+0048 ±13.0 +052 ±13.0

176427 18 58.8 −44 13 8.34 +0.32 G_2(4)

26133 F2 IV +14.4 ±1.1

45.958 1903.0 −44 12 47.63 1902.8

−226 −2.45

,73 2 50.08

+0009 ±5.7 -002 ±4.2 +1.1 DD
+0006 -006

176774 18 58.9 +19 14 6.3 R1 III -28.9

26136

11469 54.229 1904.5 +19 14 15.30 1902.5

-041 .110

.188 15.40

54.216 14.94 1933.0

-3 9

213 15.08

54.197 15.22 1939.57

0 +11 D.57

205 15.33 36.3

+017 15.20 33.8

31.8 -20

4840 8140

-8410 9494

12 Aql

-0016 ±2.5 -034 ±2.2
-0013 -038

176478 18 59.0 -05 49 4.2 gK1 -43.9a

26141

1147R 0.587 1896.6 -5 48 39.83 1897.0

085
.672
40.527
20.132
0.659
-7
652
-21
638
0.605
-4
599

618
-054

40.7

+1.80
38.03
46.02 1934.83
478
41.24
1.41
39.83
+21
39.62
39.54 1939.77
+4
39.50 39.54
-1.53

460
37.3
40.3

+0013 ±2.7 -088 ±2.0
+0012 -074

16 Lyr 19 00.0 +46 52 A4n +7.66

HR 7215 +77194 5.00 +0.18 +0.07 +013 -088 GC

26181

W11497 11497 A7 +014 -086 Gn(2)

+021 -087

3, A (25) 1,399 1890.6 +46 51 46.65 1894.8

077

322 +0010 -082 4.86

32.38, 51.51

1925.7

+241 +434 -210 1.8.97

+354 +096 +928 42.398 40.0

-887 +345 +308 1.360 8.50 54

48.50

+ 370 365 371 49.31 081 27.7

45.40

-2.11 32.9

+0137 -3630 -3493 -13.9 -15.5

+0170 -0323 -0203 +048 +013 49.23

-0420 -1341 -1741 1.35 -14.9 -7.0 48.9 1929.7

-11.3 -1.6 361 -15.6 -32

-0.6 +7.1 -3.4 48.58

-5.7 +2.3

-946 259 730 683 +014 -087 +7.4 -064 +5.5 -280

014 -062 004 -017 147 -275 +5.2 +1.3 -5.0 023

+7.7 -17.0 -6.8

+17.5 +6.2 -7.1

+6.2 -14.2 -3.5 03

+13.8 +6.5 -4.9

.229

315

+15.0 -22.7 -13.2

11498 19 00.1 +74 59 6.5 dF3 -27.46

26183 (5247)

178089

+42 +08

6.54 +38 -06

357

-0126 ± 2.2 -062 ± 2.2

-0093 -055

+76°71.2

4.198 18873 51.01 1889.7

790 374

.988 5475

-.0120 -057

4.225 51.62 1945.29

24 .08

.449 51.70

.539 -2.05

ABS11572

+0003 ±4.9
−0006

+005 ±5.4
+012

176884 19 00.1 −19 19 6.0 GGL −20.28

26184

11500 7474 1901.4 −19 19 9.5−1 1901.1

9"8" −015
1459

−24
9.75

39.330
28.172
7.502
−16
1486
−10
1476
+017

18.72 1928
685
11.87
158
10.32
+24
10.08
+33

177W8 2 18 BD.3 +14 30 -16 Van [illegible]

6q2 +58 G29

+0 114 +001 174

+168 +001 /

24.

-16

177159 19 00.7 +19 35 6.2K1 III +1.3 DD -7.01

26198

11509 −0004 20 +002 22 N30

−0003 ±4.4 −004 ±4.4 GC → N30

922

54 Sgr 19 00.7 −22 47

8.1v gmc
+42c

177017
−2204958

−0021 ±5.7 −027 ±4.5 [illegible]
+3 ±2
−0018 −025
±025

+008 −012
−6 +1
+002 +011
+5 +2
+007 −011

291 122 −944 | −0344 −0144 | −0488 −22.7 = −62.8 −35.8
359 905 227 | −0425 −1072 | −1597 −64 +9.5
−887 407 −219 | +1051 −0482 | +0569 +17 −5.2

17689 75 J 2183877
-358 13306 19 0.6 -38 08 8.55 +0.66 Cyg

I 1391 G5B 464 yr. B-V

a=0.20 9.7

+4.4 S(M-M)=00

+0010 -042 Y+C 3 1966 8.44 +0.66+0.2

+0.12 75

+011-043 393 2882 0443 9.74

-8492 -7566 0021 433

-1.15 5.4

0.0087

5.29

+0008 -46 Gy $P_c = -38.6$

+0017 -019 Gv +33

+0022 -065 Gv -64 .74

13 Σ mass = 1.49

+00332 -0631 1.74

+0274 0688 p.v. +2.1

+026-064 +0060 0.0136 4.33

19.000
R.A. : -38.100
DEC. : 33.800
R.A. : -64.000

```
                19.000
   R.A. :      -38.100
   DEC. :       33.000
   R.A. :      -64.000
```

Pushmut Report

177474/5 $_{SM}$=0 19 03.0 −37 08 F8 V 385

7226/7 4.20 +52 0 C 385

G624243 2 488

δ UA 341 164 433 2.631

U4 .338 .169 .336 2.632 ② 4,2,7,6

[m] 230 +16 341 127

[C1] 268 −34

1.05 +54 −16.50

344 144 355 +3 −10 −8

336 145

350

344 154 365 2.430

+008 −012 ±12 Y

3 99

SU Sgr 19 00.7 −22 47 +420c

±57 ±4.9

−0021 −027

−0202 −024 FR4

−028 −024

530 +185

4.48 1.74

460

2346

2 3

58

815

m−M

8.50

9.35

8.75

176661 8.57 +0.045 −0.31 (1) A0 +195

176632 9.34 −0.04 −0.33 (1) B8 +10

176164 8.48 +0.05 −0.42 (2) B8 +185

541 540

162 142

5

515 5.30 5.4

333 5.40 352 347 E(R−I) = +11

E

+14

16

142

E = +19

SU Sgr 8.15 +164 +0.90 −5.1 −42 −64 +17 −25: +42.0 EC

177017 5.25 +1.90 8.35 −5 −14 +6 −25: GM6 −13°

9

0.000*

19.000*
0.700*
-22.000*
-47.000*
-0.028*
-0.024*
0.150*
426.580
42.000

-0.053
-0.948

-62.532

-0.150
0.231

-54.440

0.071
-0.220

21.221

ADS 11979 9m 5"

-0013 ±3.1 -030 ±2.2
-0015 -024

177483 19 00.9 +52 11 6.4 g G8 +4.28

26202

-1.6 (4)

11514

56.414 1895.9 +52 11 15.30 1886.6

070 1.90

.484 17.20

1230 5.7 1925.4

21.11 10.45

35.308 408 16.15

56.418 -076 1502

56.405 41

13 (39.3) 16.76

+5 16.20 2257031

418 1947.39 16.74 35.2

56.374

+9

383 16.15 15.76 1944.91 (48.4)

56.424 424 -25 -25

+5 -060 15.77 15.57 16.07

429 -1.19

177095 14 01.0 -20 32 1

9.61+0.66

172
57
+78.2 f 4.2
2297
-200 -522 Hyd. 9.12
~~+255 -550 (...) Tt(2)~~ 874
-242 -595 Yale (4.5)
~~-285 -605 Newitam~~
-245 -575 Tt(3)

→ -255 -575 4.5

177095 19 01.0 −20 32 dG3 +78.28 W(3)

−236 DR
−214 YR

GC 26204

W11516 9.4 2 24″ −172 ±15 (−207) ±15 GC

Y4422 −163 ±6 −603 ±6 mw

−20°5385 9.61 +4.65 1.65 −207 −293 ±7 −581 ±8 CR

−201 ±13 −564 ±10 Y

−241 ±15 −707 ±15 GC

−200 ±13 −564 ±10 Y

−293 ±7 −581 ±8 Cap RH

: −220 −654

−148 −294 −60 .010

134 (10)
150 (3)
−65 (8)
3 ±7

-0172 ± 15.0 -707 ± 15.0
-0163 -603

59.682 1911.1 -20 31 41.86 1910.8

669
0.3357

59.951
-3
948

3433
25440
0.270
-17
253
.2563
190
.064

242

17.3

-282

+27.71
14.15

27.86 1933.60
+6
2780

5680
28.4

32.2
+870
50
23.56
+1
94
21.123
71
21.

1923.2

951
24.76
-10.61

17.6

1+0177085 R5

-20°5385 19 01.0 -20 32 +78.28 (4/3)

9.41 +1.65 1.65 21 mc lum
S = 20

BC 26204 9.4

Y 4422

W 11516

-148 -294 -60

-253 -581
-225 -571
-253 -581
-287 -620
-264 -583

Ask Barnes

243 24
-236 -571 DR
-253 -581 CR
-214 - YR
010 -264 -568 Hyd corr
-242 -594 Y corr
-287 -620 GC corr

-214 YR
-200 -522 Hyd.
-241 ±5 -707 ±5 GC
-200 ±13 -564 ±10 Y.
-253 ±7 -581 ±8 CR
-236 -571 DR

13 Y (10)
15 D (8)
-11 C (5)

-264 -568 Hyd corr
-242 -594 Y corr

-253 -581 mean
-287 -620 AW + C + Y
-253 -581 CR

-272 -590 mean ←

19 177
191

-282 -90

-966 259 -367 920 -288 -40 178.2 216 -29 -2601

-272 207 -073 055 -1549 635 19 -70

-133 -6 -289

[-152 -280 -19]

-12 -5 -135

-65 2 -217

116 0 -135

-153 +1 319

[-167 -314 -19]

-13 1 -149

-74 0 -240

133 0 -149

-58 -38 -159

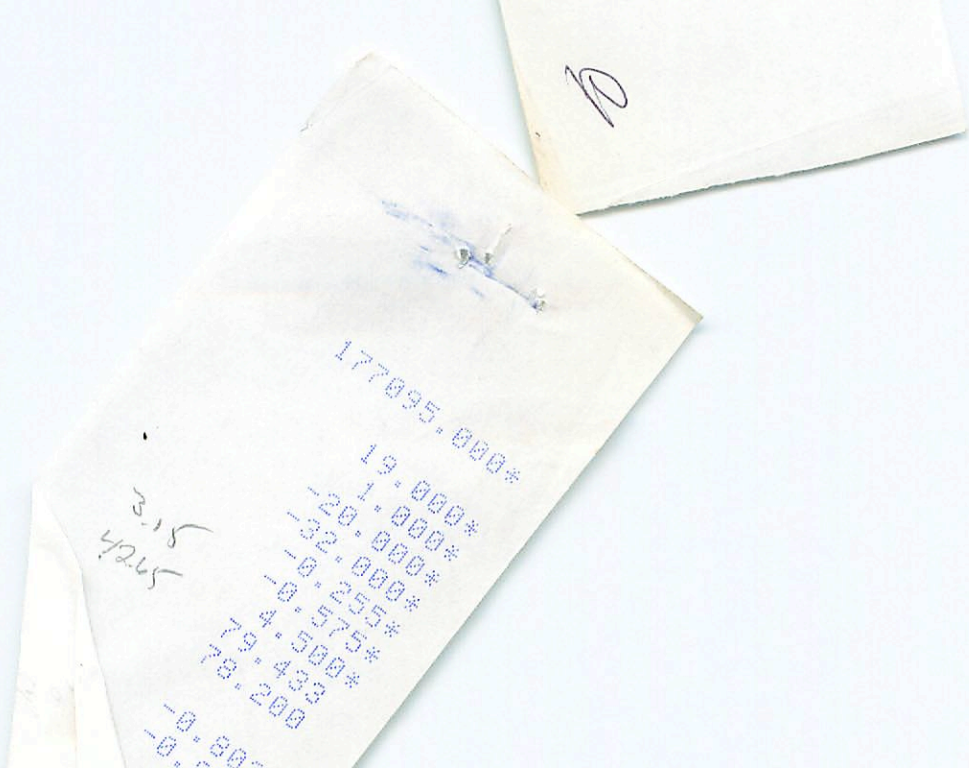
[-113 -131 -19]

-5 -33 -75

-28 17 -120

50 6 -75

```
0.0
-0.868

-29.287

0.013
0.487

21.421

-0.034
-0.095

-11
```


17095.000*
19.000
1.000*
-20.000*
-32.000*
-0.255*
-0.575*
4.500*
79.433
78.200
3.15
4/2.65

0 Sep ADS 11996

+0056 ±1.4 −062 ±1.6
+0053 −059

177241 19 01.7 −21 49 3.9 g G 5 +25.2a

26224 +27.2 (4)

11523 41.234 1890.9 −21 48 59.74 1891.9

−337
40.903

+3.60
56.16

11.363
29.758
41.121
−18
103
−10
93

42.7

10.11 1927.65
−10.10
0.01
157
58.44
+24
58.20

471.3
33.6

41.7

255
128
+225

41.177
−15
162

59.12 1939.48
+6
59.06

58.63
−2.47

AD011989 15 01.3 -21 36 -27

.177166 (congeal)

T 1887.0

27.3 (No)

0.97

Baird

A Aboyd

44,196

+0056 ± 67 -049 ± 59

20.862 99.1
-285
577

+0045 -048
+0048 -040
+0050 -046

2345 57.8
2.56
20.89

+00511 -042

0712

20.913
-21
892

20.923
-8
915

24.05 (69.36)
-25
24.33

24.05 (70.10)
-20
224
23.81

+0075±9.0 +0075±9.5 DS

177459 19 01.9 +0078 +17 29 +04.5 6.6 F4 -67c

26232

11528 -71.6 1G

55.825 1900.6 +17 28 46.11 1901.7

370 -3.63

455 42.49

55.724 734 359 44.48 19333 30

55.744 279 44.70 36.5

44.70 1939.7 34.8

+11

44.81

44.75

+2.2

177399 18 02.1 -08 44 K0 -71d v(c)

GC26234 -63.7 15th

W11530 7.5

-8° 4836

+095 ±8 +008 ±8 Y

+083 ±7 +017 ±8 GC

085 +014

+95 -4 -54 .005

+83 -4 -34 .007

+78 -13 -22 .010

-964 267 -151 588 +085 +014 -71 -002 +11 066

082 -002 023 0 389 099 -70 -19 +67 014

+056±7.1 +017±7.8 +9 +23 +16

+64 +27

5.930 1900.2 -8 43 39.99 +72 -17 -13

-279 -8.83 1900.7

5.651 40.82

5.876 40.16 1933.60

-10 23

866 99.93

ADS12007 Oplus 7m

-0004 ±4.8 -034 ±3.8 -20.3 (3)

-0003 -038

177463 19 02.3 -4 06 5.5 g121 -17.78

26235

11534 17.980 18943 -4 7 0.02 1888.1

022 2.10

18.002 57.92

59.874 13.10 1934.42

19.140 11.78

18.034 1.32

18.27 138 13 86

027 988 59.94 36.9

-23 +20 48.8

004 -014 59.74

42.6

17.978 59.90 1939.44

5 +13 59.76

912 59.77 -1.84

BL Tel 177300 -0003 +005

19 02.7 -51 29 +9.5

-51.11113 +008

-51.11917 -002 0002 +004 -0012 -026 ~~+004~~ FSI 6/5

34°.2 -0019 -034 -0112

-0017 -030 -013 -027

-0177 19.05

-020 -035 -51.5

-21

-27

10.00

R. F. Wing M.N. 125, 189, 1963

F 9.5 778 mp

HD7223 -002 107 pc 3480 -22.4 -0006 -003

7134 004 124 3436 -22.4

-0017

+00027

+0019 +001 +0043

46.512 (27.55)
57.648
44.160
-77
44.083
-41
.042

56.09
17.30
44.77 9 2
2.06
42.71
+21
42.50

(44.7)

43.74 42.2

43.913 1.1
-93
.820

42.31 58.5
-05 -05
42.36

43.769 (86.78)
-36
.733

42.10
-19
42.29

-0017 -002

43.794 (67.52)
-27
773

42.37
-19
42.56

=

CHECKSUM ERROR*

19.050
-51.500
-32.000
-35.000 10.81
10.000 145.79
1000
91.000

0.361
-0.342
-0.890
20.385
-58.398 -40

0.352
0.307
-0.230
-163.773
-204.854 -284

-0.585
0.244
-0.394
43.183
7.024 +27

19.050
-51.500
-21.000
-27.000
11.000
1585 1942.3
91.800

0.301
-0.342
-0.890
25.113
-41.902 -33

0.352
0.907
-0.230
-137.940
-239.701 -249

-0.886
0.244
-0.394
23.675
1.363 +10

11

+0055 ± 4.4 −071 ± 3.3
+0059 −077

177808 19 03.1 +31 40 5.8 gK5 +6.08

26266/

11545 3.454 1907.4 +31 40 6.52 1908.1

−234 2.97

220 9.49

3.414 7.34 1941.30

−8 −22

406 7.12 28.1

186 771 710

386 35.5

3.35 −23 7.9 1929.7 27.4

15 +66 −29

365 7.61 7.37

2.12

177931 19 03.1 +45 51 6.8 B9 −9.5 b

26268

11546 +0009[19] +024[20] N30

+0027±4.1 +017±3.0 (LL→N30)

+6501319
178326 19 03.3 +65 30 7.2 eg GS +20.48

3W

11550

+021 +037 GAZ
+005 +040 G1

ADS12029 [illegible]

−0005 ± 5.3 −068 ± 3.5
+0001 −066

177749 19 03.4 +06 28 6-9 1FY 17.86

26278

11552 21.183 1893.6 +6 28 13.60 18826

028 4.58

,211 18.18

8.13 C8
10" [illegible]

Δm=1.89

21.215 ~~+0017~~ −077 14.35 1935.2
7 16
222 +0008 −083 (Comb) 14.51

21.199 14.55 1936.47
10 (42.2) −3 1.67
209 14.52 35.8
216 +0012 −083 14.52 (55.2)
+005 −3.66

5340 4235 0807
−8455 −9060 −0242

V805 Aql 19 03.5 −11 44 ∂ = −39.6 km/sec

−35 abs

+067 −023 Y
− 4 − 3
+ 4 + 1

+067 −025

+308	+303	−402	+1008	−0360	+0648	+35.7	+42.2
+347	+847	+403	+1134	−1000	+0134	−15.9	−14.6
−886	+437	−156	−2895	−0520	−3415	+6.2	−28.0

177716 19 03.8 -27 45 3.4 gK1 +45.4 a

24291 +47 (2) V a

11558 -0038[51] -252[52] N30

-0037 ± 1.6 -251 ± 1.7 Ac → N30

38 ± 9

177017

R Agl 42° +0.5 12h

						E	m − M
177958	9.26	+0.34	−0.015	B8	②	+42	7.3
177832	8.57	+0.455	−0.08	B8	②	+62	6.9
~~178102~~	8.84	+0.11	−0.36	B9	①	+28	8.8
177624	6.86	+0.18	−0.365	B5	③	+34	6.55

+320

E = +0.20 +10

+0.002 −0.068

4.0 +1.80

3.80 1.73

220

1.60

35

1.22

63

7.5

12

-49.679

0.000
-0.159

-44.469

0.669
-0.208

-83.526

-0.744
-0.189

32.000
316.228
7.504+
-0.000+
0.002+
9.000+
0.000+
4.000+
19.000+

```
177095.000*

    19.000*
     1.000*
   -20.000*
   -32.000*
    -0.255*
    -0.575*
     4.500*
    79.433
    78.200

    -0.802
    -0.942

  -137.312

    -2.871
     0.267

  -207.175

    -0.059
    -0.205

   -20.675
```

3.15
4265

-108

-102

10

-18