120



10

40

45976 / 6 48.3 -7 59 6.24 top

018955

HR2534

-0005 ± 7.8 000 ± 7.1

-0008 -009

+22.4 / detour

17.828 18958 -7 8-8 53.22 18949

$\frac{0.22}{850}$

$\begin{array}{r} -6 \\ -9 \\ -8 \\ \hline \end{array}$ $\begin{array}{r} -1.6 \rightarrow 1000 \\ -10 \text{ mm} \\ -6 \end{array}$

9.74 1935.63

5.574

42.25

12.2528

$\frac{51.99}{1.28}$

38.6

$\frac{17.828}{838}$

$\frac{817}{817}$

$\frac{53.27}{1.33}$

$\frac{52.85}{1.32}$

34.7

000

$\frac{0.3}{0.3}$

$\frac{52.9}{1.34}$

$\frac{52.85}{1.32}$

39.5

17.828 - 0.3

1933.07

$\frac{16}{79}$

$\frac{53.00}{1.35}$

52.75

-054	-622	+781	+0030	+0560	+0550	+15.9	+12.5	1024
+499	+661	-54	+0274	-0555	-0321	-3.2	-12.6	551
+465	+420	-274	-0476	-0328	-0854	-8.4	-6.1	-14.5

290

055

147

50196 6 48.5 -45 23 K5 III +149 C4

FD1150

6C 8902

6.54 +1.51 (2.54)

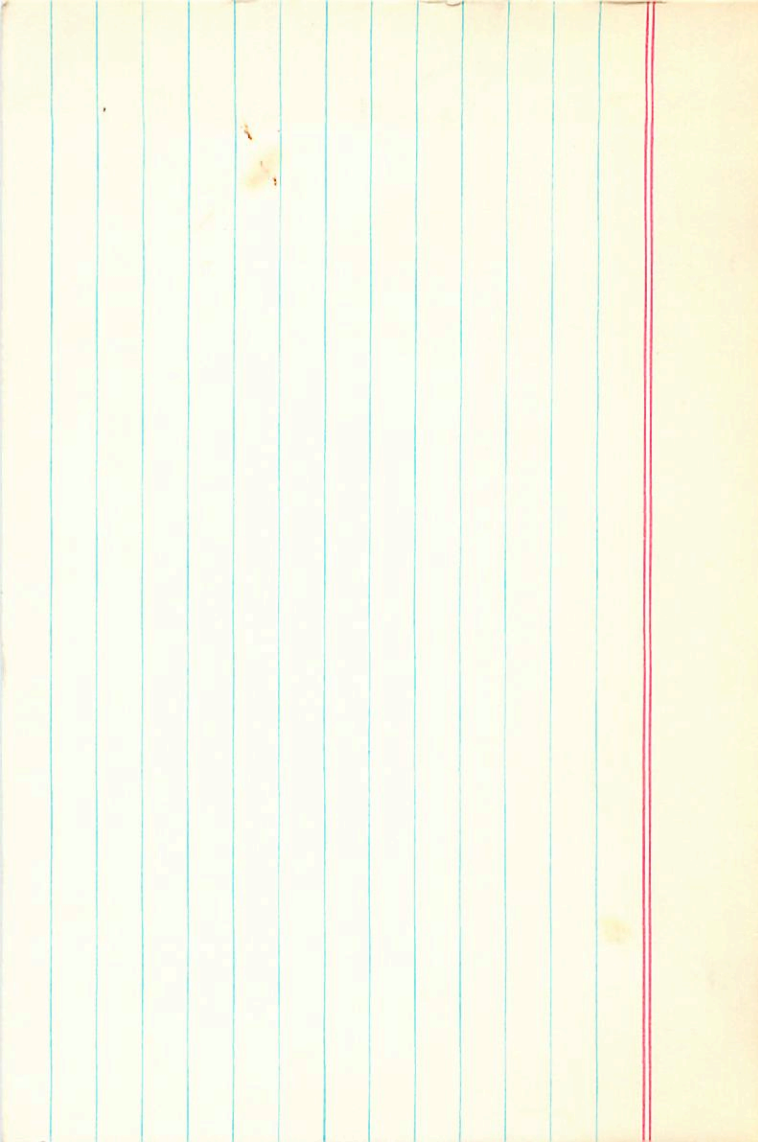
+0.0009 ±8.7 -048 ±8.0
-016

30.246 1401.3 -0.6010
 $\frac{-044}{202}$

24.23 1899.1
 $\frac{+2.44}{21.79}$

46.449
 $\frac{43.720}{30.166} -0.27$
 $\frac{175}{175}$

38.65 1927.07
 $\frac{-43.20}{22.303} -44$
 $\frac{122.35}{115}$
 $\frac{22.23}{22.23}$



W.O. P = 194
L 48.8 - 5.2 34 865 + 26.000

HR2554

50337
4466
8972

4724
844
24184
932
122

4.39 + 0.92 + 0.07 - 0.08 + 0.25
1009 ± 41 + 0.25 ± 3.4
46.134 8.5 ± 1000 4788 2.6
37/177 1.14
5.9° 2 70.15 - 12 4057
46.109 4755
1112 4754
46.180 (40.4) 4808.5
27/83 - 2.10 4754

10083 + 0.15
60046 + 0.176
- 6046
9107 + 0.15
413 4574 0.168
9107 4890 0.074

6.8
- 53.6
24
19
3.5
+ 260

91

2014
10/14/14

10/14/14

10/14/14

10/14/14

6.800
-53.688
24.800
18.800
3.500
50.12
26.800

4.05
-64.76

-8.247
8.963
8.189
65.478
6.119

+7.1

-8.388
8.885
-8.922
-25.802
-25.252

→ 256

8.888
8.278

18

50571

6 49.4

-60 11

+22,27
(2)

8987

~~8987~~ ✓

21.339 09.3

+1005 ± 6.7

+105 ± 6.3

2682 5.1

02

319

21.318

69.52

24.66

1/2

324

HR
2532

49944

6 49.5 144 54

+3c

1,7)
2,1

+010-08564 →

100 ps.

$$\begin{array}{r}
 \begin{array}{ccc|ccc}
 -254 & -250 & 934 & -0132 & +1007 & +0875 & +8.8 & +2.8 \\
 -384 & 913 & 140 & -0200 & -3678 & -3968 & -39.7 & +04 \\
 888 & 323 & 328 & +0463 & -1301 & -0838 & -8.4 & +10
 \end{array} \\
 \begin{array}{ccc}
 279 \\
 984
 \end{array}
 \end{array}$$

+011-089

+11.6
-39.2
-7.4

6 49.6 + 38.56

6.1
11.5
4.9

5534 A 6.11 + 0.4D + 0.14 2.60 2g A7

A 6.14 + 0.38 + 0.14 2.100

B 10.24 + 0.70 + 0.17 2.60 - 22" + 0.02 (+5.3)

B 10.20 + 0.68 + 0.19 2.100

-5
+6

-00021 + 0049 W350
-00025 + 0008
-0026 + 0057

p = +1

Solar Sp.

-004 + 0006
+ 0008 + 0004 0.6

loc

A B
6.03 10.13

95.5

6.03 10.13

+ 0.36 + 0.66

+ 0.12 + 0.16

S (-0.09) + 0.04

M_v + 1.2 + 5.2

-254 -151 + 955
-384 + 922 + 044
+ 589 + 355 + 293

-0046 -0029

-0145 + 0175

+ 0336 + 0067

-0125 + 12 + 10

+ 0030 + 03 -

+ 0403 + 3.8 + 3

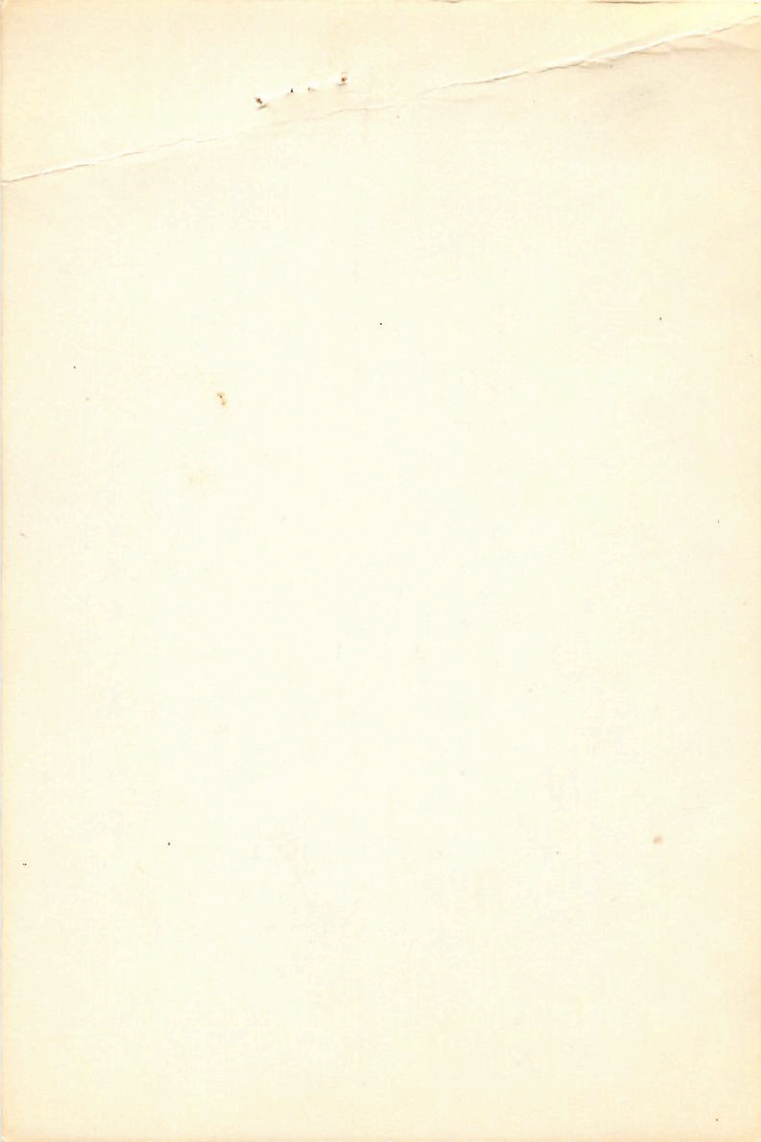
Σ K = 0

V = 0

W = +4

-0029 + 0055

-0004 + 0006



42

61002

ans e

q.d

8650
5598
x.d

9400	-1884	EL10	1
3912	-5827		

-00.10 = 9.0
-00.21

+046 ± 8.3
+027

50803

6 49.7 -47 16

+21.3 ± 0.86, (4)

7.32 + 1.16 10214 Cg

628996

$$\begin{array}{r} 44.122 \\ 49 \\ \hline 171 \end{array}$$

47 15 56.61 1897.4
~~-2.42~~
5903

$$\begin{array}{r} 2.589 \\ 41.520 \\ \hline 44.109 \end{array}$$

(40.1)

44.24 1926.38 -011 ± 5 + 0.86 ± 860
-46.42 -020 + 0.52 - C.P
57.66 -016 + 0.89 ± 1.86
-74 40.9
58.40

$\frac{110}{113}$

58.25
52.85
150 57.86
+11.17
43.5

174
 $\frac{187}{184}$
-0.84

44.067
 $\frac{4}{061}$

57.29
~~-14~~
57.43

1955.48

977-215[✓] -735678 -016+049 +31.3-036-23.156[✓]

016 035 003 008 038[✓] 180 +21.2-5+21

+5+66+16 004

+65-16-8

(8)

6.850
- 47.300
- 27.000
49.000
7.000
251
31.300

- 0.250
0.940
0.210
241.326
67.250

- 0.301
0.102
- 0.919
56.820
- 14.485

0.000
0.310
- 0.333
- 0.244
0.000

43

1702581
 50277
 5724153 185470
 2715
 6 50.4
 -0034±5.5
 -0055
 -034±3.2
 -036

27 5.8 ASn + 26.86

4491

9007

1914.5 78 26 33.79 1906.9

$\frac{155}{357}$
 $\frac{1.81}{35.60}$
 $-0045 -034 \rightarrow$

4.0

-0078 -034

$\frac{6.206}{33}$
 $\frac{241}{241}$

34.54 1433.1

21.6

$\frac{240}{117}$

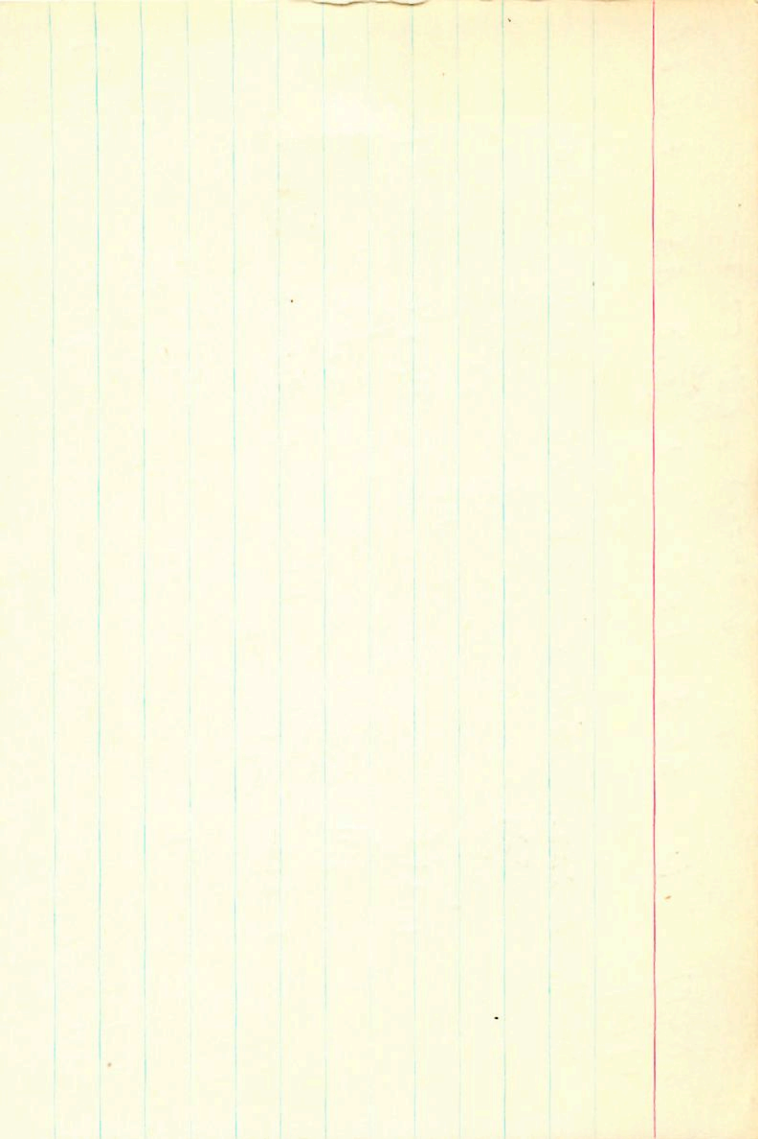
$\frac{34.23}{+2.2}$
 $\frac{34.43}{3635.6}$
 $\frac{1938.14}{71.24}$

$\frac{6.212}{27}$
 239

61760

$\frac{34.57}{1.03}$
 $\frac{3635.6}{28.7}$

-254 354 900
 -394 818 -430
 898 454 072
 +0807 -0571
 +1220 -1318
 -2820 -0732
 +0236 +1.5 +24.1
 -058 -06 -11.5
 -3552 -21.9 -1.9
 -12.1
 -23.8



-0024 ± 3.6
 -0028
 $49.0 + 23$
 40
 5.8 g MS

4471

8976 57.907
 $\frac{119}{58.026}$

57.917
 $\frac{26}{58.173}$

26.752
 $\frac{21.143}{57.895}$
 $\frac{17}{90.28}$
 $\frac{30}{940}$

57.914
 $\frac{19}{94}$

1504.2 + 23 39 45.42 1504.9

$\frac{59}{46.01}$

$\frac{24}{45.55}$
 $\frac{79}{45.79}$

$\frac{43.00}{80.42}$

$\frac{16.2}{47.42}$

$\frac{119}{45.80}$

$\frac{99}{45.99}$

45.59

1504.9

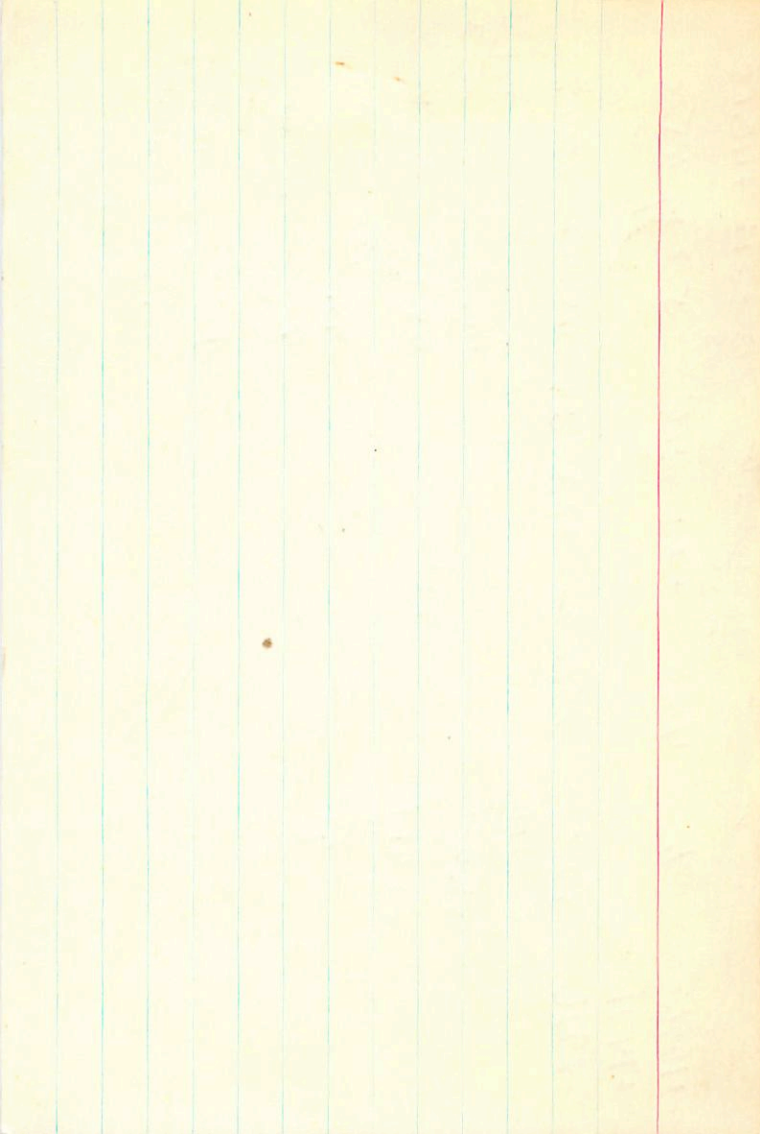
$\frac{34.1}{29.2}$

1935.0

1927.80

$\frac{79}{45.79}$
 -0.22

1939.58



156 Ma

B1 IV

2571

6 51.4 -20 8

B1 IV

50707

+81 ①

9034

483 -21 -94 35

2.629

33862
51.4
11.0
1008
1008

-084 +055 -002 ③

2.544 ④

35

-606 000

+70 1307 6

E + 06

113.8
MV

V0 465 9.45

AV0 -27

MV -48

44



2571.000*

2574
50806 6 51.4 -28 28 6-5 IV

3.20

629038

-53 -116 0

79023

-206 -133 +24/100

"
+1.97 -440

+71.5

6.02 + 0.715 + 0.255 (2)

0.00

5.04 + 0.235 (2)

539

80309

504
320

348(10)

7/10/10

856(7)

425 223 384

436 226

380

6.06 437 230 311 (2)

32237

4

53.3 114

DRG

29m(4)
440(4)

8.2410721024K

4.12

-28.3

-56 -116 -40
-43 -224 -71 / 100

440(4)

"
-405

PO

515
895

9.31

-0033±10.0 -073±7.5 6.34 ± 5.5 + 6.9
-0030 -070

50384 50384 6 51.6 445 54 67 +30.78

1402556 9039 4505
-0036 -080
-6.11 -074
-0033 0

-034-07366
-017-0636(2)
-025-065

W4505

34637 1408.5 445 53 30.10 1904.6

-0034 -074
-036

23.41
3.31

19269 20.3

576
28.8

21.5 1927.6

44.24
50.512
34.124
70.7
714
-060

-4790

143
21.72
-1.6
-1.6

33.60
-1.66
31.94

152.28
29.745
15.54

31.226

37.543
+ 2.2
1.615

21.3163 1930.0
-31.57
31.57

34.6733 / .703

24.55

975 - 223 715 656 - 025 - 068 + 30.7 - 049 + 22. - 223
024 048 006 011 062 256 + 214 - 5 + 21

$$+1 + 47 \quad 0$$

01

$$\boxed{42 - 21 - 9}$$

015

$$-1 + 35 + 7$$

$$\boxed{+36 - 11 - 2}$$

011

$$+1 + 44 + 2$$

$$\boxed{+10 - 17 - 7}$$

407 979 708 145 3-35 0-536 059
408 1054 44127
6 51.9 -11 5-8 +97.3a

OCmc

2574 4.07 +1.46 R₂ III
5075 1.249 2.24 FM 0=024
4154 1.224 1224 2600 2024
9051 -0095 ± 1.0 -018 ± 1.2 6 → 130

137.1 -0141

-00973 -0173 W₂ 50
-00954 -0177 5.95
-140
-141

-144
[-142 -017]

17K 3.75
+473
B162) 06
V0 387 (R-F) 480

-140
-141
3.75
+97.3

45

VEL.	:	07.000
DULUS	:	75
TANCE	:	3.750
DEC.	:	-14.000
R.A.	:	-140.000
DEC.	:	-11.000
R.A.	:	0.000
1 (U)	:	-0.250
2 (U)	:	0.240
3 (U)	:	0.718
50	:	04.000
U	:	10.000
1 (U)	:	-0.381
2 (U)	:	0.410
3 (U)	:	0.890
50	:	000.000
U	:	000.000
1 (M)	:	0.000
2 (M)	:	0.400
3 (M)	:	0.000
WB	:	-000.000
M	:	-40.000

76

R.A. : 6.850
DEC. : -11.950
R.A. : -140.000
DEC. : -14.000
TANCE : 3.750
DULUS : 56
VEL. : 97.300

1 (U) : -0.258
2 (U) : 0.646
3 (U) : 0.718
dU : 124.583
U : 76.887

1 (V) : -0.381
2 (V) : 0.615
3 (V) : -0.690
dV : 206.666
V : -55.542

1 (W) : 0.888
2 (W) : 0.452
3 (W) : -0.088
dW : -606.348
W : -42.632



E-010 643 082 222 923 2.851
M 11.50 7.16 520 -59 16

Am 1.6
25P
+038 15.9
+048

3.2

2592
51210
-19.716

-102224
-0024

+028 43.13 006
-021 -1.63
44.76 112.00

1.976 3.3 10010
103
519

GC 907

-007 +033

32386 2240

9137 -1419
4064 9899
+22705
0038
708 70.08

22.092
1.47
-15

5115
520
43.35
43.54
+5

-0019 +031

-0016 +037
-0122

43.96

12.2

1.445
2.10
1.450 43.00

1.450 43.00
+2453 -49
43.44 +0277

FU Car 6 52.4 -59 32 +3072

$r = 0.74$

11.92

+25 +52

+0.43

+9

-19

~~58~~ +3

-13 -35 C(60)

~~45~~ -32

1538

-263 +965 +6 +1005 -1008
-378 -100 -921 +0.08 +0.14
+887 +245 -390 -0.52 -0.78

-1023 -1573 +1.8
+225 +340 -282.7
-0.535 -81.5 -119.7

-10 1449

Aug 11

6

52.4

-1

19

+11.8

8.5

margin 85% - 1.5

111.0

M₁ = 00

8.5

-3
-25
-51

$$\begin{array}{r} -0.15 \\ -0 \\ 0 \end{array} \begin{array}{r} -0.21 \\ + 2 \\ -1 \end{array} Y$$

$$\begin{array}{r} -0.18 \\ -0.20 \end{array}$$

R

$$\begin{array}{r} 22.49 \\ + 18 \\ \hline 513 \end{array}$$

$$\begin{array}{r} 40.59 \\ + 7 \\ \hline 40.52 \end{array}$$

1937.51

1

96



+0024±3.1 +019 52.6
+002-1 +019

50551 6 53.0 +57 38 6.1 913 -5

4535

9081 52.165 1897.4 +57 37 45.62 1894

$$\begin{array}{r} 126 \\ \underline{.039} \\ \hline \end{array}$$

58.0

542

$$\begin{array}{r} 48.82 \\ 8.293 \\ \hline 57.113 \\ 57.118 \\ \hline 0.327 \\ \hline 657 \end{array}$$

42.4

$$\begin{array}{r} 87.8 \\ \underline{5020} \\ \hline 47.60 \\ -223 \\ \hline 45.37 \\ \underline{.6} \\ \hline 45.77 \end{array}$$

$$\begin{array}{r} 365 \\ \underline{128} \\ \hline 493 \end{array}$$

$$\begin{array}{r} 45.48 \\ \underline{45.48} \\ \hline 0 \end{array}$$

$$\begin{array}{r} 57.139 \\ 22 \\ \hline 1172 \end{array}$$

1446.97

$$\begin{array}{r} 45.55 \\ \underline{17} \\ \hline 45.38 \end{array}$$

1944.77

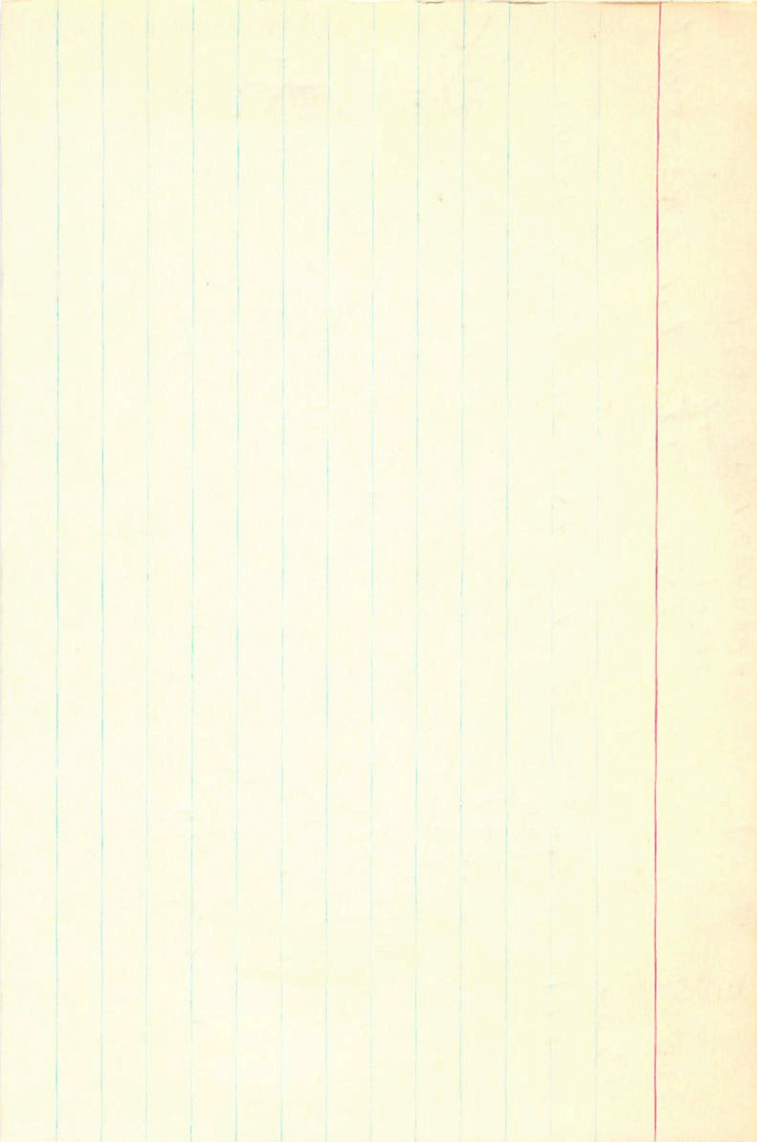
$$\begin{array}{r} 45.46 \\ \underline{.16} \\ \hline 45.30 \end{array}$$

$$\begin{array}{r} 57.126 \\ 34 \\ \hline 156 \end{array}$$

$$\begin{array}{r} 45.30 \\ \underline{45.30} \\ \hline 0 \end{array}$$

39.8

45



15 days

1 + R 25.50

6

48.6

+ 58

3.3

566

+ 8.92

+ 0001 = 1.2

+ 58

- 134 E 1.0

4.5

50522

4536

5082

AD55586

57.209

- 5

204

47.23

10.052

5.170.5

6.23

57.285

- 19.9

.192

W, SD

57.173

10078 - 1345

336

1946.97

29.45

1945.57

209

29.45

2.512

1946.97

29.45

1945.57

1529.6

10.0

35.8

50.15

1928.3

718 4977 1881
6121 - 830
+ 113

33.98

40.2
42.4

+ 001 - 1346

26.99 1847.8

6.44

33.98

40.2
42.4

1928.3

50.15

31.75

2.314

2.512

29.45

2.512

1946.97

29.45

1945.57

27.51

27.28

27.28

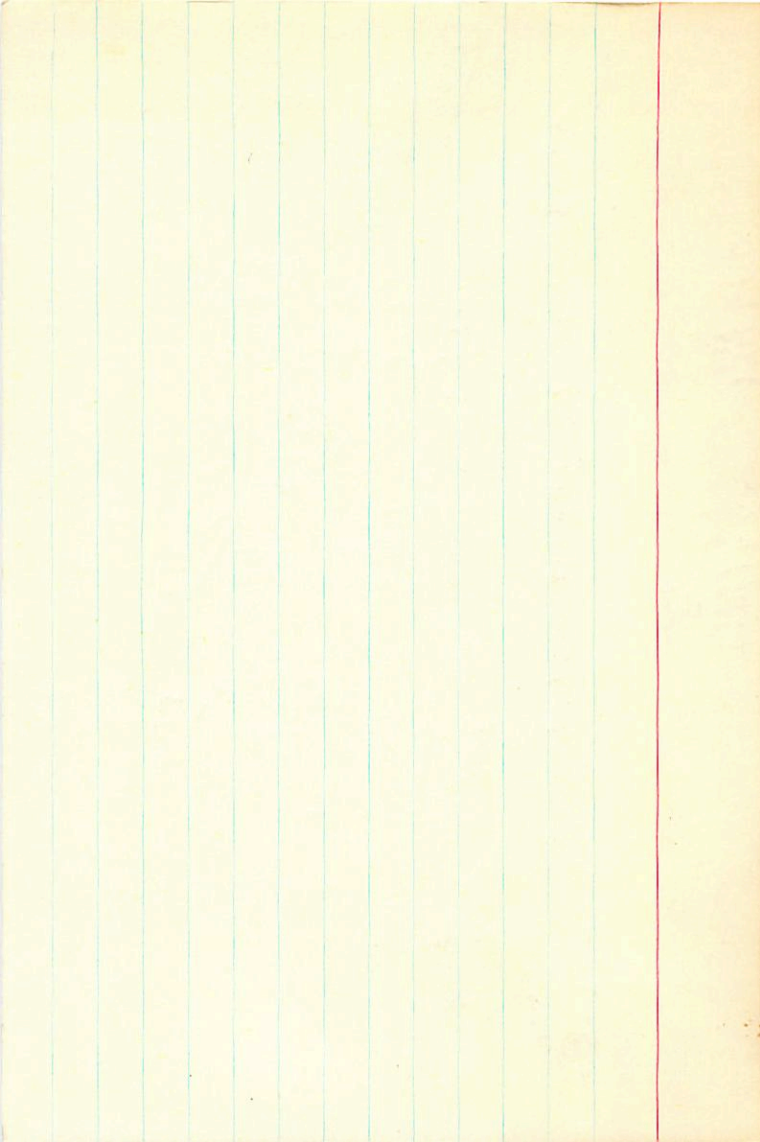
5012
- 004 - 139

57.173

27.51

27.28

27.28



27

15 dyn

6 52.9 +58 29 G-5 III -15

256d

44 } "
55 } "

AB 4.35 +0.85 +0.51 35

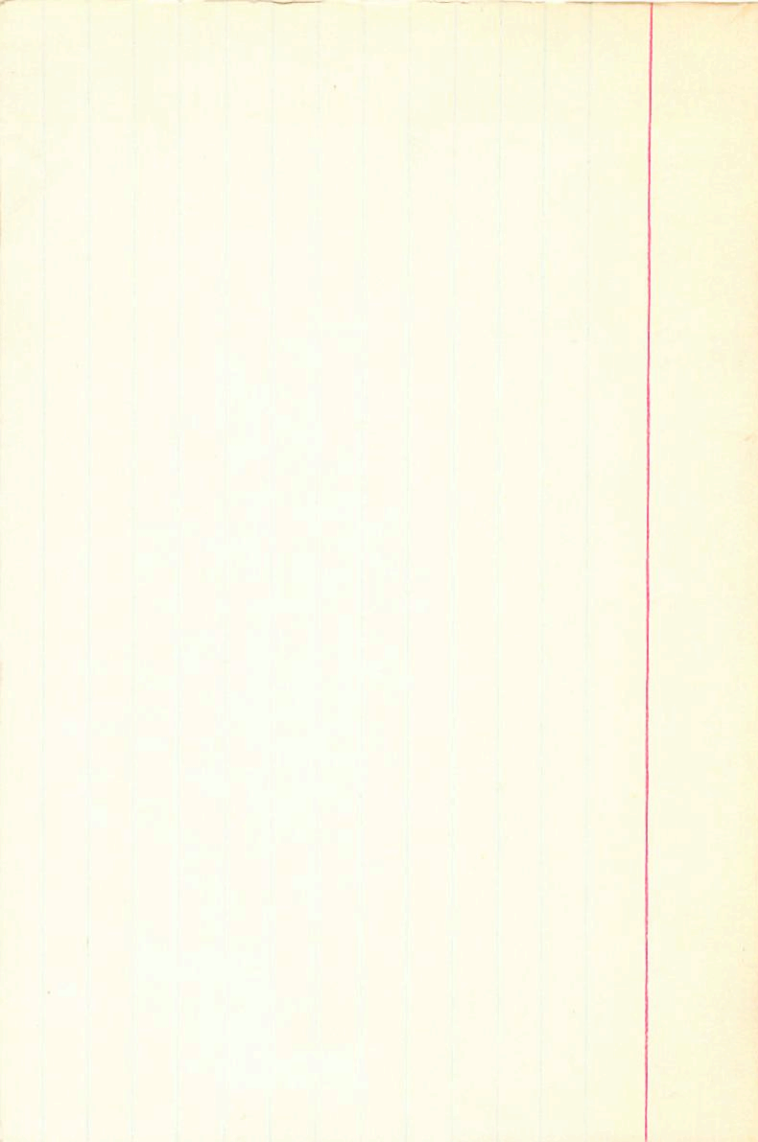
50522

4.03 +0.30 35

X

b1.0

+0.00010 -0.1360 G-6 + 1846



-0096 ± 9.0
-0082
-084

50763 6 53.2 + 46 46 6.0940 + 39.36

9089

4539

13.809 1509.2 + 46 46 21.01 1903.3

+ 392
14 201

+ 448
25.49

18.2

22.62
515120

14.137
-0.47
13.667

17.1 1924.7

-51.40
25.78
-1.98

14.051
-1.50
12.551

547
1927.4
241.1

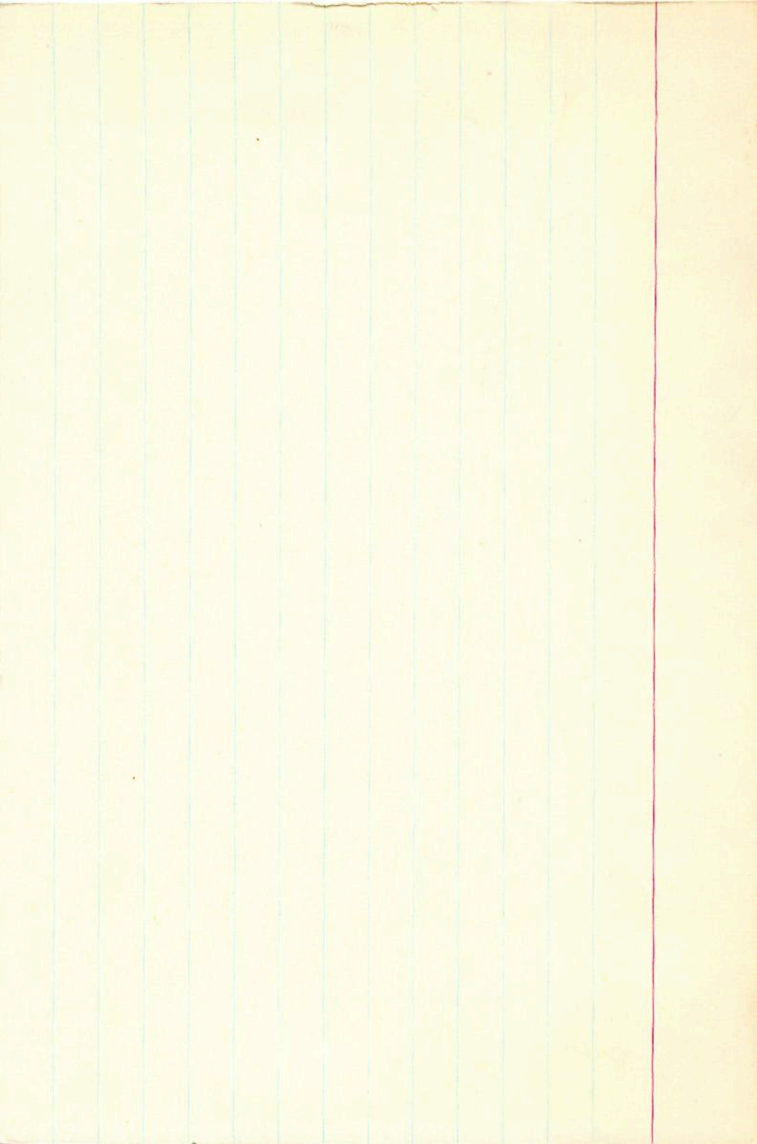
491
23.40
-2.03

22.94

13.98
2.1
11.0

23.0 1930.0

13
2297



2589

51104 6 53.7 +10 01 5.9 88 +33.0 8

4347

24

9100 -0009 -021 N30

-0019 ± 4.2 -020 ± 3.4 GC → N30

-0.199

$\frac{-0.199 - 0.20}{-0.13}$

6.3

6.9

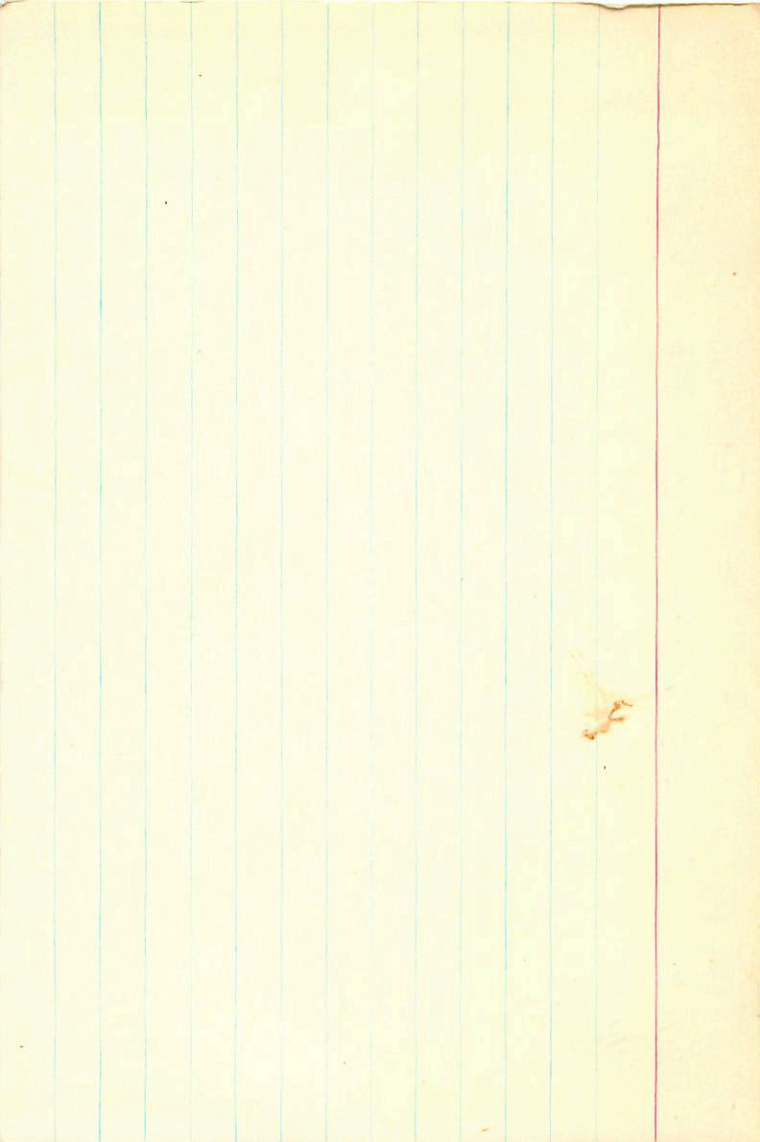
+10

-18

-20

6.3

+33



51220 6 54.0 +60 10 66's +47.28w(4)
 +00717 7.46 +1.02 +2.06 2.184
 W4556 7.41 +1.025 +0.81 29500

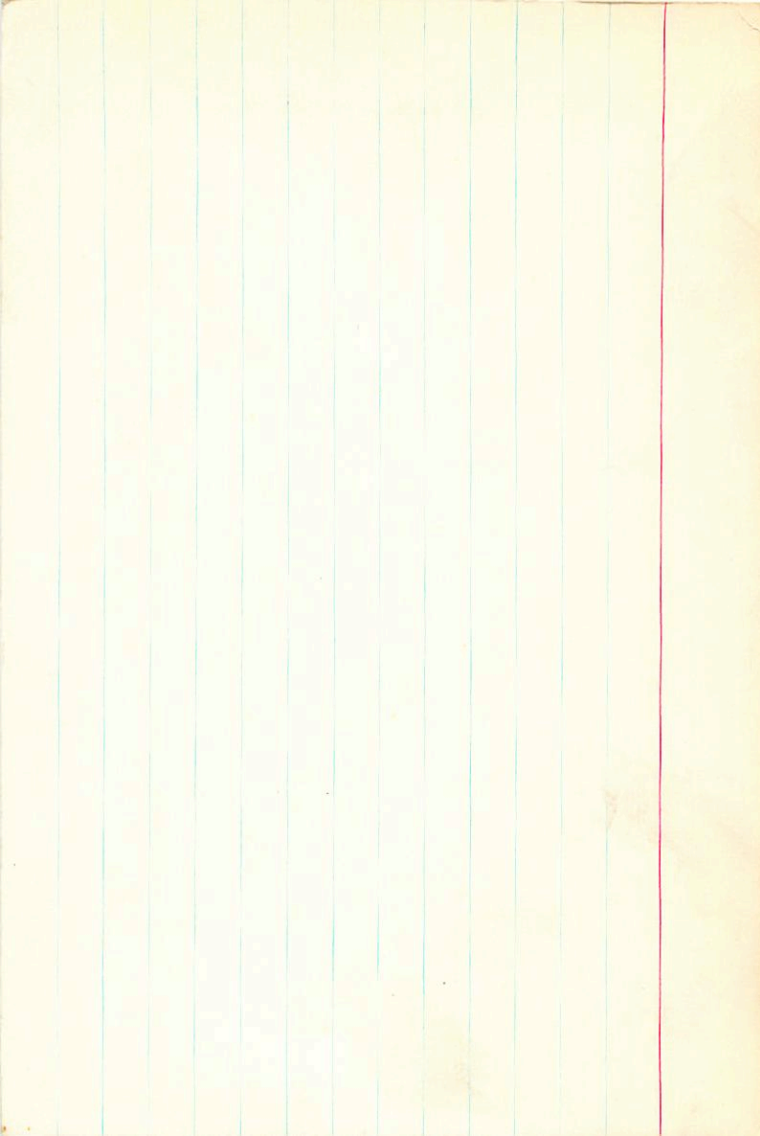
.59,444 +0 10 20.79 1937.57
 $\frac{24}{47}$ $\frac{10}{20.89}$

-0.3946 -00024
 0 +2
 -004

+42 -24 -6 .002
 +40 -21 -7 .100

Hyades

—



104

132

0.0

MS

4-11

6.800
38.950
-4.000
6.000
5.000
1.000

-0.247
-0.152
0.957
-0.677
0.889

+0.9

-0.388
0.920
0.046
31.902
3.236

+3.2

0.888
0.388
0.286
-0.046
0.002

0.0

42

6.80000
38.95000

50019

6

4914

+34

01

A8 III

Ans E

Q. No

33018

3.54

060 175

1763

2.848

12 = 1008

1964

997

+1008

18.0

5598

9400

-1884

7516

3412

-9827

10473