

Bu Run L' 09.3 +22 56

HR 2197  
~~1701247~~

6:39 +224 +248 4.63 +1.19

~~525 +1.18 +1.48~~

I Run

Table 2 of Supp. 131

B 2 +40

Bu Run 6.4 +225 +~~28~~ 6.4  
HR 2197 4.6 +1.17 10.2

TV Mem 6 08.8 + 21 53 + 17

HR2190

-001 + 002 LB

465' + 120 eggs

$\frac{495}{46} + 1.07$

46 + 1.15

E + 40  
eggs - Supp 131

TV Mem

6.55 + 2.25 ~~4.05~~ - 6.9

HR2190 46 + 1.15 10.7



+14 +2 -10.0

4000

-159	688	-698	-0132	+0065	-0067	-27	+4.8	+7.0
605	646	464	+0401	+0061	+0462	+184	+13.8	-46
-771	230	545	-0512	+0031	-6481	-192	-246	-54

W her 16 33.4 +37 27 -51 R

-607 +023 MC

$$\begin{array}{r} -6005 +011 \\ -1 +5 \\ \hline -6 +16 \end{array}$$

Bauer

-607 +016

$$\begin{array}{r} -254 893 -370 \\ 402 413 644 \\ -210 066 669 \end{array} \left| \begin{array}{r} 26084 +0677 \\ -0206 +0336 \\ +0245 +0550 \end{array} \right. \begin{array}{r} +076.1 \\ +0130 \\ +0245 \end{array}$$

+18.8  
-32.8  
-84.1

W her

8.1  
6.8 +175 9.9  
-49 +90 -20 -6 -7 -510 250  
+42°  
+500

+05

X Has  
 144205 16 01.1 +47 23 6.35 gmc -91.78

-6044 ± 12.2 +053 ± 7.5  
 -0058 +046

SRL(100)

21577 8875 19063 +47 22 3546 1910.4  
 5228 192

(7.5)

9067 -069 +0600BL -2.10  
 33. 36

1928 1928 +135 -80 -21  
 +33 -6 +13

Spud

23.65  
 45.275  
 8.925

(28.0)

43.2  
 9.80  
 33.40

2011 →

7.8  
 6.65

34.16  
 9.2

(16.01)  
 16.01

1807  
 904

1940.42

954  
 20  
 904 -16.3 3.45 +1.20

33. 9  
 35.1  
 -1.2  
 34.9

46.62  
 34.3

MW 6.32 +1.39 +0.80

34.44  
 +1.10

(23.9)

X 1hr 16 01.1 +47 23

592

X 1hr	8.85	+1.55	+1.05	-4.8	+103	-83	-26	-69	-91.7	95±
HD 14205	3.60	+1.70		6.8	+38	-10	+18	+59		480
										$\Sigma = +03$

280

-91.7

-069 + 060 LB  
-069 + 059

275 910 -180

651 896 647

646 - 125 741

+1226

-2129 +1107

+2158 -0350

+2545

+1022 -235

+1808 +416

+3771 +86.7

-1022 -235

+1808 +416

+103

-93

-26

+16.5

-59.3

-67.9



+2303090

RS New 17 19.4 +22 58 -41 R

Banner

-0010 ± 3.7	-005 ± 4.2
0	+4
-0010	-001
+014	-001

-025	-005	MLC
+1	-1	
-024	-006	

-086 786 -613	+0057 -0037	+0020	+26	+25.1
563 546 620	-0374 -0026	-0400	-42	-28.4
-822 292 489	+0545 -0014	+0531	+2	-20.0

E = +106

2.65	+1.6	+1.2	-2.9	+26	-42	+2	-14	-41.0	220 <sup>d</sup>
6.1	+1.10	8.15	0	-4	+5	-1			+29.5

85 Wer 16 30.5 76 58 SM 22 -Y 6.0

$$\begin{array}{r} 0 \\ +1 \\ \hline \text{wer} -003 \end{array}$$

$$\begin{array}{r} -0007 -002 \\ 0 + 8 \\ \hline \text{Pardone} \end{array}$$

$$\begin{array}{r} -0007 \\ \hline +006 \end{array}$$

$$-010$$

$$\begin{array}{r} -005 \\ \hline +002 \end{array}$$

0.0000

16.0000

30.5000

6.0000

58.0000

-0.0050

0.0020

10.9500

1548.817

-46.000

0.012

-0.768

53.768

-0.008

0.317

-27.178

0.021

0.557

7.024

SX 1400 14 05.3 + 25 02

Water Cor 2 in 342

pm

pm

R-1 = +700. Min

1150 M.

SX 1400 7.8 +1.4 +1.3 -3.4 -127 -172 +46 -18 +200 103 +44  
7.10 to 6.00 1034 -10 -16 +3 -36 (33 up +46)  
E 2104

~~12503034~~  
 8.8  
~~256~~  
 Ruller 14 08.2 125 12 1.90 9422

SX 1er 12503031  
 16 05.3 125 02  
 V.8 V +20.06

~~4022-0304~~  
~~5015-0304~~  
 20.91 1917.3  
 -00175.0  
 -03844.4  
 -048  
 +25 2 28.17 19.5.2

sur  
 Pender ~~12503031~~  
 035  
 916  
 945  
 -0022  
 -043  
 +7  
 134  
 29.53

Ap. 5. 12 941.5  
 20.92  
 17.1  
 19.1  
 28.9 1930.3  
 -32  
 28.58  
 29.35

1026  
 916  
 938  
 102  
 29.12  
 29.5  
 28.58  
 29.35

361 775 518 20.933  
 1.44 608 454 942  
 1.70 171 722  
 10300 -1322 -1044  
 -0384 -1037 -1591  
 +0572 -0392 +0800  
 29.12  
 29.5  
 28.58  
 29.35  
 1928.41  
 -88 48  
 -202-193  
 +64 28  
 44.4  
 1000 Pa.

-361 775 -518

+649 608 457

-670 171 722

-0.027 -0.030

+175

L & Hon 16 05.5 123 37

CHW039

~~CHW039~~

-227

411  
165  
242  
265  
709  
164  
130

LG1br 5.7 H159 H156 -395 +8 -40 -4 -23 -27 ?  
H16024 4.25 H138 69 -2 12 +6 -17 H1411 4450

(103)  
15

-0017 -0020  
20.281 1913.8 -0012 -0024 22.50 1914.46

-0016 -0022  
+5  
-023 -0017 A

30.268  
+7  
21.56 1933.5  
+01

-0.351 766 -589 +0383 -0617 -0234 -56 -7-78 +133  
.646 614 452 -0704 -0448 ~1199 -288 -40 -11.1  
-678 190 710 +0739 -0150 +0586 +14.0 -9 -17.5



D.P. Men

17 55.4

415 22

163550

415 6.702

555-

D.P. Men

6.05 41.60 41.56 27.2 -42 +9 -13 41 4130 ?

415 6.702

4.30 41.50

7.15 -14 -1 -7 -32 415 428

405

II-III (15)

OP 72.2 +29.2

122782 75.4 +29.8 640 -15-37 AP

164429 72.4 +27.8 640 -07 -26 B9 104 6.00

167466 69.4 +24.0 660 -12 -50 B8 +05 6.15

+00162.5 -08722.4

22.282 1922.58

7000

55

22.49

1916.36

032

7011

11 Nov

12.5  
20.0  
5.5

16.0  
20.0

17 12.4 +14 27

17 Nov 6466

R 1<sup>2</sup> R-I

Johnson 3.06 + 1.45 + 1.01 1.34 + 1.66

1.55

+0.5

600-111 M<sub>1</sub> = 10.5

sp

21 Nov 30 + 1.5 -

24775

+34 -11 -10 -10 -349 .

?

1 Nov 1.3 + 1.65

4.55

+12 +9 +6 +34 M5E

1280

100

2 H<sub>2</sub>

B Sp. O. P<sub>2</sub>

156014

17 12.4 +14 27

3.5 gm<sup>5</sup> -33.1g

23277

-0008<sup>87</sup> +033<sup>56</sup> N30

5.4 dF<sup>8</sup> -36.7g

9944

-0007<sup>50</sup> 6 +035<sup>±0.60</sup> C → N30

34.9

A0510418

97

G 12w 16 27.0 442 00  
F 76146

475 +1.55 +125 2.7 +1.75 595

G 12w 4.75 +1.55 +1.25 -5.0 -1.0 +1.5 -1.4 6.25 13.4 707  
F 76146 2.7 +1.75 6.05 -6 +8 -1.0 -5 16.71 +442  
2.37  
2.24  
0.13  
22.  
402

30 Hz

~~Graph~~

148783

16

27.0

+41

59

HR 6116

22172  
9485

4.2 - 5.4

1.6:

+0025<sup>37</sup>

-008<sup>19</sup>

N30

+0020<sup>±1.9</sup> -003<sup>±1.5</sup> GC N30

9 M6 +3.4 a

+028 -008

~~+053 -041 GC~~

+025 -008 GC

+028 -008 N30

+027 -008

669 743

1001

1002

544a

7.2-13.0 26.0 d

-0006 & 4.7 +011 & 4.2  
+0000 / ✓ +0009

+LL.5.0m.

76011

8 51.0

+3 16

7.22

SMY +748

12278

57.545

1911.04

-0001 +012

30.00 1905.64

5850

57.512

1846.3

+3 15  
-0006 +010

30.35 1892.2

↓ B

544

57.527

-0002 +012  
-003

29.78

29.91 1935.4

-0006 +012

21  
548

-007 +003 MC

30.10

29.91 1935.4

2003

+1  
-006 +013  
-010 +010 for →  
-002 +011 Num

+39

-439 452 623

+0091 +0257

+0218 216.3 HL2

+461

-059 778 -625

+0008 +0442

+0450 +210 -25

-462

767 436 471

-0109 +0218

+0139 +6.5 117

+102



S Rayer 8 51.0 73 16

Bonus

S Rayer 79 41.55 +1.20 -29 +62-25 +17 = 3 +74.0 2.56 +05  
6.3 +1.10 9.35 +3 +4 +1 +12 +38.0

5850.000\*

8.000\*

51.000\*

3.000\*

16.000\*

-0.006\*

0.012\*

8.350\*

467.735

74.000

0.044

0.622

66.504

0.046

-0.622

-24.470

0.003

0.476

36.595

Mayer

10 35.4

-10 07

2.0-9.5

(M2/C3)

Number

used

HR 4163

2438044

5.31 + 3.22 - 3.53 + 0.91

920551+D

8166

4.97 + 2.28 - 3.32 + 0.96

FL 14611

8389

4.70 + 2.50 - 3.40 + 0.92

8450

4.93 + 2.72 - 3.49 + 0.95

NW 6632

8785

4.85 + 2.66 - 3.44 + 1.00

4.

(N3p(C5))

Y Rupa 9 48.8 - 22 47 8.3 - 12.0  
303d

+3.06

+0031-005 LB  
+ 1 0

+0436-005d

ms-II

T for

3

5-9.3

-50

50

7.2-13.7

via

217.2<sup>8</sup>

NO

P=+50

SL Leo NY Leo  
 94705 10 53.4 +6 27 -0.12 6.0 gms -12.88  
 -0015 +2.5 -013 +1.6

15032

6772 25.739 14013 +6 27 9.18 1896.7

$$\begin{array}{r} 073 \\ \underline{.812} \end{array}$$

$$\begin{array}{r} 25.754 \\ \underline{20} \\ 774 \end{array}$$

84

(32.6)

$$\begin{array}{r} 9.44 \\ \underline{3} \\ 1533.9 \end{array}$$

$$\begin{array}{r} 9.47 \\ \underline{3} \end{array}$$

$$\begin{array}{r} 68.77 \\ \underline{59.30} \\ 9.47 \end{array}$$

$$\begin{array}{r} 6.183 \\ \underline{339} \end{array}$$

$$\begin{array}{r} 7.823 \\ \underline{17.94} \\ 25.763 \end{array}$$

$$\begin{array}{r} 761 \\ \underline{81} \\ 051 \end{array}$$

$$\begin{array}{r} 25.763 \\ \underline{452} \\ 25.311 \end{array}$$

$$\begin{array}{r} 461 \\ \underline{+9} \\ 470 \end{array}$$

$$\begin{array}{r} 9.44 \\ \underline{9.40} \\ 0.04 \end{array}$$

$$\begin{array}{r} 9.43 \\ \underline{-44} \end{array}$$

(37.2)

$$\begin{array}{r} 9.07 \\ \underline{+27} \\ 9.44 \end{array}$$

$$\begin{array}{r} 25.725 \\ \underline{+27} \\ 25.752 \end{array}$$

$$\begin{array}{r} 9.21 \\ \underline{+14} \\ 9.35 \end{array}$$

$$1940.82$$

375 172  
337 215  
229  
141  
12  
10 534 + 6 27

HR 4267

+03

VY Leo 5.75 hrs +1.25 -5.0 +14 -6 -25 22 -12.8 ?  
HR 4267 3.85 +176 7.2 +6 -5 -5 -10 MS III +550

you are

—



10915

+0037

+004 -0355  
50918

R Sup

4 57.3 -14 5-3

NGR 432.47

1+R1607

15 120 below

u.s

7022 7022c

CG 6043

19.256 1899.6

+0015-5.5 -0008

47.42 1895.8

70004 7015 G<sub>2</sub>

+001+024

11.357  
5.263  
1902.20 475

17.27 1934.04  
47.87 1934.04  
17.27 1934.04

300 / 1056

170 689 704

+0008 +0585  
10783

10630 4816

+22.8

-596 641 -482

-0028 +0729  
10484 1130

10484 1130

-15.6

744 336 -520

+0039 +0387  
10136 120

10136 120

-16.8

+0791

+41.4

+37

+0707

-24

-3

+0414

-3

$963 \quad 270 \quad -257 \quad 846 \quad +022 \quad +022 \quad +324 \quad -006 \quad -8 \quad 088$   
004 015 -004

$-021 \quad 006 \quad 002 \quad -090 \quad 057 \quad +313 \quad +8 \quad +30$

$-004 \quad 007 \quad 001 \quad -014 \quad 024$   
 $-10 \quad +41 \quad +12 \quad 005$

$$\boxed{+40 \quad -13 \quad +8}$$

$+0001 \quad +024 \rightarrow +3 \quad +38 \quad +15 \quad 003$   
 $+034$   
 $+0015 \quad +022$

$5 \quad -102 \quad -159 \quad 163404$   
 $19756 \quad 1894.6$   
 $47.42 \quad 888.8$   
 $-5 \quad +35 \quad +6$   
 $007$

$$\boxed{+36 \quad -14 \quad +1}$$

$56 \quad 51 \quad 55.6 \quad 1890.88$   
 $11.387$   
 $46.87 \quad 1934.04$   
 $17.72$   
 $47.15$   
 $+60$   
 $49.75$   
 $+40$   
 $49.35$   
 $19.645$   
 $-036$   
 $1.19$

$$\boxed{+25 \quad -14 \quad +4}$$

$19.645$   
 $+20$   
 $19.845$   
 $28 \quad 2332$   
 $20 \quad 344$

+6015 ± 5.5    +022 ± 5.8  
 -8    +016  
 31996    4    57.3    -14    53    5.5 Van    Nice    +32.48

2957

u<sup>24</sup>  
896

+0003 +017

→

477  
17

6093  
Rings

19.756    1899.6    -14    5-2    47.42    1898.5

-076  
+680

-1.13  
48.55

378  
314  
u<sup>24</sup>  
805

193204

11.357  
 8.2632  
19.6202  
 634  
 +220  
654  
 -026

44.87  
 17.72  
47.15  
 -1.20  
48.35  
 +35  
48.00  
 +.55

(M62)

4 52.3 -14 53 5.5-10.5 <sup>of</sup> <sub>of</sub> in

RR Stop

432.5

HR11407

Standard

+3246

Now

-150915

HS031556

2439587.6 709+784 -

+0.000 / +0.024 ↓

GL6053

41.6 7.81 4.75 -

53.5 253 4.84

W2457

61.5 763 4.86

65.5 765 4.96

bins

SL # 136458  
 20639  
 8881

-1544084  
 15 19.5

-0097 ± 12.2 +007 ± 11.3 +294.00  
 -20 13 9.78 9112.2<sup>3u</sup>

31.180 15035  
 172  
 352

-20 12 32.66 1502.1  
 -34  
 33.00

-0036 +11  
 500

-514	+205	-539	+123	2	+0107	+1339	+67.0	-158.5	-91.5
+667	+705	+628	-1598	+0367		-1231	-61.6	-199.3	-2609
-539	-235	+502	+1291	-0122		+1169	+58.4	+147.6	+206.0

R hyn

2440237

32605

378.86

L 57.2 +55 24 S34-5.6.6

243

53-

R R-I

223.7	8.20	6.32	+116	9180	6.07	+142.06
236.7	8.05	6.17	+112	9203	6.73	+186
241.7	8.03	6.21	+116	9216	7.76	+236
<del>260.6</del>	<del>8.48</del>	<del>6.51</del>	<del>+132</del>	1137		
				4003		
				287		
267.6	8.38	6.30	+132			
285.8	8.58	6.72	+153			
410.8	9.27	6.34	+124			-150
6314	8.34	6.24	+128			
657.8	8.55	6.64	+144			
675.7	9.71	7.15	+173			

S 3.9

448

Cont. Torino Obs. No. 41 1967

$\rho = +20$

Residual

-0.021 -0.009

McLomax

-0.023 -0.010

-0.022 -0.010

696

-281	-409	868	+0293	+0194	0487
-366	882	297	+0382	-0418	-0036
889	232	398	-0925	-0110	-1035

+17.4  
+5.9  
+8.0

14

13

10

6.05

597

1452

43

426

587

141

42