

3656

-210167

00

43.7

-20

56

8.765

Y

-130

-40

933+0.64+0.045D

130-40 3.7

-0.479

-0.993

-0.009

9.406

0.106

0.171

-34.155

0.043

-0.622

0.000

54.954

3.700*

-0.040*

-0.130*

-56.000*

-20.000*

43.700*

0.000*

1283.456

1255
25682

4

027

+53

53

120711

-12

-8.06

6.31+0.99 +6.752A

GL 7.55
10070 -0965

5.48 +0.355 (3A)

1259 $\frac{1}{2}$ 0.14 -20 18 $\frac{1}{2}$ 122 $\frac{1}{2}$ +24e

2564 2.01 +122 (230) GC

1220 Y 5.2 459 46 68 II -1438

25877

6.28 71.14 70.52 A

CV

49 Nov

1277

25975

4

049

+37

36

121 III

-40.26

6.09 +0.535 +0.755

(3)

-1088 -1967

-14 +2.5

5.69 +0.325 1A

1280

26029

4 05.1

+17

12

9 15.5

-30.66

5 pm 4.5

+0029-0115

GC # 20

1281 4 882 +72 60 141 III -416
26076

RC

1292
26101

4 078

+68 22

100

-2356

22

1286
26311

4 07.8 +3.3 27 C105 +15.6
5.72 +1.44 +1.47 A CL

1301
2665

4 10.6 +37 50 69 III 12426

6L

1304

4 188

+43

13

28 III

-3774

26654

546 + 87

+44

R

-6248 + 1025

6-L 72.0

47 Jan 45
3170

4 11.2 49 08 965

~~374~~
1311

4.83 + 0.80 + 0.50 =

2.35^{min} 1.1

-4
18

4.51 + 0.81 45

26722

± 2.5

4 18
3 9
4

-0.00060 - 0.0380₂₀ 64+

3
4.25

- 6.6 a

end

12
-6889

-6889 - 0.40

-5.947
-0.484
-0.129
-8.150
-0.055
-0.120
-11.364
0.873
-0.079
-6.600
70.795
4.250*
-0.040*
-0.008*
8.000*
9.000*
11.200*
4.000*
1311.000*

1313

26755

4 13.0

+57

44

101

11

-38.3

G-L 73.5

+037 -033

670 SYL
4

1316 4 11.0 -44 30 150 —

26820

6.70 +1.47 +1.80 C GL

6.04 +0.595 (4)

1317

26836

4

19.3

480

42

986

-916

RL

1323

4

119

-40

30

85

✓

26507

6.36 + 1.47 (2.51) C

6.2

1327
27622

4 160 +65 61 B5 III -18.5e

5.57 +0.81 +0.47 J⁴
4.94 +0.29 2A

B-C ±2.5
-60 395' -002

564 ±2.0
-60 43 -60 33

1335
27245

4 17.4 +60 37 M10 III +28.56

S.41 +1.50 +1.81 (3)

GC ±2.0

~~4.40~~ +0.7 (3)

+0081 -107

1337
2922

7 16.8 41 41 585 124.16

BL