

2531 ✓ 43082

-610 1263 9 32 40 -61 52 9.84 +13

9.89 -585 +250 -473 2.208 10 mon 76
9.68 -526 600 452 2.208 24 Apr 76
9.64 -580 79 452 2.208
9.68 -580 79 452 2.208

2.208

3404326 1660 08 - 254.1 -1.4

PS 20

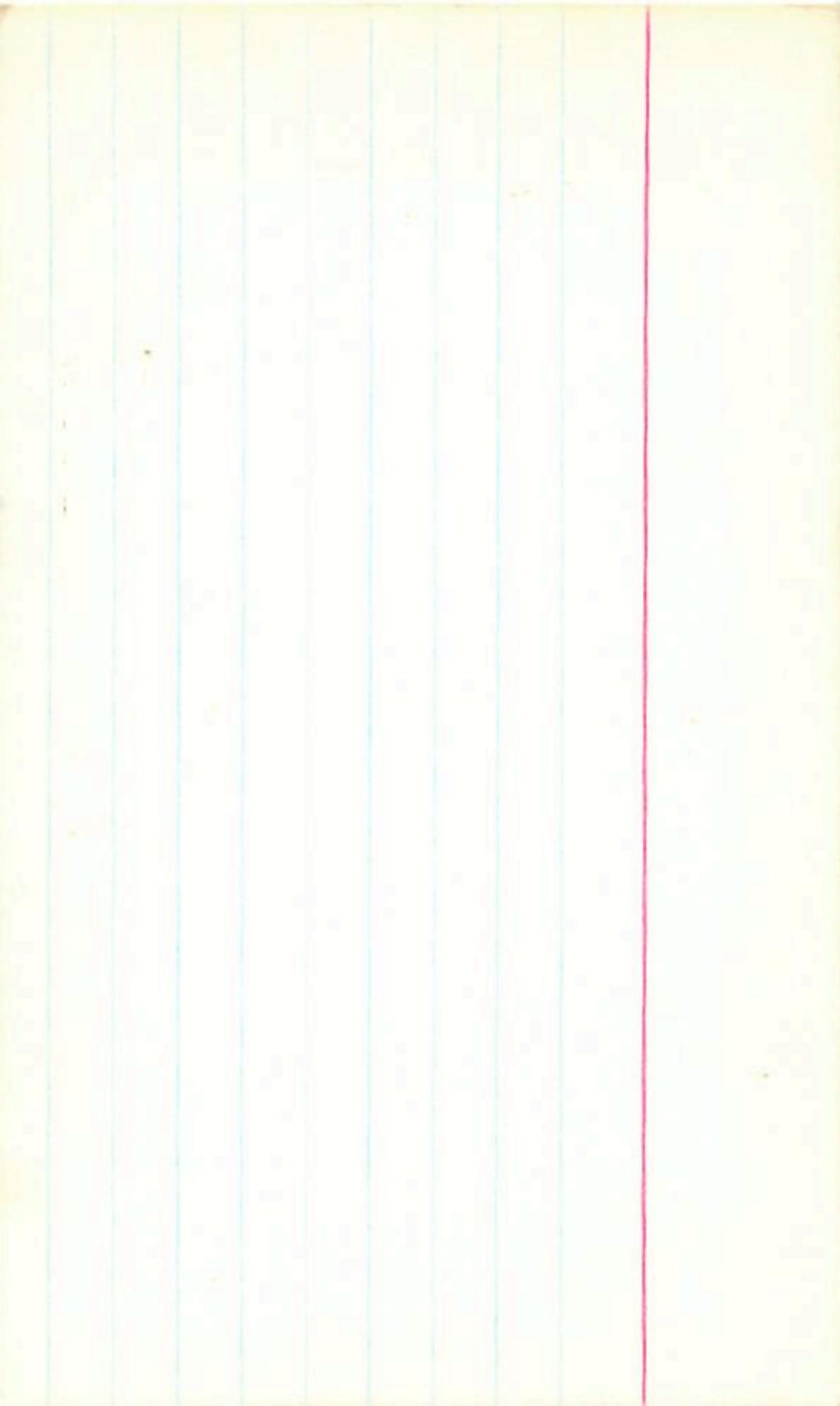
8 11 420 -86 36 237416 -55

9.42 -511 +701 -676 2.111 174
9.37 -519 692 -664 2.094 21.091 76
9.34 -505 701 -676 2.167 22
9.36 -517 710 -672 2.103 23
9.38 -514 701 -673 2.104 ④

~~16~~ ✓ 1044 00 254.0 +0.3
15 ✓ 1533 -35 32.5 -1048 +82.0 ✓

5

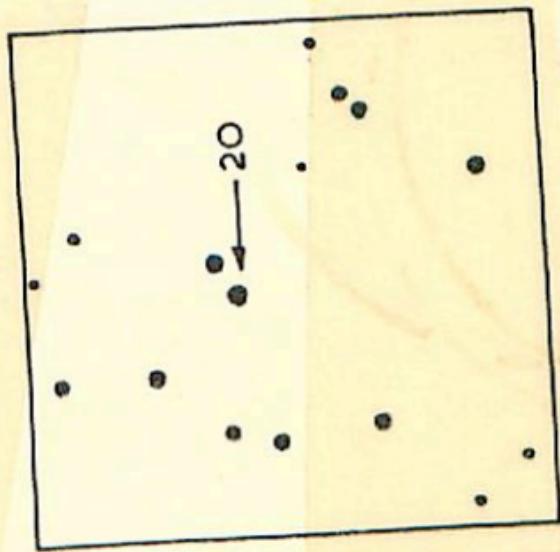
10.44 -89662 -675 2.085237 ✓
10.54 -866613 -577 2.092240 ✓

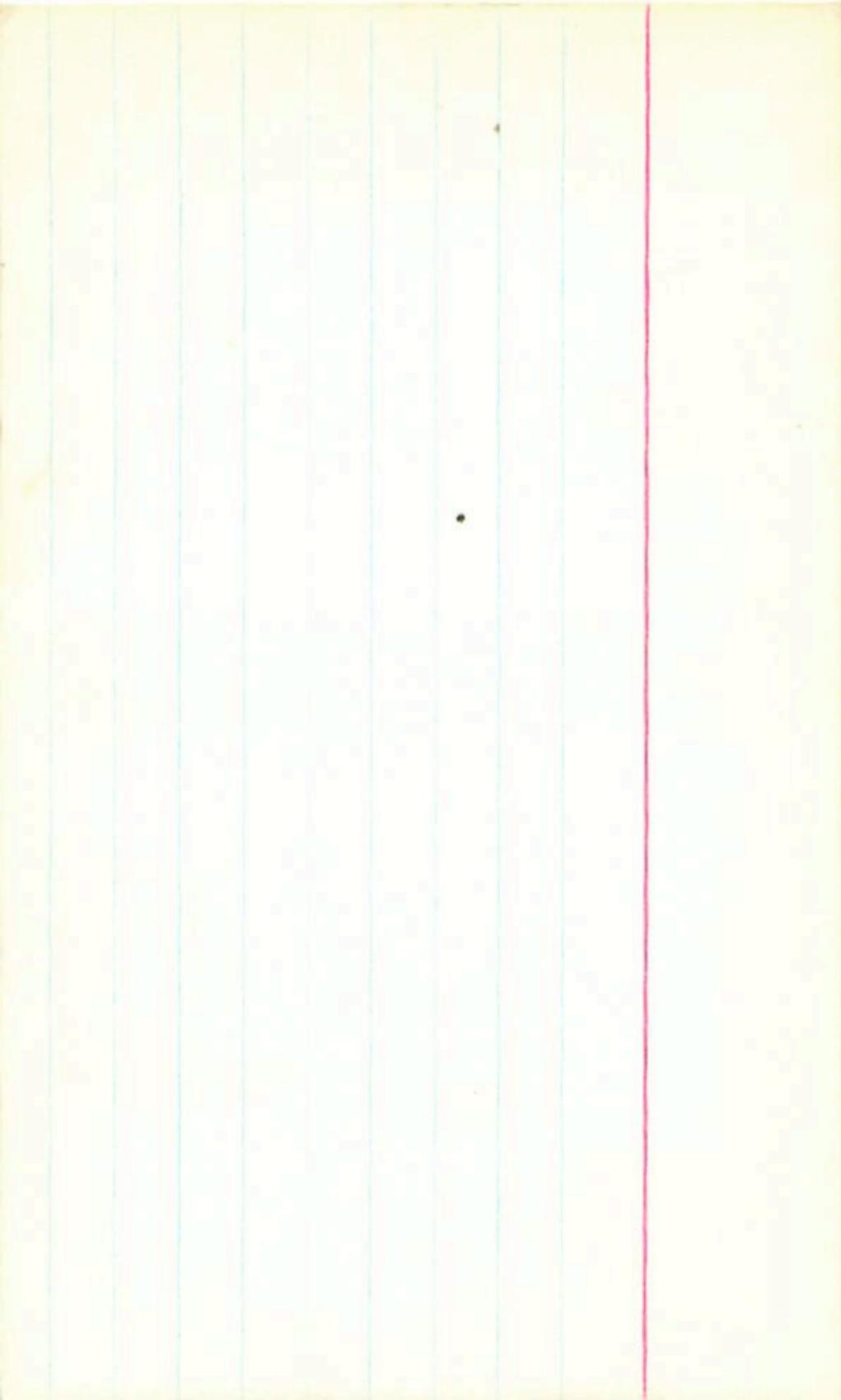


20 8 11 X 4 2 - 3 1 3 6 9 3 7 + 1 6 - 5 5

$$\begin{array}{r} 9.37 - 5.6 \cancel{6} 9.2 - 6.6 \cancel{.1} / 9.054 \\ 9.25 - 5.6 \cancel{6} 7.01 - 6.76 \\ 9.26 - 5.6 \cancel{6} 7.01 - 6.76 \\ \hline 9.38 - 5.6 \cancel{6} 7.01 - 6.71 \end{array}$$

2.101 (3)





RS 22 8 14 27 -36 00.5 11.5-01.17

-607 +764 -⁴⁴⁰₃₆₇ 2217

11.18 -643.775 -422 2356 21.75

$$B(803) = +0.11 \quad V_0 = 6.4$$

+0.11 +0.11 -0.05

$$2.14 + 0.47 - 0.16 - 0.10 \leq 0.2$$

$$\frac{7.11 - 0.76 + 0.67 - 0.47}{7.14 - 0.92 + 0.64 - 0.41} = \frac{2.103}{2.105} = 0.973$$

$$+0.7 \quad -0.7 \quad -0.5 \quad 2.16$$

$$26 \quad 8 \quad 13 \quad 0.8 \quad -36 \quad 58.5 \quad 2.14 - 0.9 - 0.42$$

$$+0.5 \quad 0.1 \quad -2 \quad -0.05$$

80.5 II

115 -3404359 1014 0B 3545 4.3

26 9 13 05 -36 525 2.14 -05 -62

7.11 -6676 +75 -157 2.103 26 fm 76
7.17 -708 +740 -891 2.105 28 fm.

7.11 -620 +661 -~~554~~ 2.094

7.17 -642 +726 -~~726~~ 2.096

7.18 -656 +727 -671 2.091 17 fm 76
7.15 -640 +726 -540 2.094 (3)

1002 CD - 34044494 0B + 2524 EO

1068 8 12 35 -34 24 932 + 35 -64

9.37

9.31 - 434 + 718 - 556 2.072 26 fm 75

↳ 9.31 - 383 + 704 - 951 2.063
2.997

9.32 - 383 + 711 - 593 2.075 17 fm 76

9.32 - 383 + 708 - 560 2.069 (2)

19

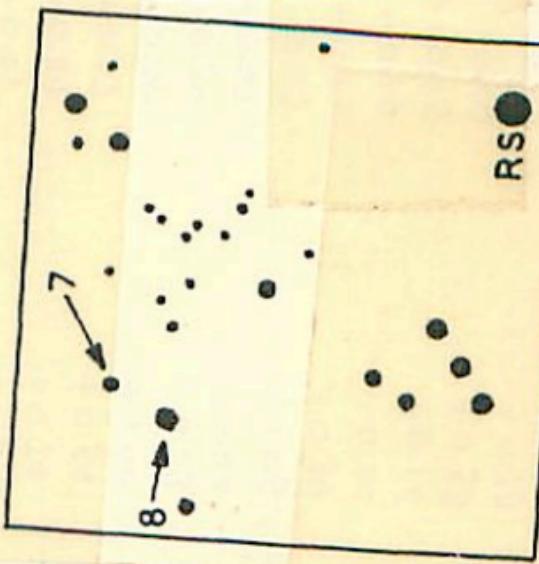
X X 8
7

12 34 -34 28

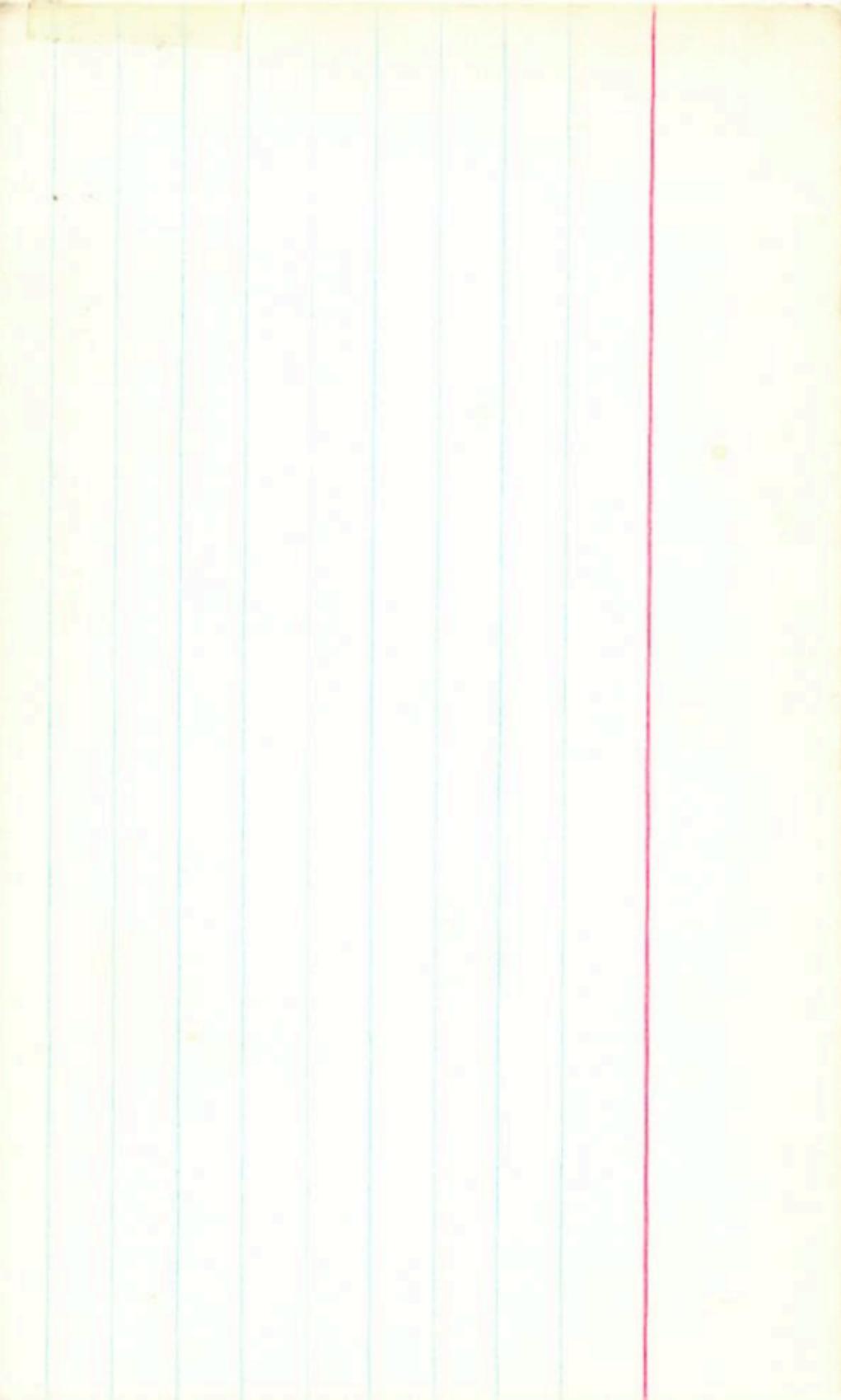
14 73

$$\begin{aligned} & 11.12 -509 +715 -782 2.137 \text{ 0.610} \\ & 11.12 -453 +701 -782 2.128 \\ & 11.04 -511 +743 -761 2.124 2.137 \\ & 11.01 -474 +731 -817 2.135 2.137 \\ & \underline{8.11.06 -481 +781 -786} \underline{-790} 2.130 \text{ ③} \end{aligned}$$

$$\begin{aligned} & 9.31 -439 +718 -596 2.072 2.130 \\ & 7 -373 704 2.071 2.133 \\ & 9.31 +320 +805 -160 2.546 \end{aligned}$$



R S



250.5 - 0.3

1051

3 06 35 -82 55.1 1005 +45 -41

$$\begin{array}{r} 10.03 -335 +68 \\ \hline 10.02 -305 \end{array}$$
$$\begin{array}{r} -274 +444 -767 -234 2097 \\ -268 \underline{-274} 2404 246075 \\ -814 -814 2.135 21.0176 \\ \hline 114 \underline{-114} 2116 \end{array}$$

+445 -463 +432

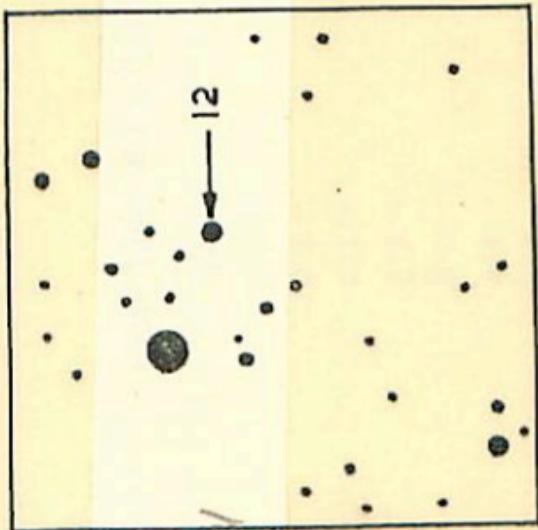
10.512 - 0.13 0.6 - 0.5 2.6 10.25 + 5.73
10.21 - 0.13 0.6 - 0.5 2.6 10.22 - 0.13
10.22 - 0.13 0.6 - 0.5 2.6 10.22 - 0.13
10.22 - 0.13 0.6 - 0.5 2.6 10.22 - 0.13
10.22 - 0.13 0.6 - 0.5 2.6 10.22 - 0.13
10.22 - 0.13 0.6 - 0.5 2.6 10.22 - 0.13
10.22 - 0.13 0.6 - 0.5 2.6 10.22 - 0.13

~~XX~~ must -7

1/2 8. 13 06 -35 26 10.25 +24 -63

540

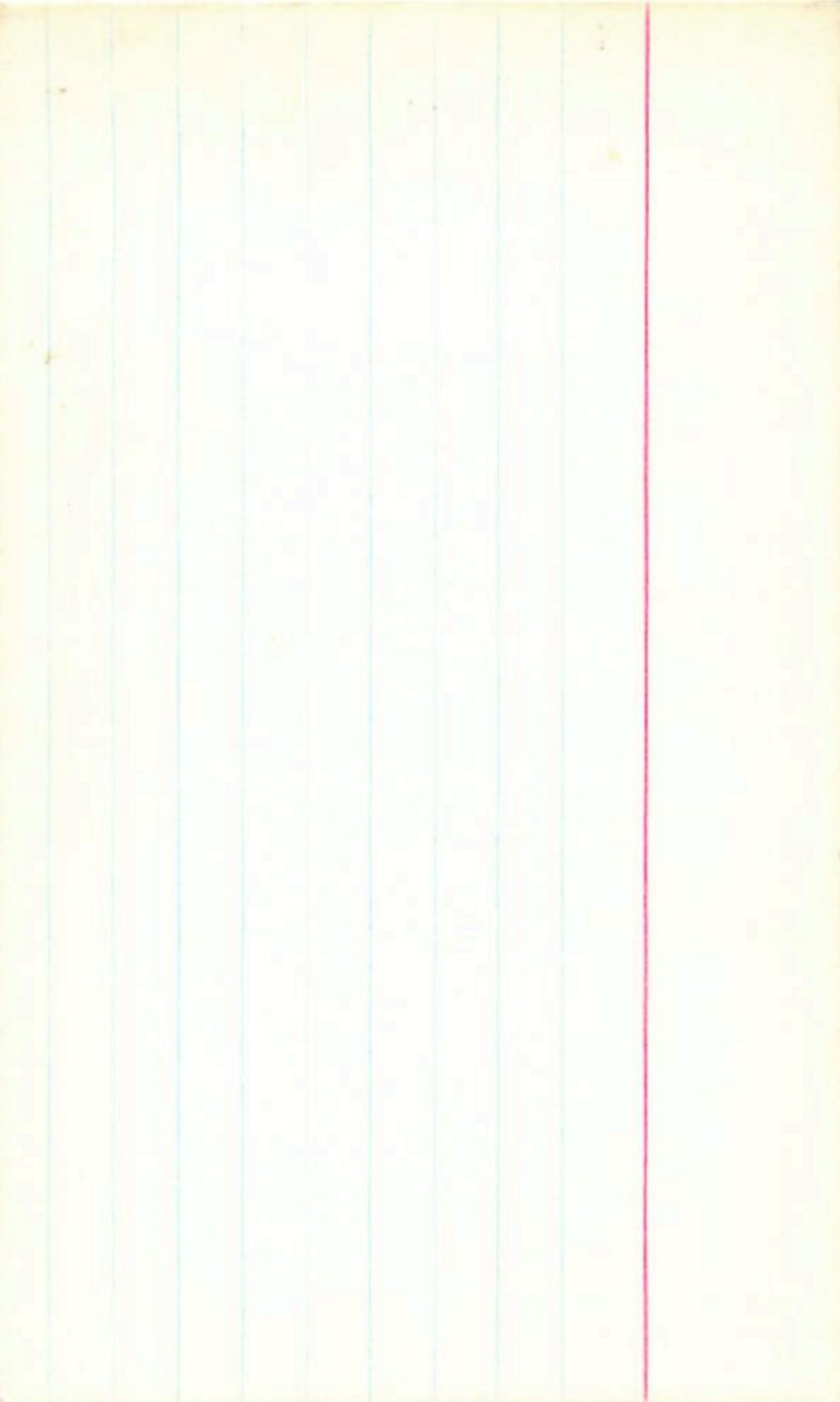
38



267

110-21-4844 #182-644 2132

10.22 - 460 + 660 - 608 10.22.3.11.8.③



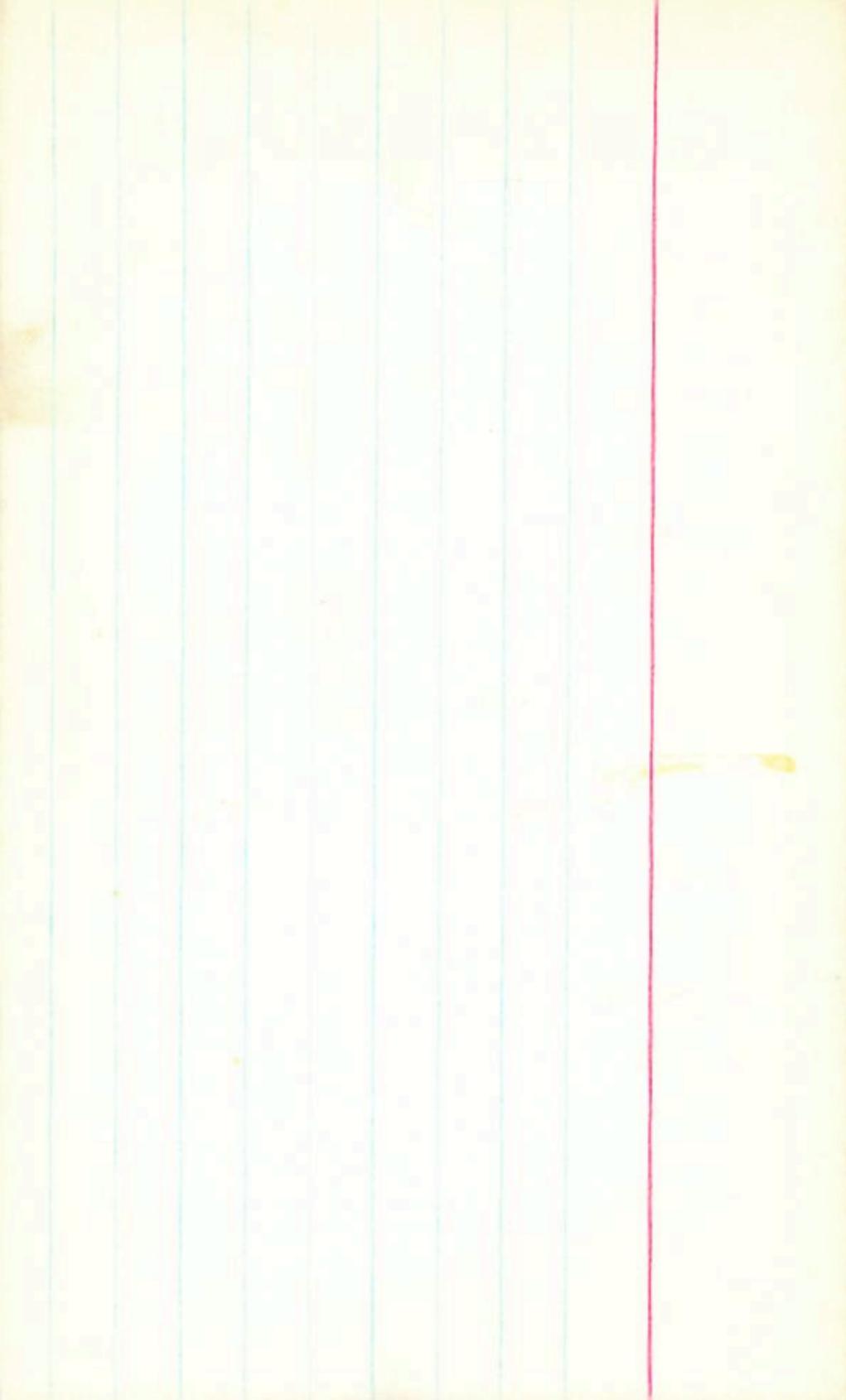
1017 08 252.9 0.0

~~9 88~~ 14 06 -34 45.1 -11.54 +16 -45

5

0.0000;

W



99.3 0.0 ne 251.7 +0.1

115.3 5 11 23 -33 45 11.18 + 9.9 - 5.5
-104.2
-25.7 +6.11 -10.9 2.06.3
11.15 -~~23~~ -33 +~~6.25~~ -10.54 2.61.2 2.6 fm 7.5

+ 56 - 67 2.575

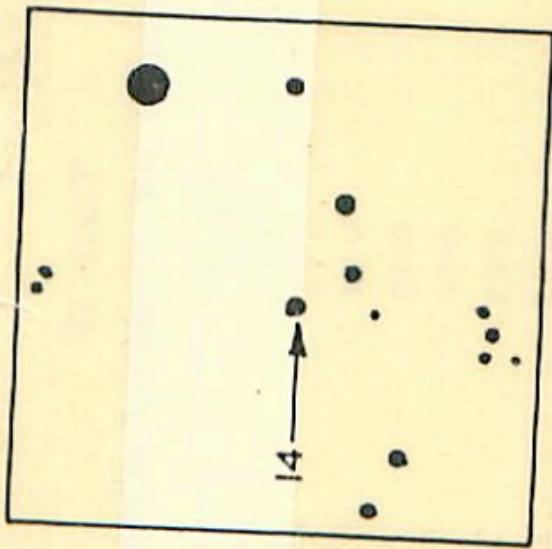
68

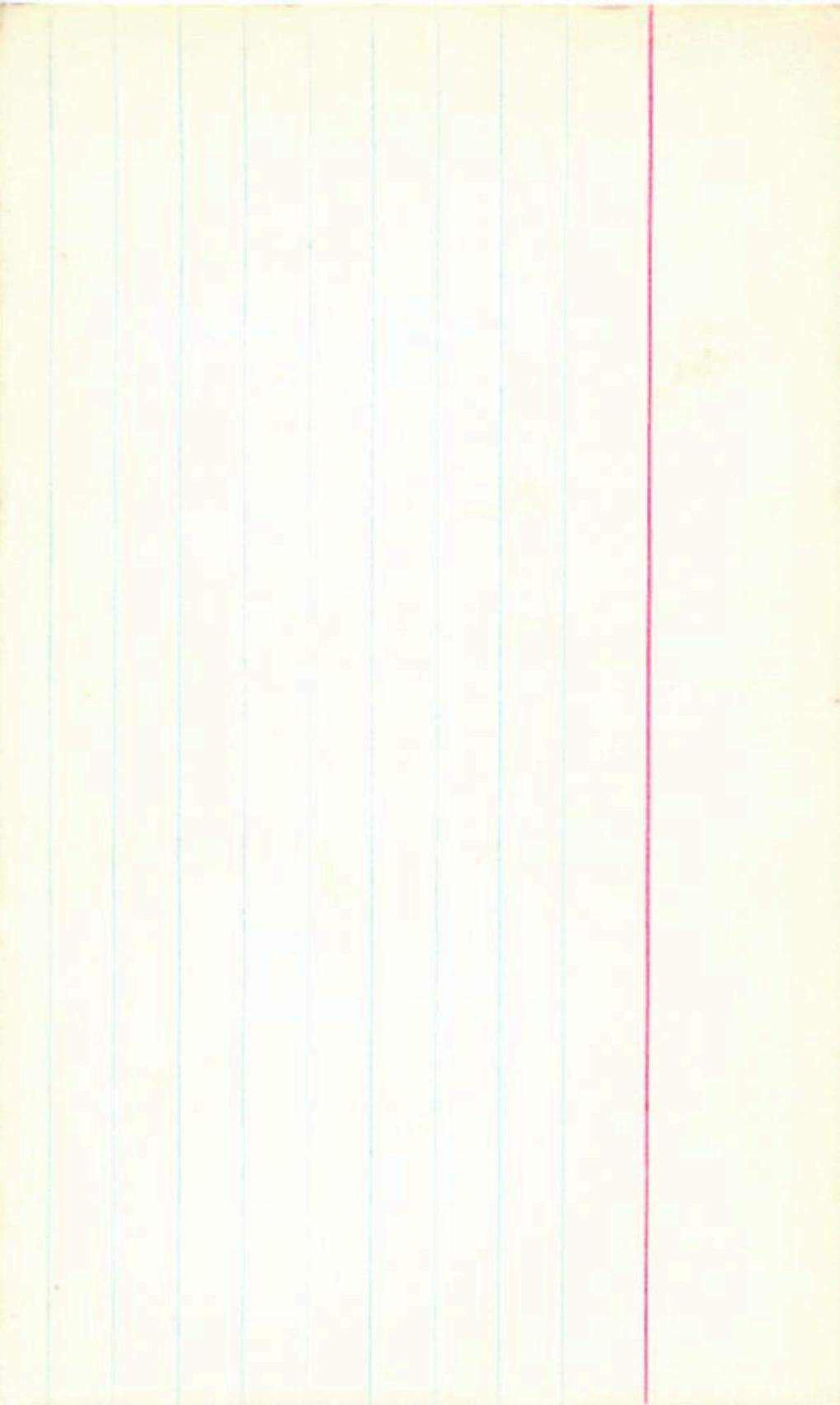
E(4055)

4056 14 20 - 85 35.5 9.21 + 45 - 55

422 - 11 - 16 24625
9.17 - 346 + 633 - 620 2.101

9.17 4421 - 070 - 103 2.579





1020 -350 4384 08 253.6 -0.4

PS 14 8 14 20 -85 83.5 521 41 -554

(9.17 -346 +633 -620 2.101 21 fm 75

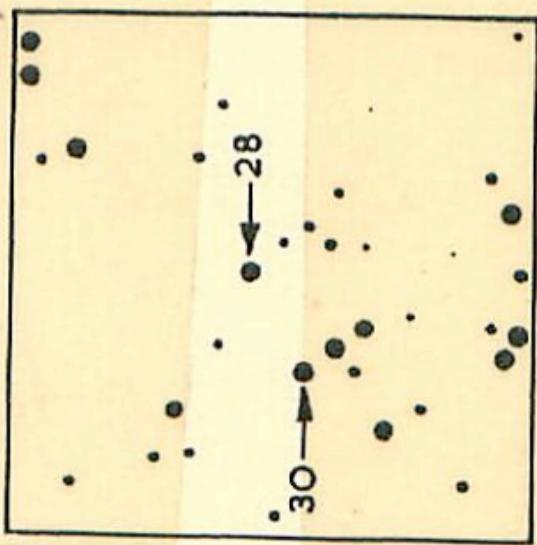
9.17 -260 +619 -875 2.052
-910

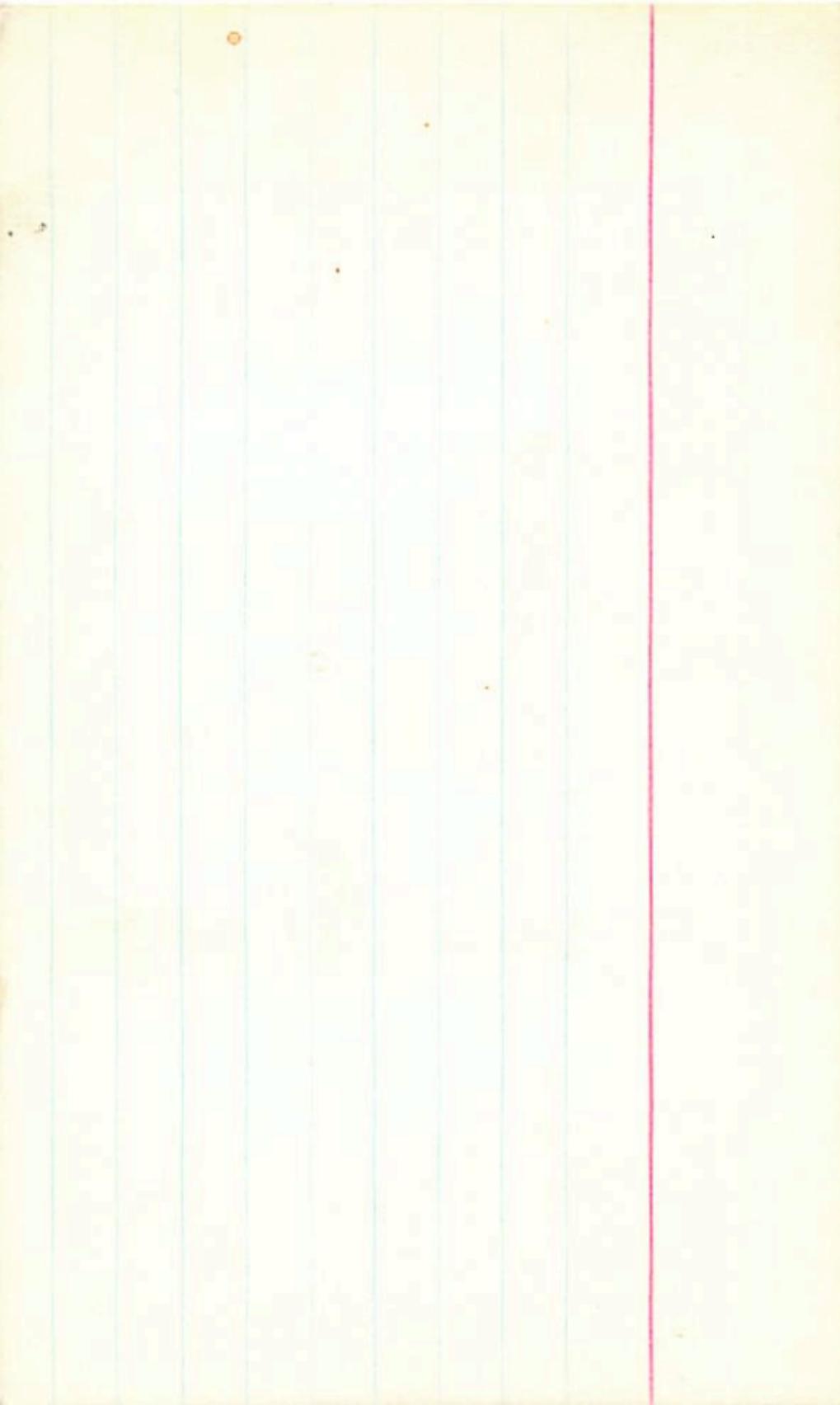
9.22 -303 +637 -628 2.105 17 fm 76

9.20 -266 629 -919 2.058 (2)

28 17 55
17 60 -36 03 10.19 + 29 -64

30 18 07 -36 04 9.17 + 32 -67





350,
39,

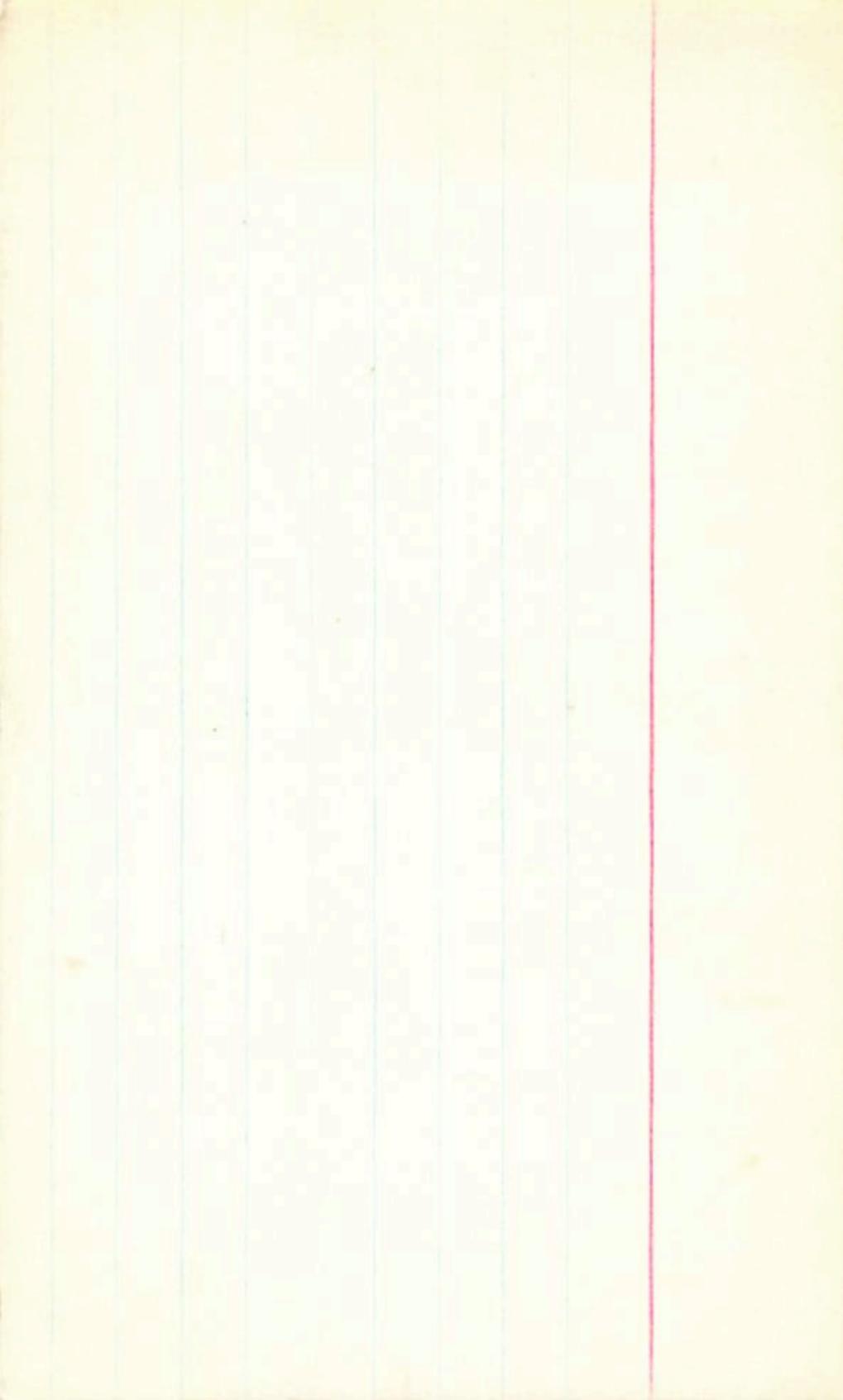
40460

58 35
58 35

✓
✓

16 7.9 KWT

4103. ✓



0000

6.21 -90 820 -304 10 666 715
6.24 -79 814 -267 11 666 716
6.19 -90 817 -367 16 666 716
6.20 -78 822 -324 17 666 716
6.20 -91 823 -264 16 666 716
6.19 -90 824 -305 20 666 716
6.19 -83 820 -330 21 666 716

7.6
7.15, 11.75

5.156

0.5
-32, 4.976

X

0.9 0.6 3.5

-32 5.0 → 10.05 + 4.15 - 4.1

26 Jan 75

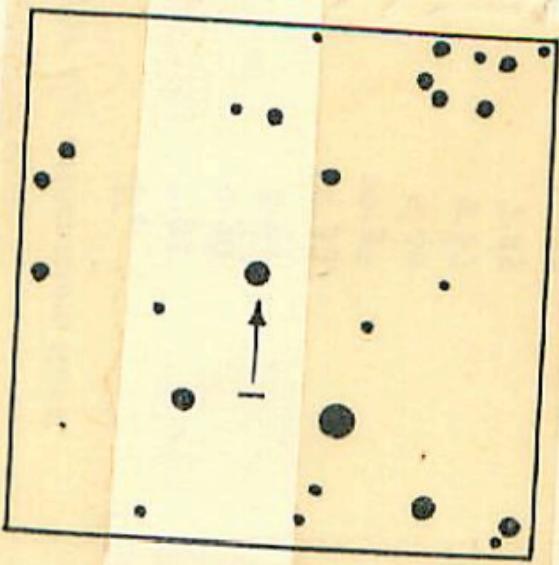
10.03 - 335 + 656 - 774 2.106

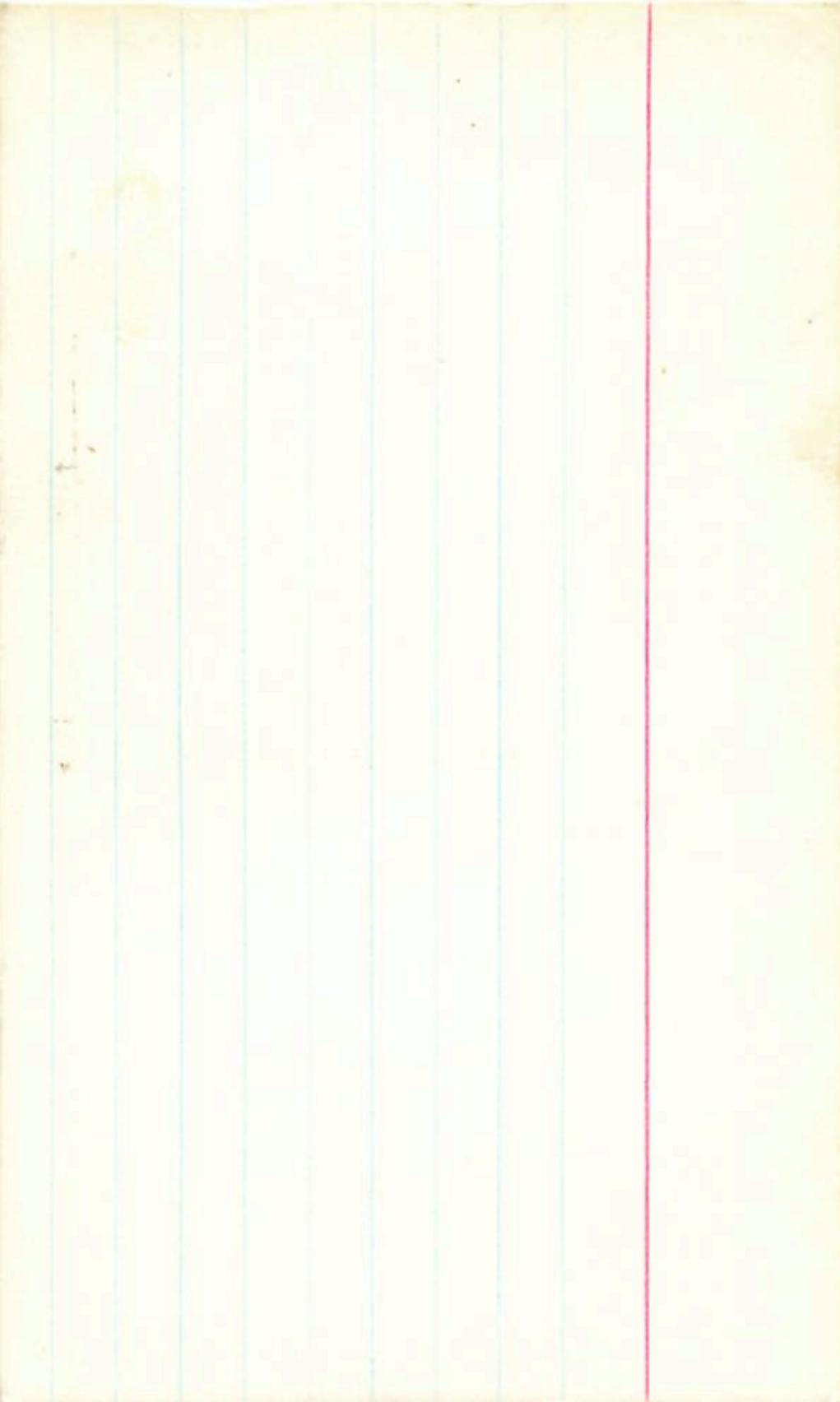
~~70.63 + 4.976 + 8.02 - 2.44~~

10.03 - 274 + 144 - 744 20.97

1001 - 305 614 - 814 2.139 24 April

10.02 - 292 654 - 752 2.118 (2)





81.72 - 36.43 = 43.91

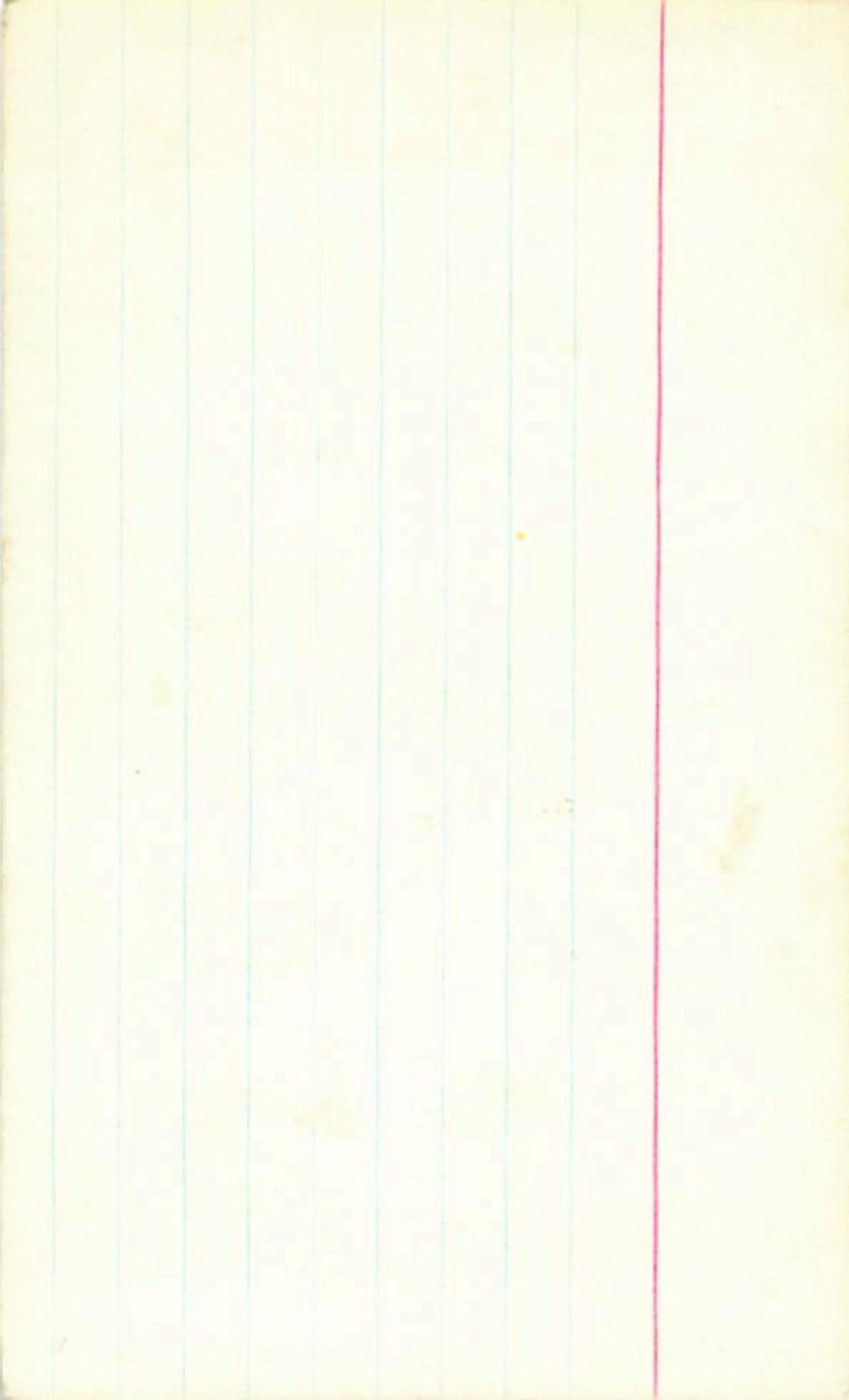
+ 0.50 + 0.10 411.00

31.03 88 14 35 - 37 02.50 9.07 + 17 - 77.91

81.72 - 36.43 = 43.91

+ 0.50 + 0.10 411.00

(9.19 - 61.9 + 73.1 80.2 - 2.115 2.115
→ 9.19 - 56.3 + 71.7 - 75.7 2.106
9.26 - 58.8 71.2 - 81.0 2.126 1.7 mon. 7.6
9.24 - 57.4 + 73.0 - 81.7 2.116 ②)



6271-6 (St 4P)

8.11.0405-06

~~8.323 8.687~~

$$\begin{array}{r} 8.66 - 624 \quad 868 + 3 \\ 8.66 - 619 \quad \underline{885} \quad + 15 \\ \hline 8.66 - 621 \quad \underline{851} \quad + 5 \end{array}$$

$$20 \quad 920 [1220]$$

$$8.66 070 130 935 28360$$

8.11.0405-06

V 830

m 1035

$$26 \quad 8.83 - 575 \quad 810 + 107 \quad 2823 \text{ year 87}$$

(+0.65 day)

$$403 \quad 120 050 \quad 1081 \quad 2523$$

7.95
7.5

3400

9.0

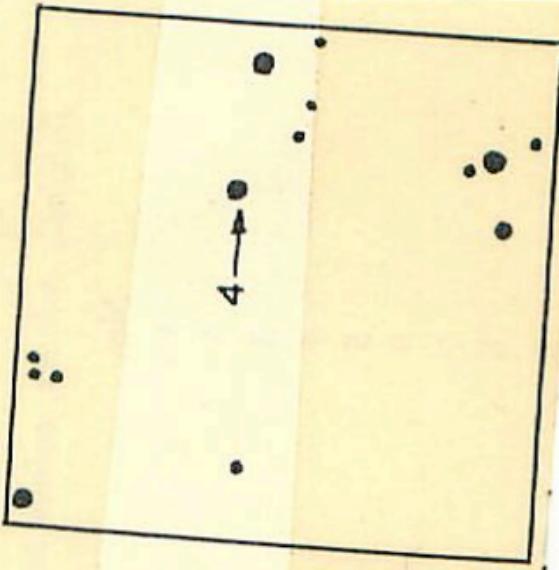
211185

202789

X X X

4 8 6 9 1 4 0 5 - 3 3 5 7. 0 5 11.11 + 09 - 4 6

$$\begin{array}{r} 11.14 - 5.23 \\ \underline{- 5.23} \quad 750 - 518 \\ 11.15 - 5.23 \quad 771 - 545 \\ \underline{- 5.23} \quad \underline{750} - \underline{524} \\ 11.16 - 5.23 \quad 757 - 530 \\ \underline{- 5.23} \quad \underline{757} - \underline{530} \\ 11.15 \end{array}$$



100% of the time

Minimization

$$\frac{94.3}{3} \quad 251.7$$

+0.1

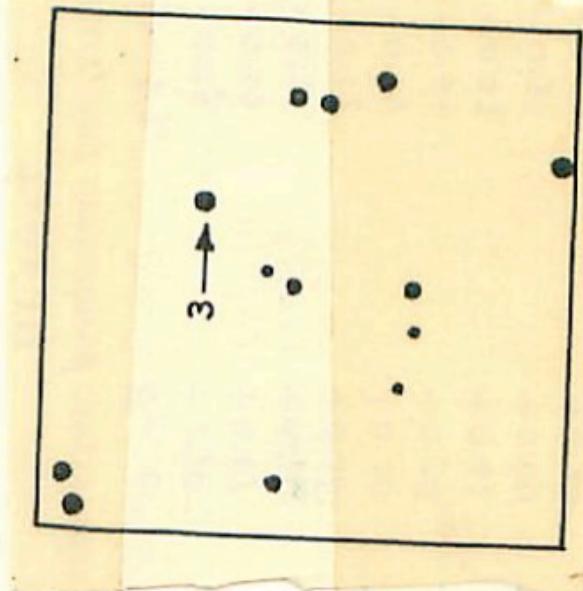
$$\frac{11.15}{8} \quad 23.08 \frac{1}{3}$$

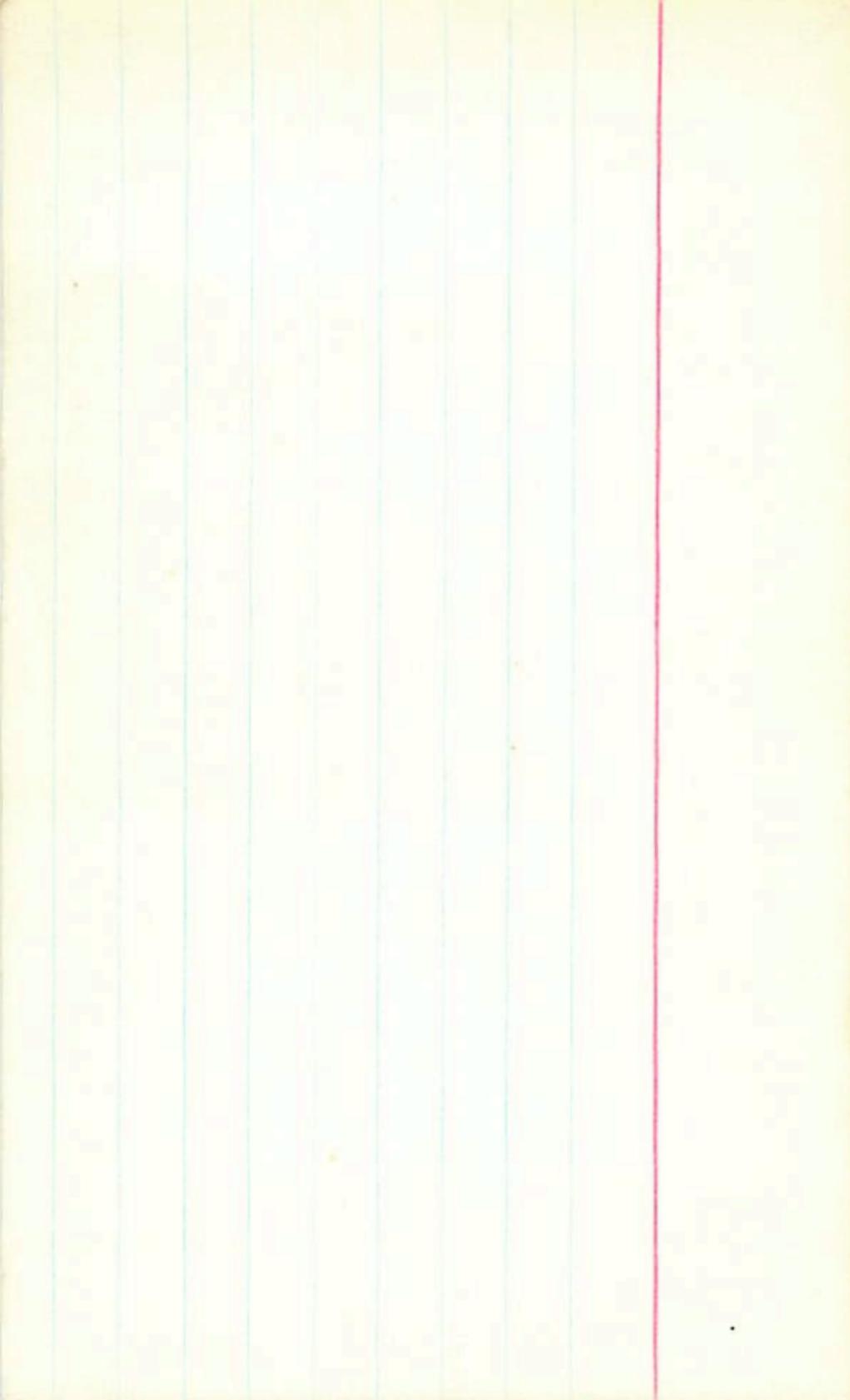
$$-33 \quad 45 \quad 11.18 + 0.45 - 0.55$$

$$11.15' - 31.3 + 62.5 + 0.54 \quad 2.012 \quad 24.62$$

$$\rightarrow 11.15' + 45.6 - 67.6 - 24.6 \quad 2.483$$

11.15' + 0.125
2.483



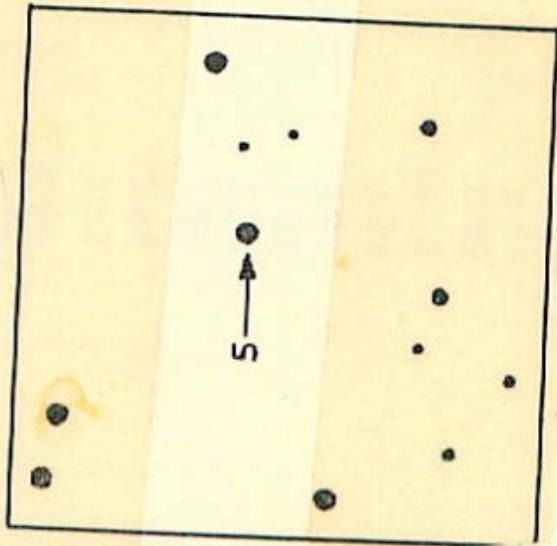


X X X

5 8 15 07

11.08 + 07 - 52

11.03 - 55.5 753 - 620 2.152 76
11.03 - 57.5 751 - 695 2.122 2.045
11.09 - 55.5 64 - 672 2.124 77
11.05 - 56.2 757 - 670 2.128 73



Plan

90436

~~850 + 2110~~

~~6101284~~

~~9 16 16 - 62~~

~~20 8.86 - 05~~

$$\begin{array}{r} 8.86 \quad 1.89 \quad 7.95 \quad 4.93 \\ 8.87 \quad 1.83 \quad 7.73 \quad 4.46 \\ 8.86 \quad 1.83 \quad 7.61 \quad 3.43 \\ 8.86 \quad 1.81 \quad 9.01 \quad 4.86 \\ \hline 8.86 \quad 6.90 \quad 7.90 \quad -4.78 \end{array}$$

(2) 2.164 152176
Q.183 162676
2.156 100016
2.160 ④

850 - 672 478 2.160 ④

~~✓~~

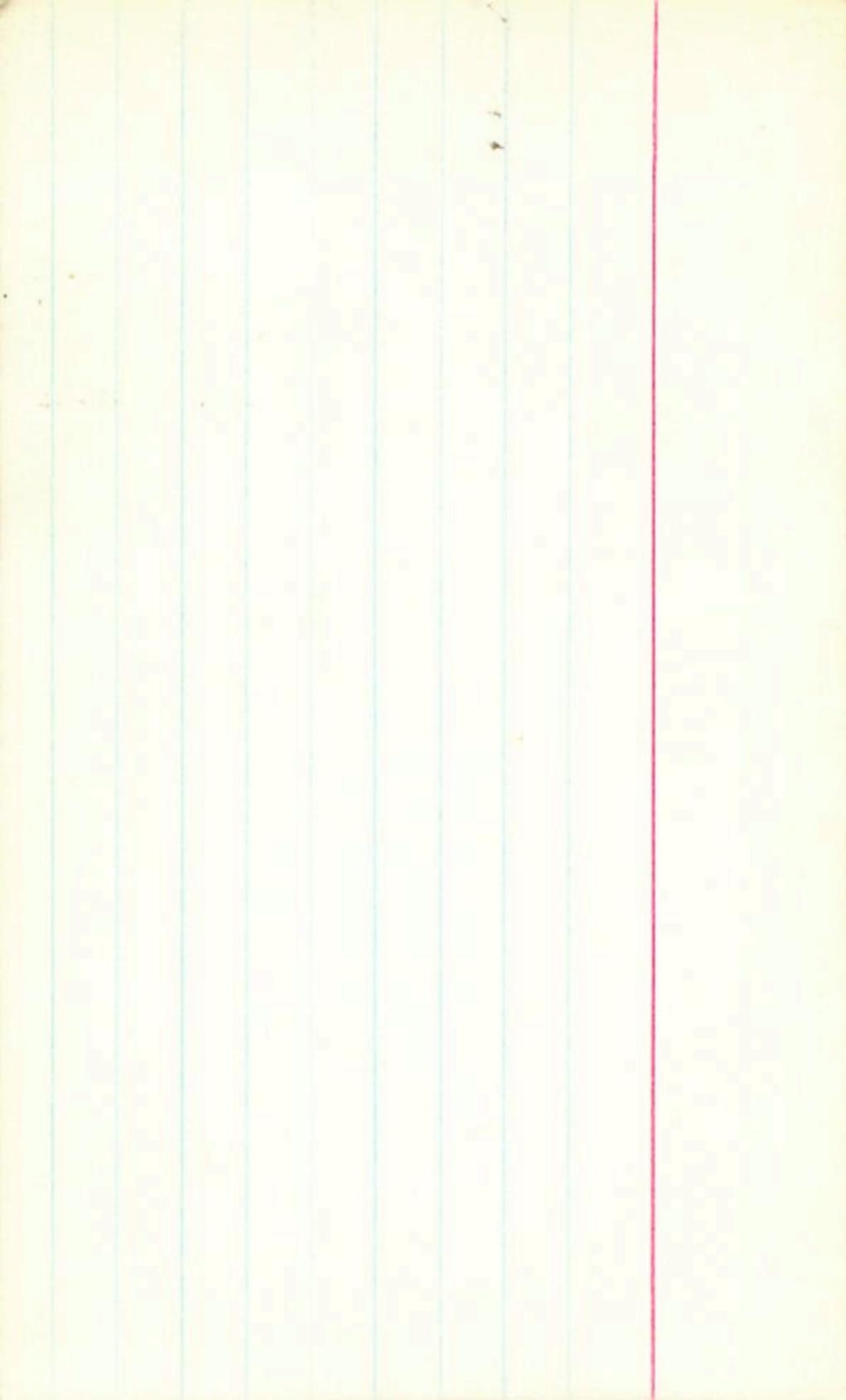
98% OB. 252.1 - 0.4

6 8 10 19 -34 21 10.63 + 14 = 60.4

5

W O .

10.68 - 535 735 - 733 2.110 24 Apr 176



135687 ~~D~~ 15 15 05 +13 33 2.07 +81

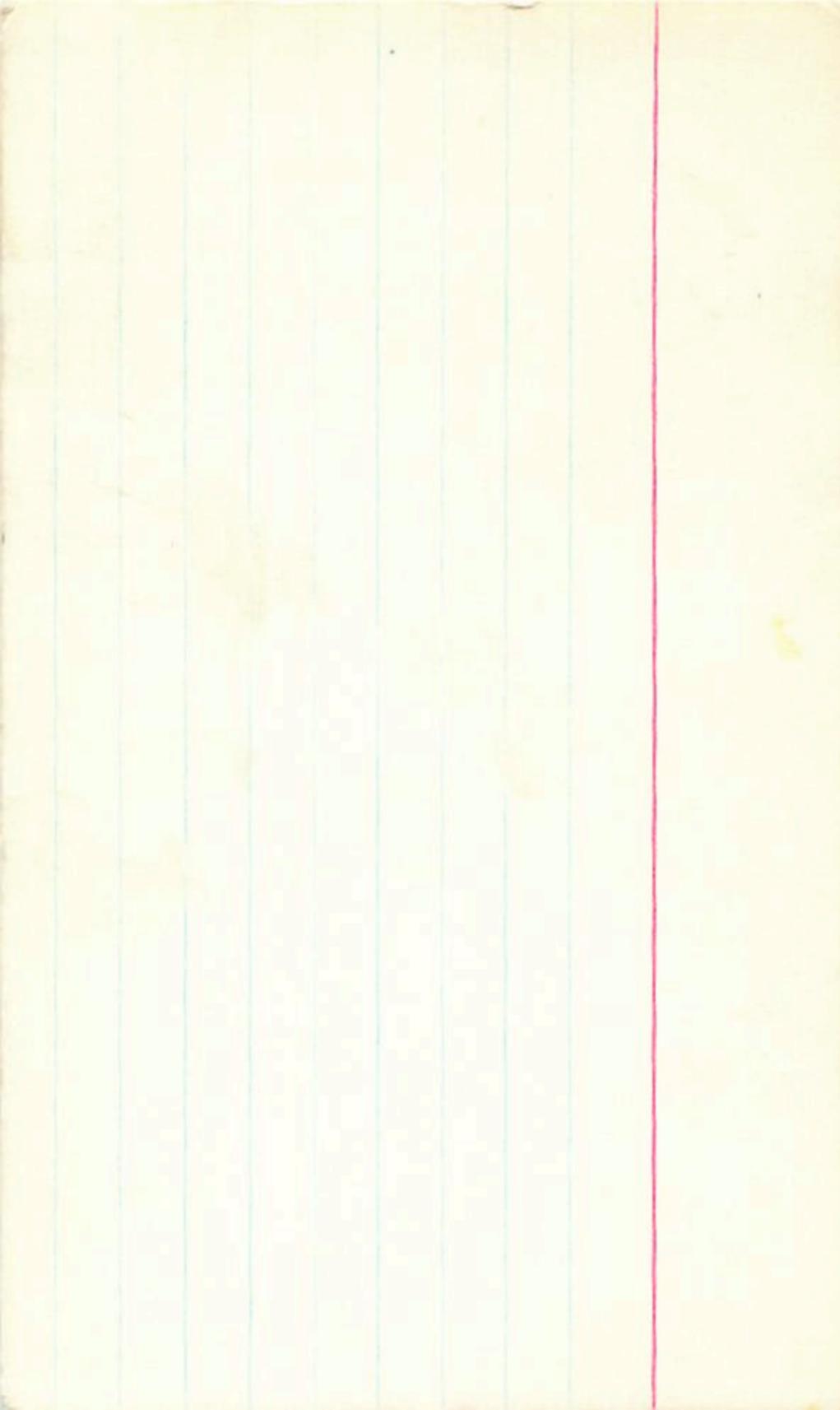
P. D. Day

X X X

15 8 14 51 -3 < 1/2 10.85 +27 -62

5. 6.

10.85 -417 656 -917
104 -416 656 -916
609 -416 656 -916
2.104 334 176
2.105 334 176
2.105 334 176
2.105 334 176
2.105 334 176



167

12 34 -34 23 11.10 +18 -15

$$\begin{array}{r} -453 +201 -766 \\ \hline 11.12 -589 +715 -782 -2.127 \\ \hline 11.04 -511 +793 -861 2.124 21.4176 \\ \hline 11.01 -419 +731 -917 2.125 22 \\ \hline \hline 11.01 -411 +739 -240 2.130 \textcircled{3} \end{array}$$

