

2337

45461

6 22.7 - 63 40 M1 -

6.27 + 1.60 + 2.01 ①

66

5.34 + 0.895 ②

4.55 444

47 Ann

2338

6

26.3

446

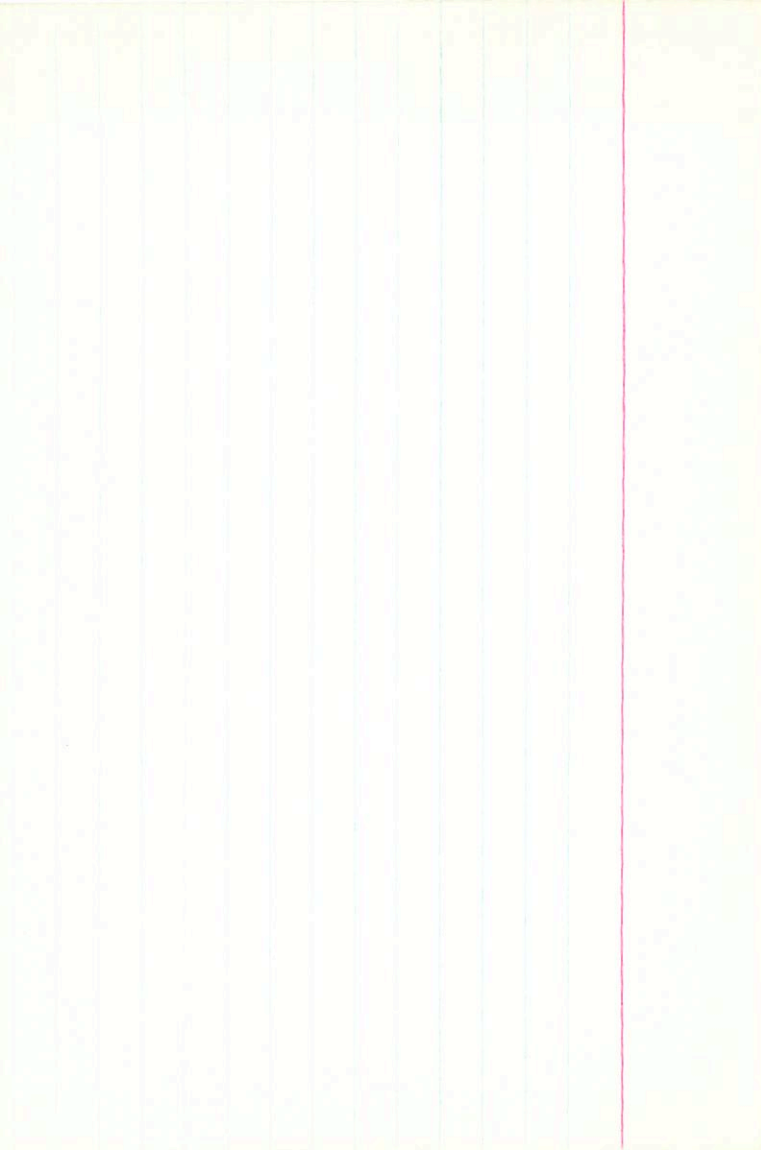
43 g 104

d

-47.3 f

45466

60



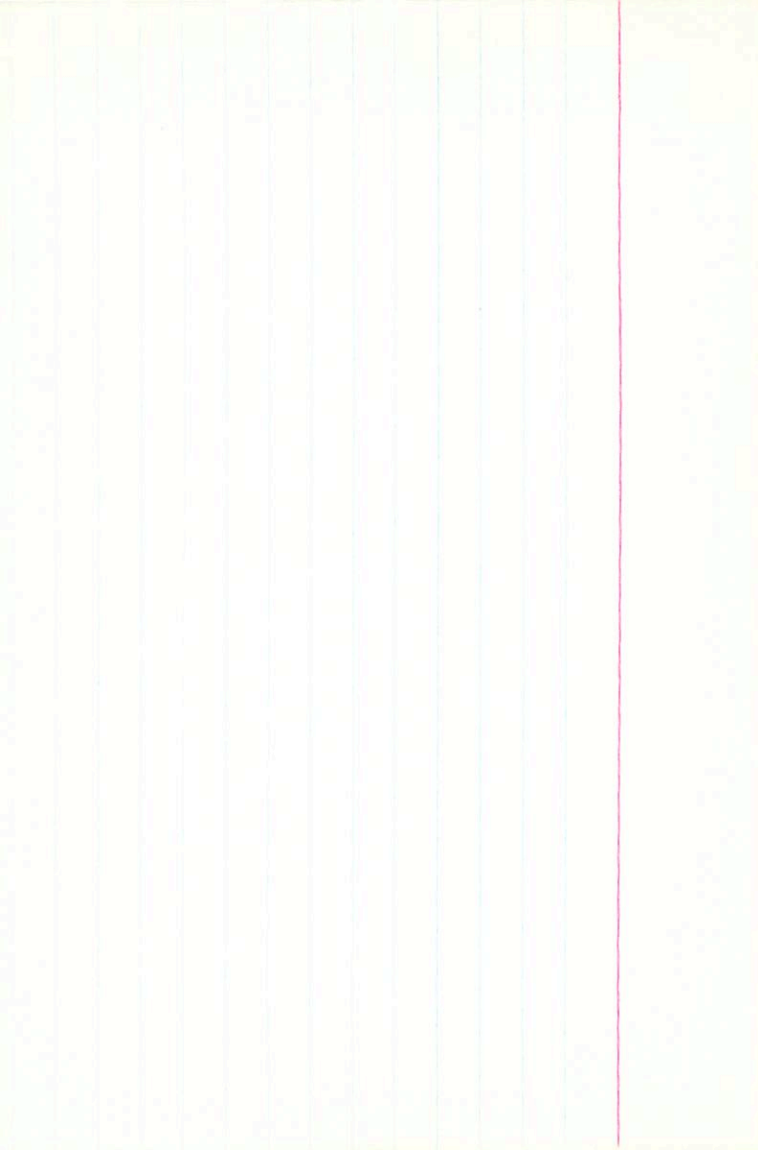
2340 4 25.6 +14 20 25 +40.86

45506

6.24 + 0.885 + 0.55 (2)

5.85 + 0.82 (4)

new position



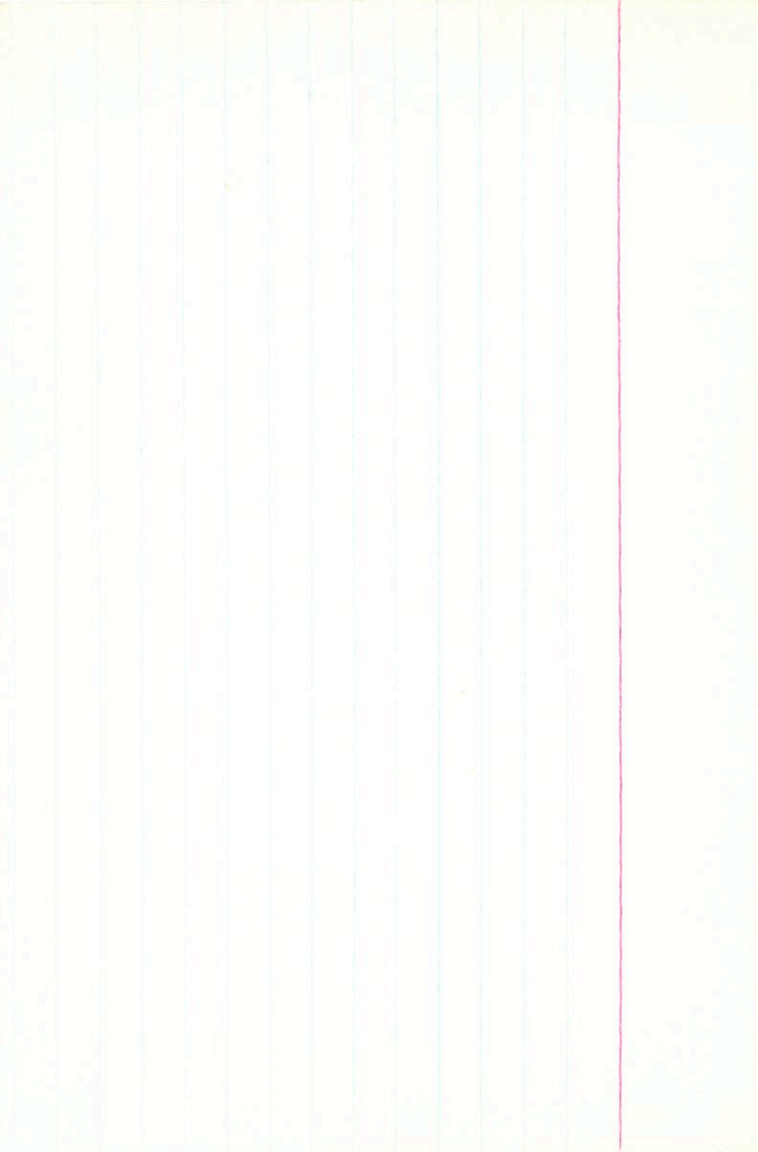
2342 6 25.6 410 21 100 -20.36

45512

$$616 + 118 + 1.14 \textcircled{1}$$

$$564 + 0.395 \textcircled{2}$$

OL



4.37 414

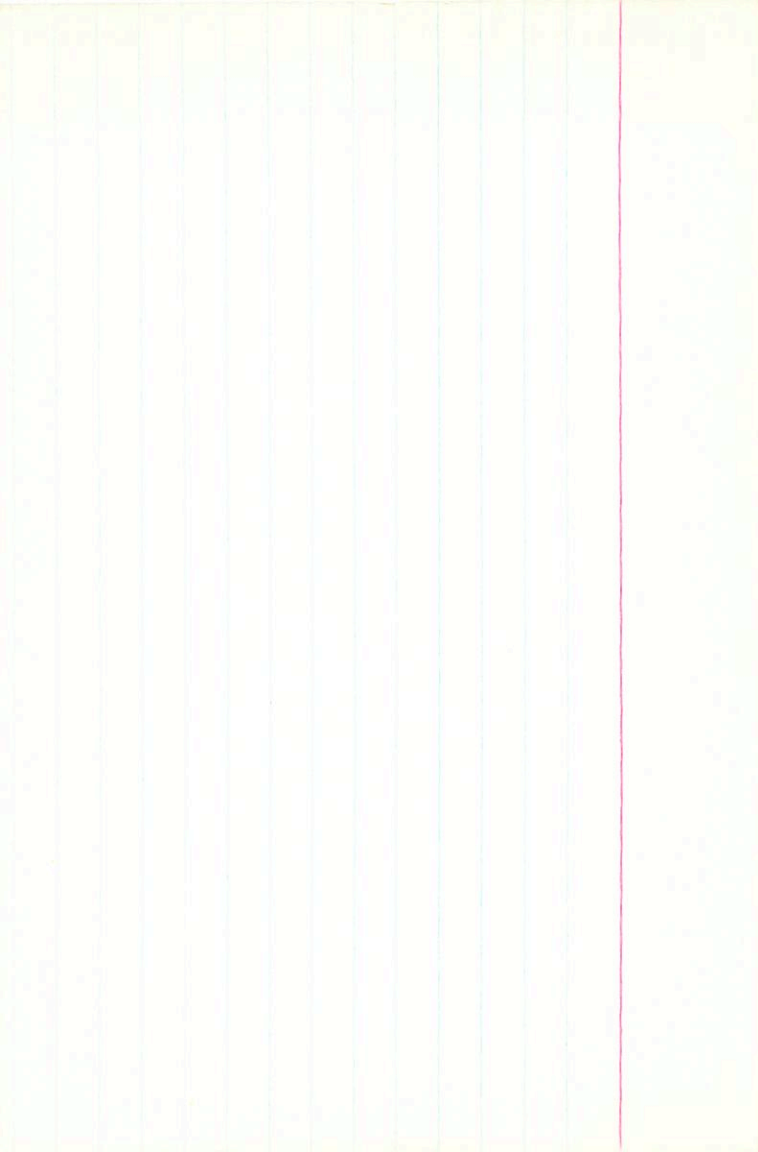
2352 6 23.1 -6.9 58 MS +15.7 f

45669

66 ± 3.0

5.55 + 1.51 + 1.82 C + 00415 + 0235

476 + 0.625 (2)



2355

6

266

+2

41

m1

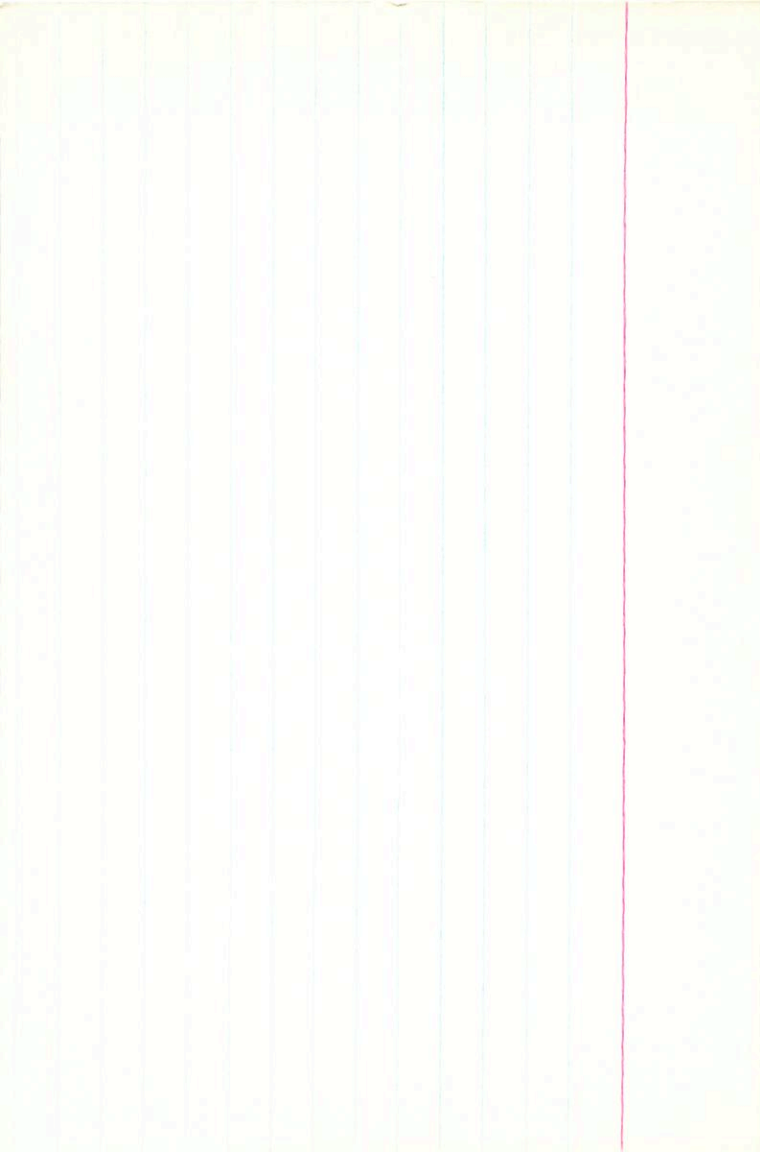
+9.28

45224

6.16 + 1.54 + 1.83 C

5.08 + 0.815 (2)

CC



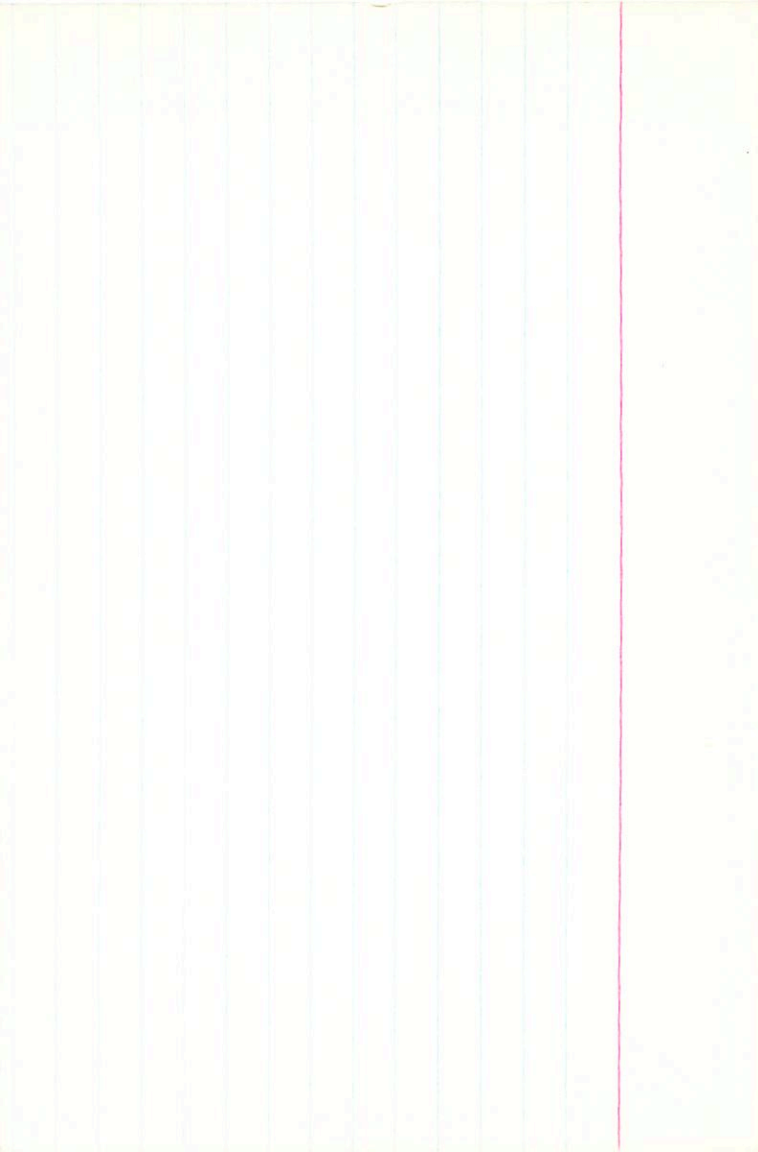
2359 6 26.4 -17 26 65 —

45765

5.76 + 1.12(2.15)C FC

5.75 + 1.15 + 0.40

5.20 + 0.405 (2)



2363

6 32.7

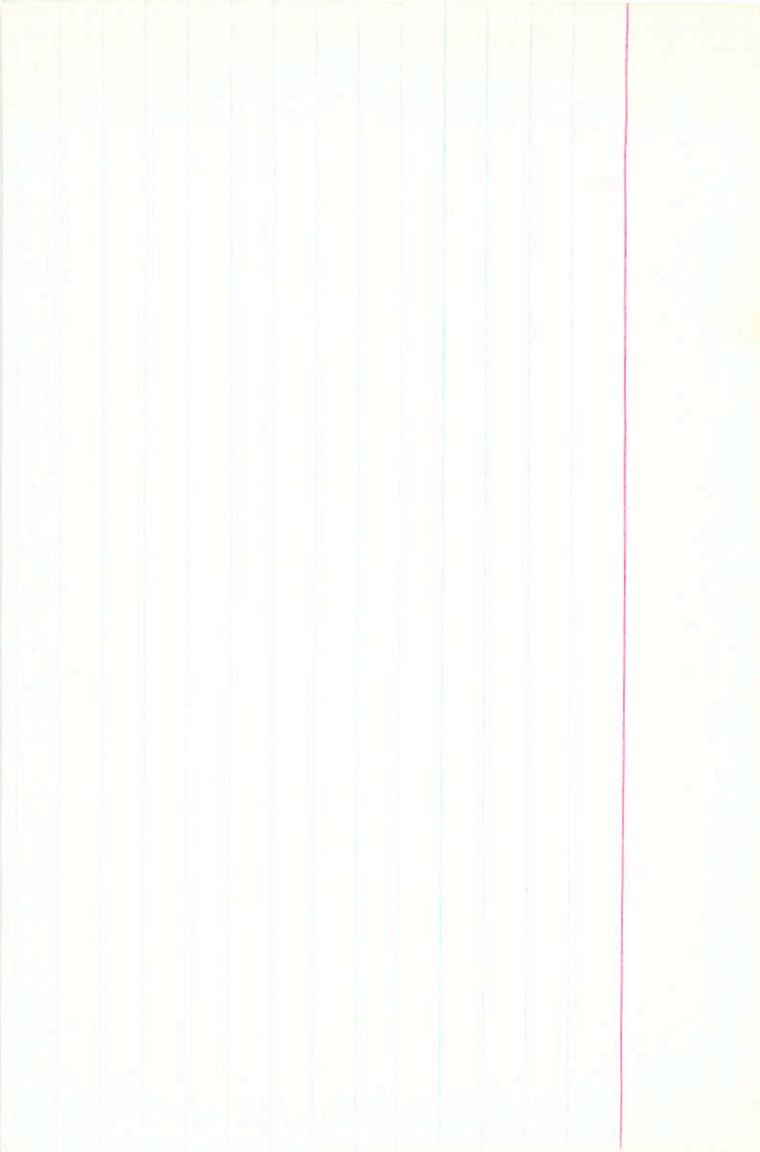
+78 02

g 155

-14.34

45866

66



2366

6

28.3

+16

59

122 111

+26.96

45951

6.18 + 1.15 + 1.03 (2)

564 ±7.0

6.17 + 1.14 + 1.05 (1)

+0001-0514

5^m 9^h
11^m 42^s

6.18 + 1.145 + 1.04 (3)

5.68 - 10.38 (2)

ⓐ 10.40 + 0.77 + 0.33 (3) 120 5

ⓑ 11.41 + 1.24 + 0.40 (3) -

Handwritten text in a vertical column on the right side of the page, possibly bleed-through from the reverse side. The text is illegible due to blurriness and orientation.

2367

6 27.8

-10 03 100

—

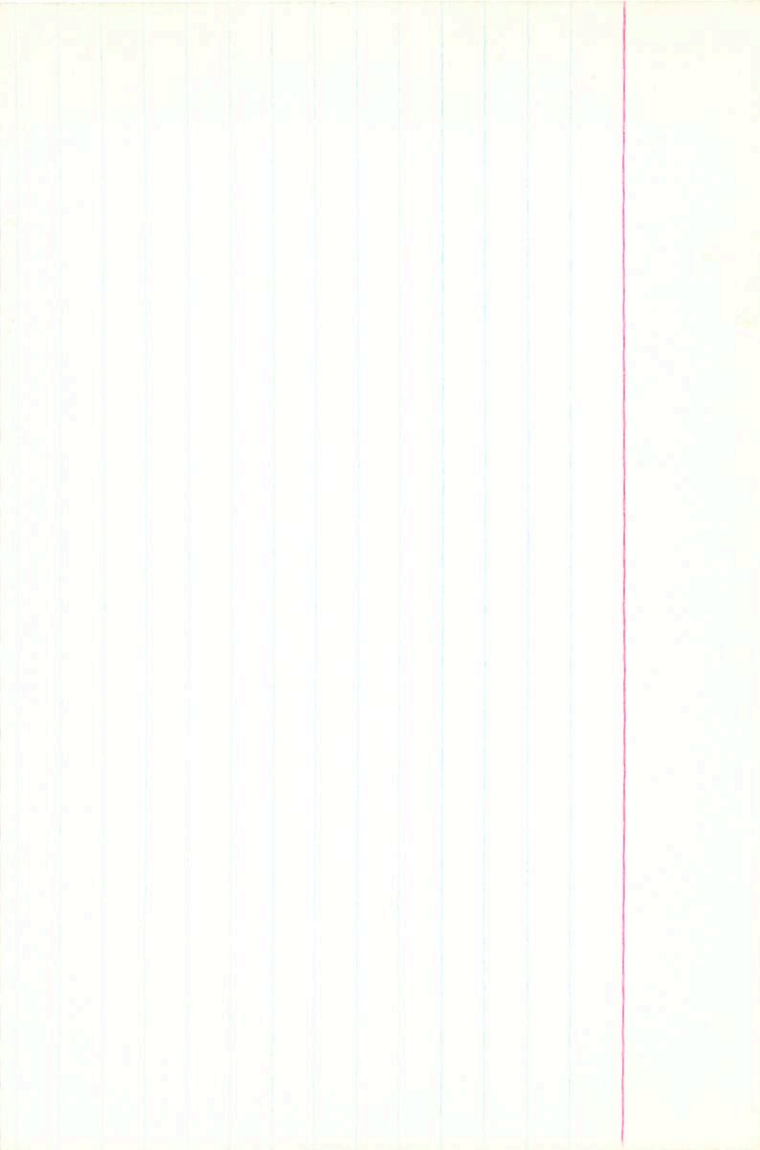
45976

5.92 + 1.38 (2.30) C

5.50 + 1.40 + 1.36 ①

5.18 + 0.52 ②

C-C



23169

6 26.3 -57 55 100 +12.76

45984

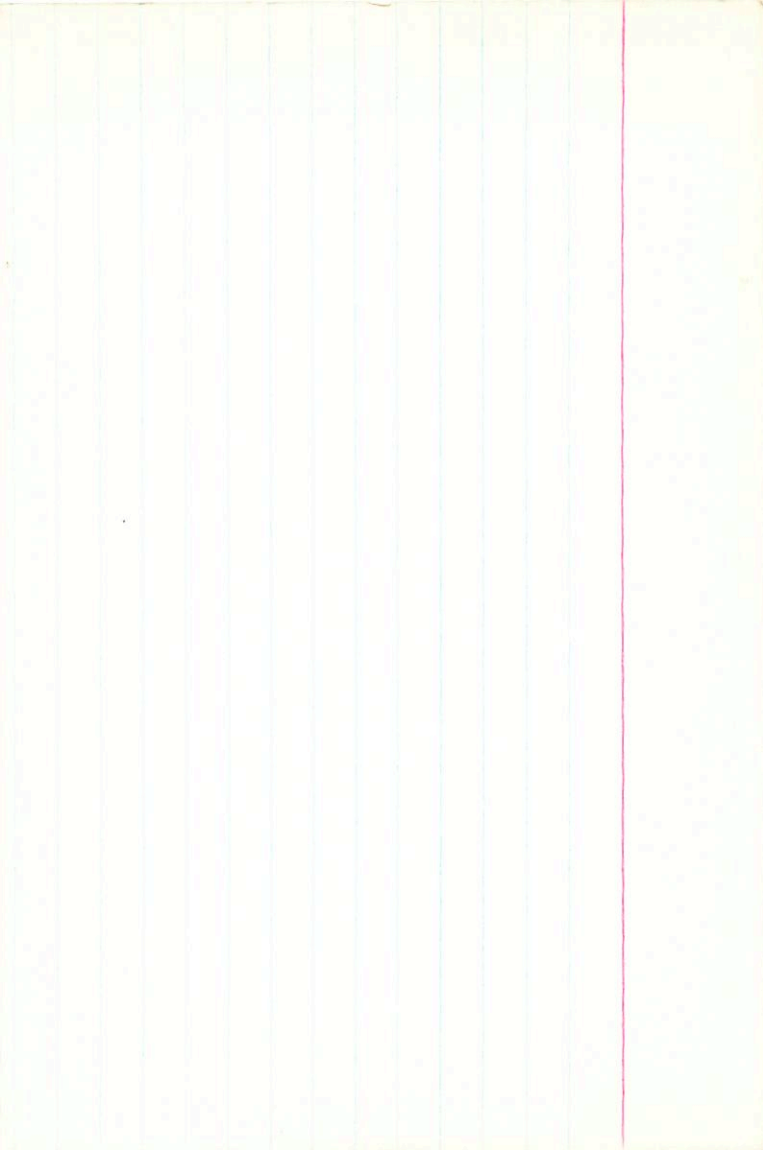
5.83 + 1.28 (~~2.58~~) C

N30 ±3.5

5.93 + 1.32 + 1.355 (2)

-0.12 -0.155

5.24 + 0.435 (2)



2377 6 25.9 -69 40 g 85 +9.16

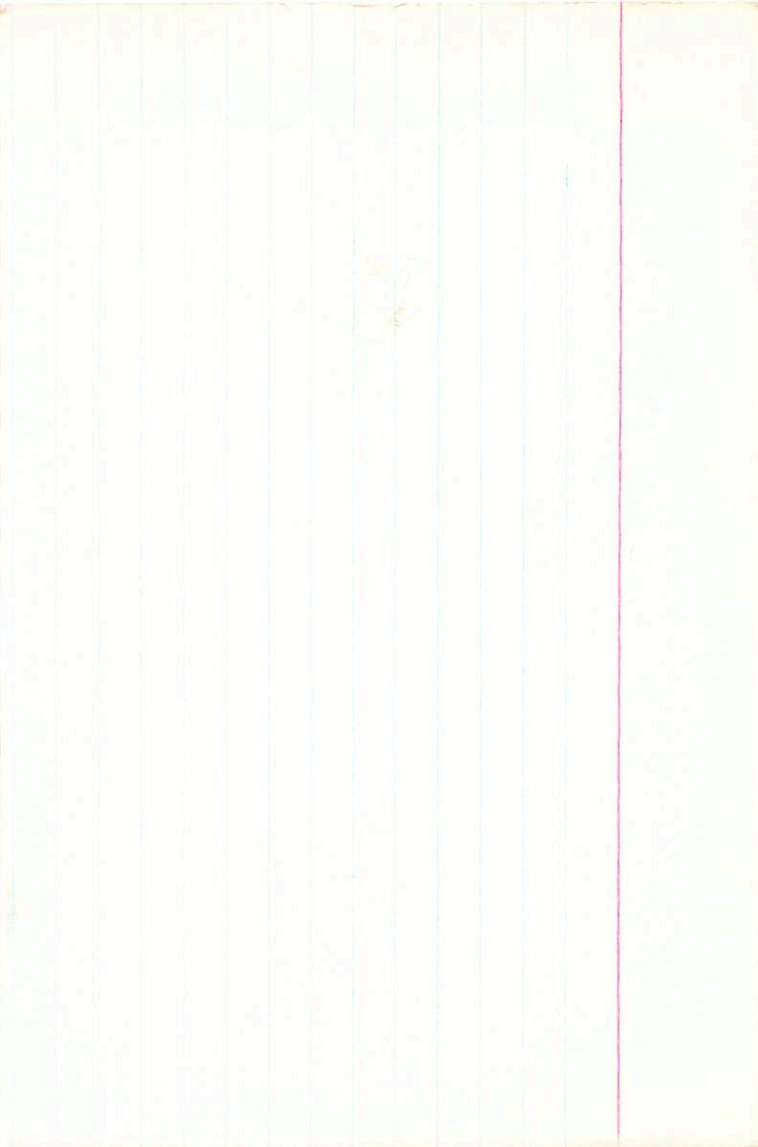
46116

5.37 + 0.97 + 0.68 C

4.98 + 0.36 (2)

N200 ± 3.0

-1021 + 1975



2378

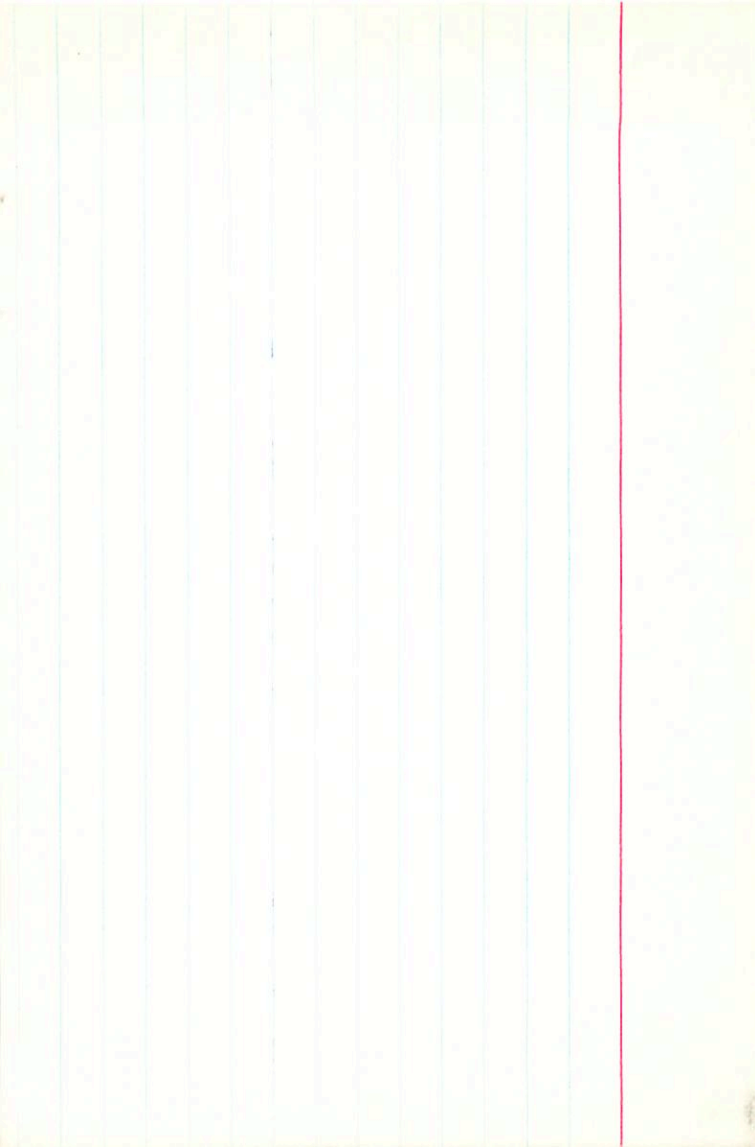
6 24.6 + 11 43 120 III -20.5 f

46178

6.04 + 1.095 + 0.56 ①

5.64 + 0.335 ②

OL



2079

6 29.1 -12 21 103 III +17.26

46194

5.15 + 1.27 (2.06) 6

5.18 + 1.25 + 1.35 (2)

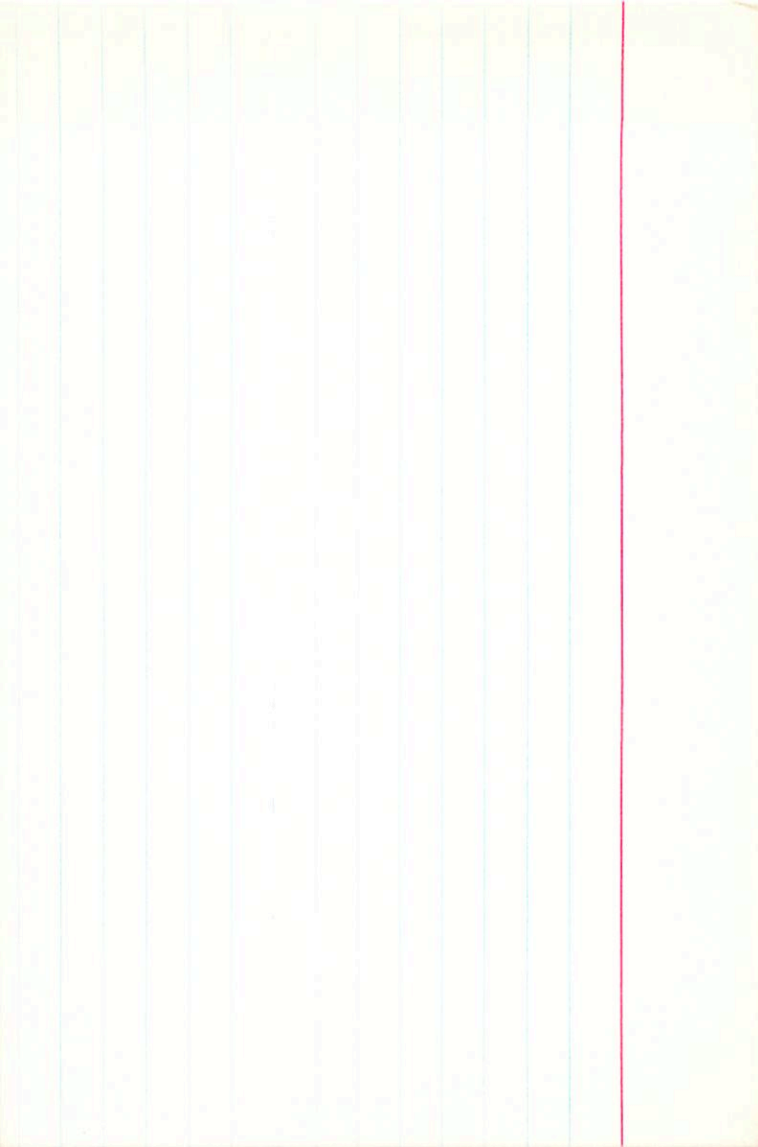
5.16 + 1.24 + 1.40 (1)

5.16 + 1.27 + 1.39 (3)

4.48 + 0.455 (2)

8/24 ±4.5

+0003 -0183



2351

6 24.6

-8 079102 - 2.5 Z

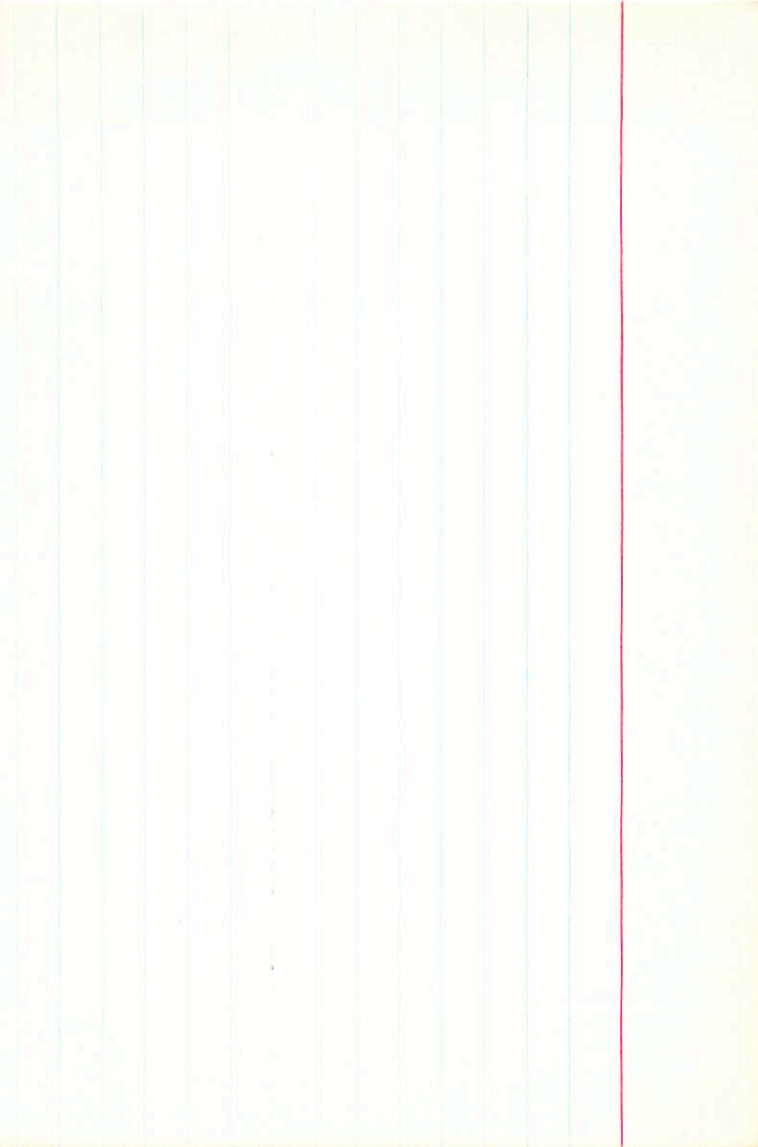
46229

5.42 + 1.37 + 1.51 C

5.04 ± 40

-0013 - 0.159

4.72 + 0.48 (2)



12mm

2392

6 29.7 +4 54 100 $\overline{111}$

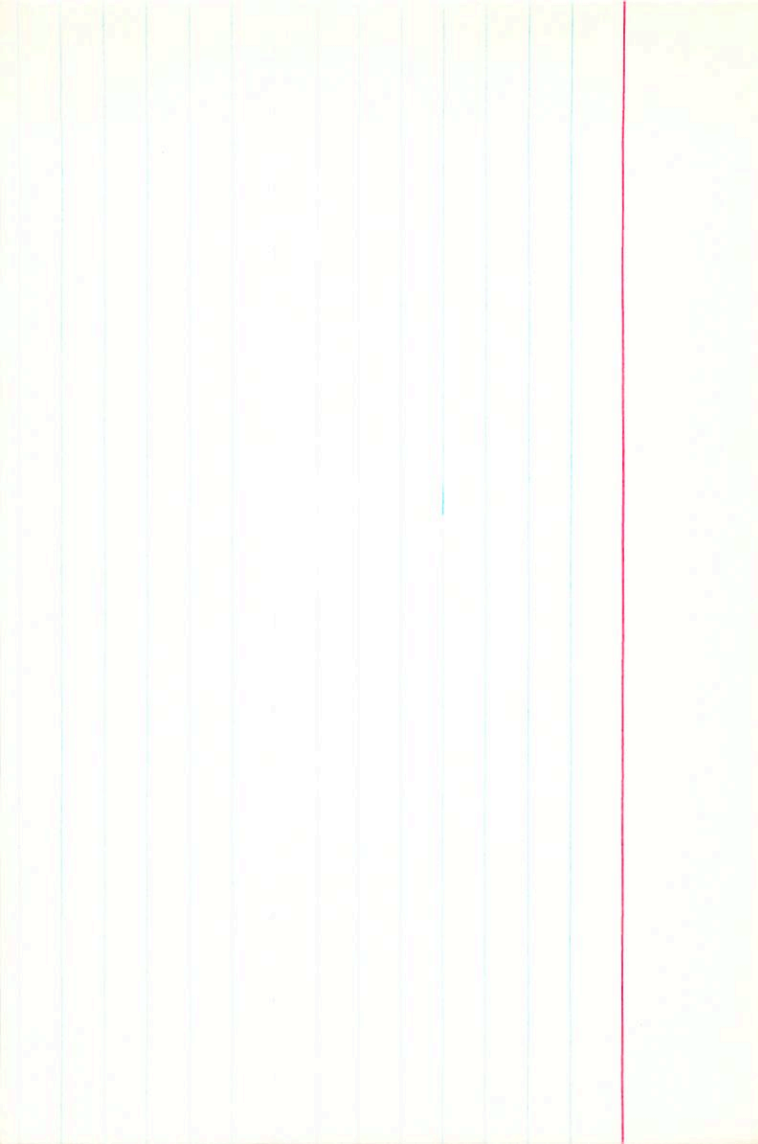
+20.78

46241

5.86 +0.49 +0.78 C

-0024 -0025

QL ± 2.5



2389

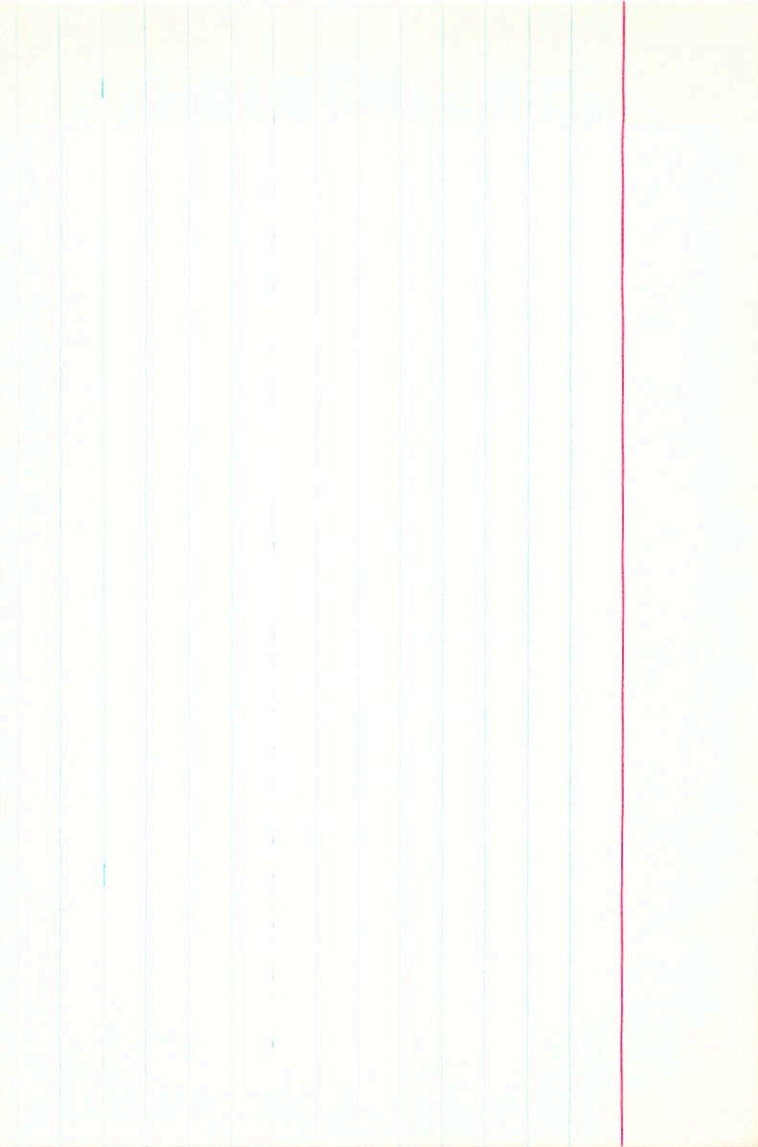
6 28.6 -56.49 989 +12.97

46355

$n = 30 \pm 4.0$

5.21 +1.09 -6

-0052 +023



2090

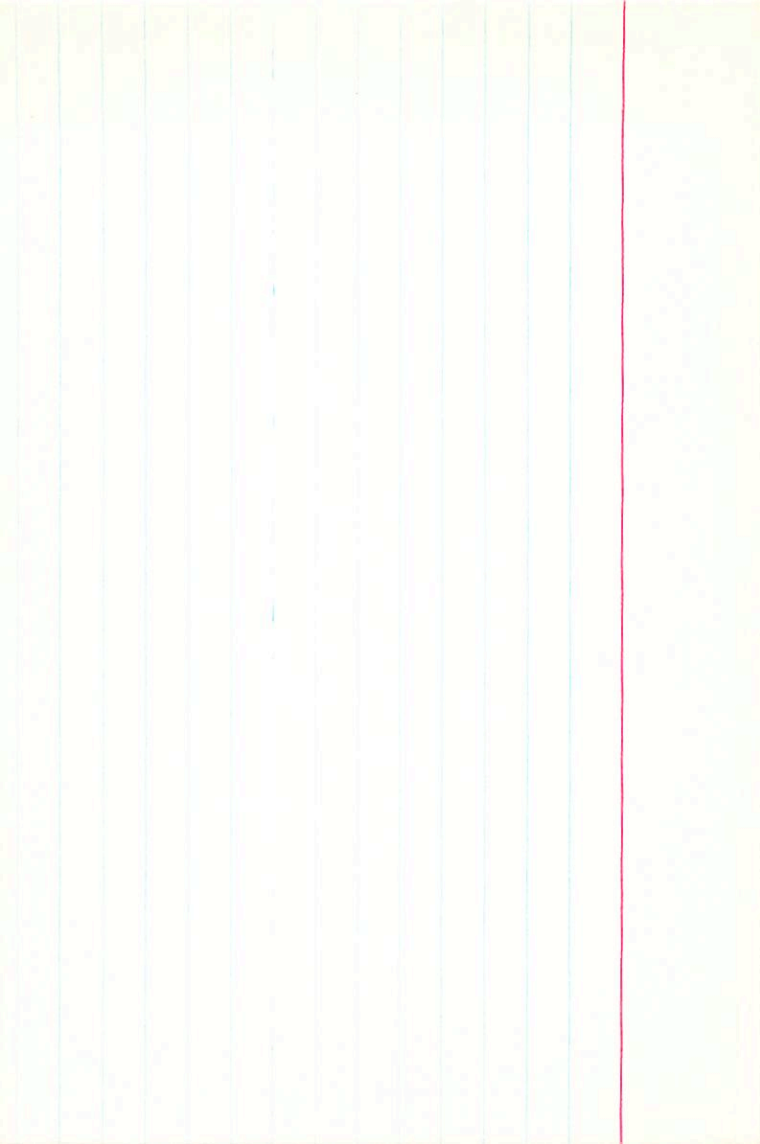
6. 29.4 - 40 53 102 —

1.78

$$6.19 + 1.40 (2.54) 0$$

$$6.21 + 1.44 + 1.60 (2)$$

$$5.45 + 0.505 (2)$$



2391

6 30.9

+14

12-9102

-12.17

46374

fA4 ± 3.0

-0011 -0900

5.56 + 110 + 0.97 ①

5.09 + 0.39 ②

2392

46407

6 304

-11 08 Kop

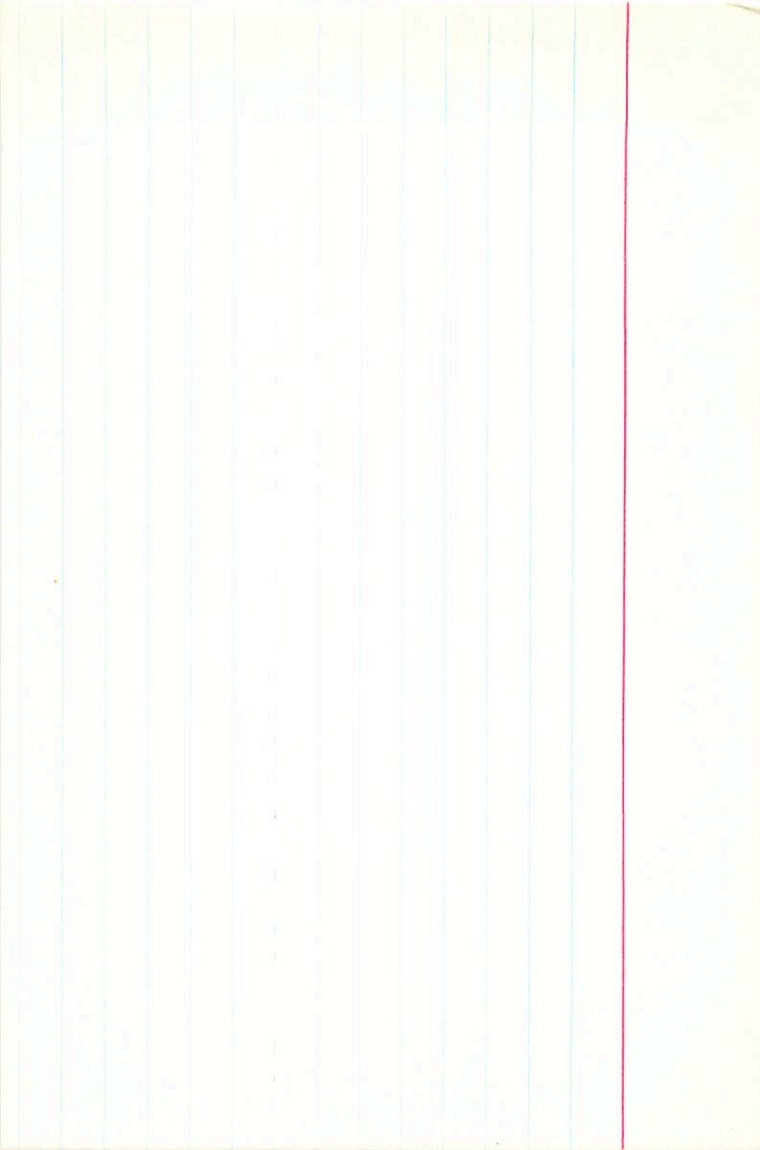
Ba II

-13.6

-0.02

$$6.29 + 1.12 + 0.75 \textcircled{3}$$

$$5.92 + 0.345 \textcircled{4}$$

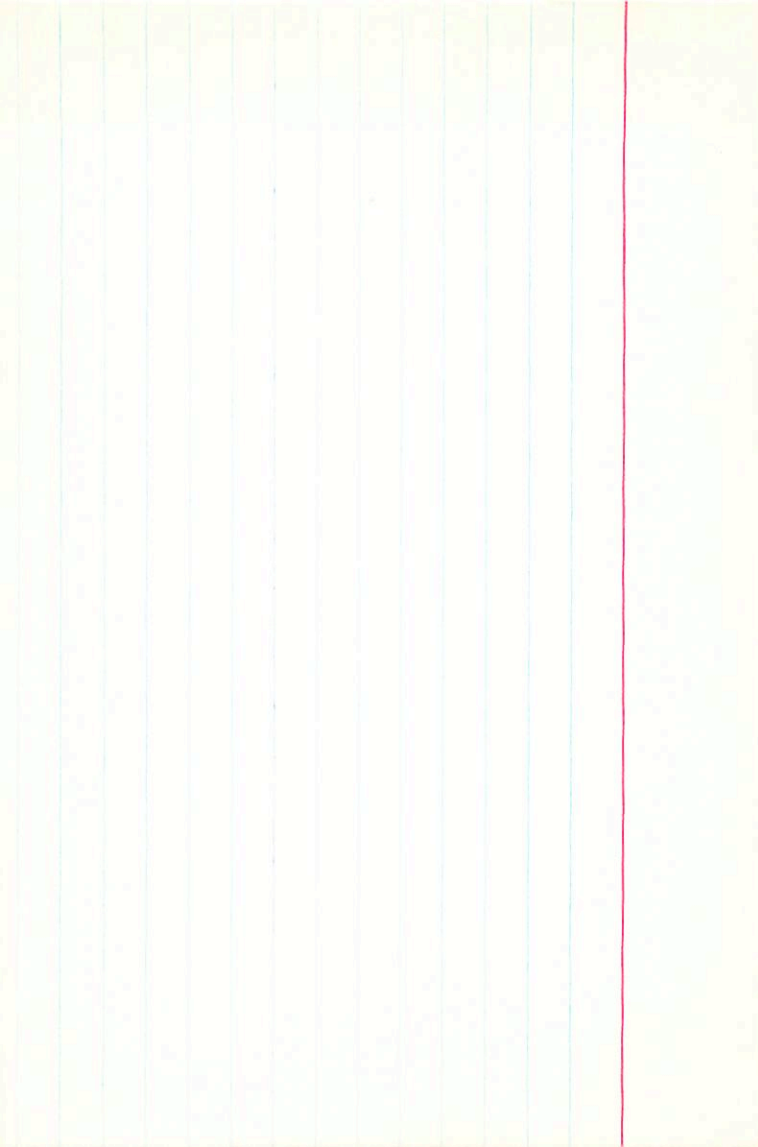


407 405

2393 6 249 -36 57 011 —

46431 6.3V +1.64 +1.91 (4)

5.14 +1.09 (2) 66



8 dyn

2394

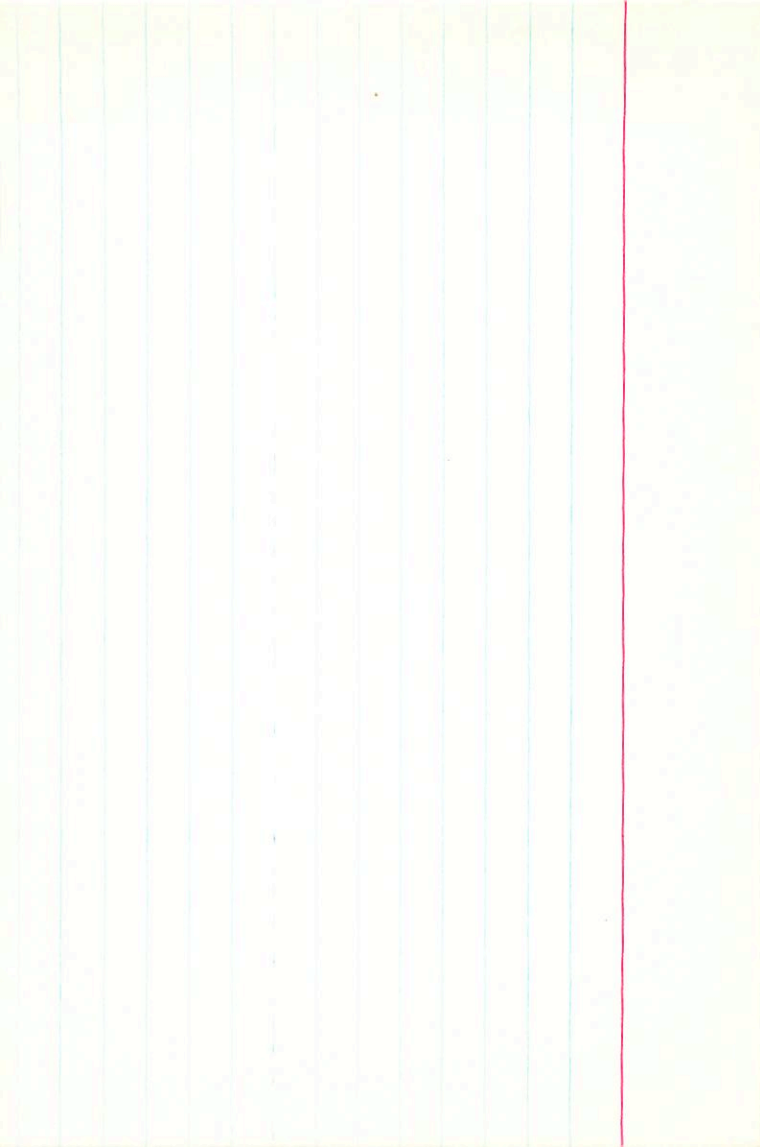
6 83.1 +6.1 32 29.87 -46.46

46450

5.94 + 0.89 + 0.52 A -02843 -2777

FK4

5.55 + 0.34 3A



2896

6 346

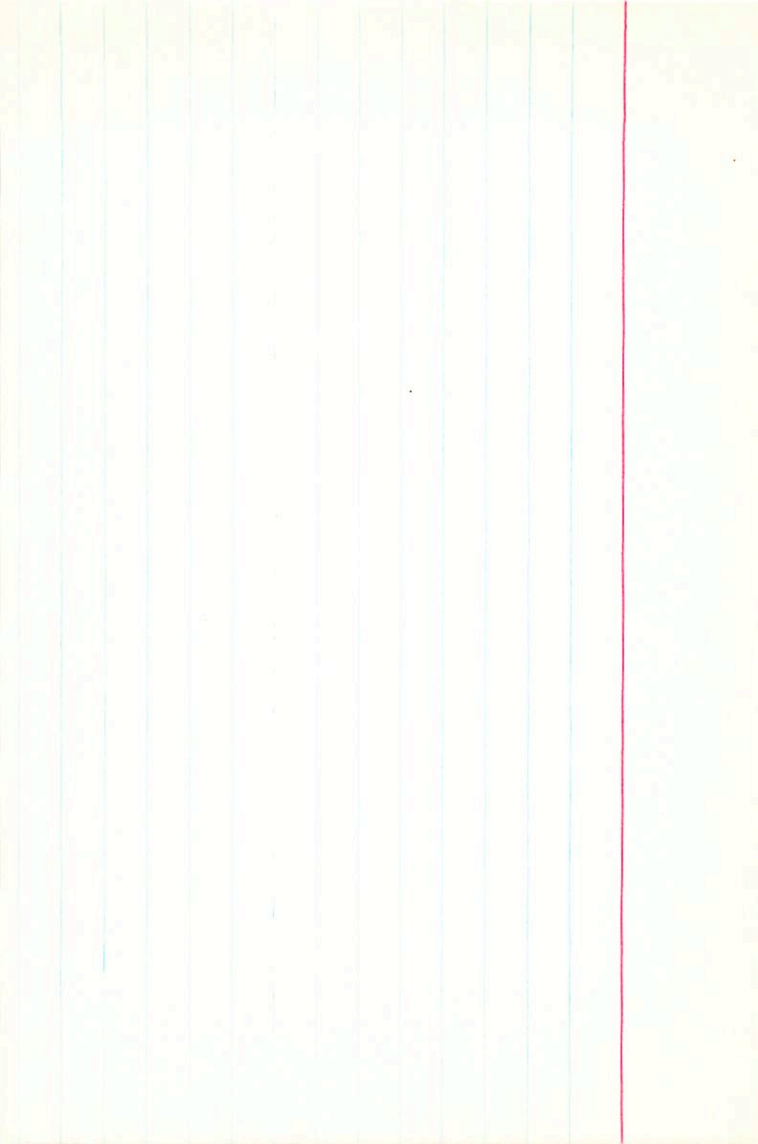
+71 48

100 $\sqrt{11}$

-23.24

46509

ac



2399

6 30.6 -37.39 968 +34.0a

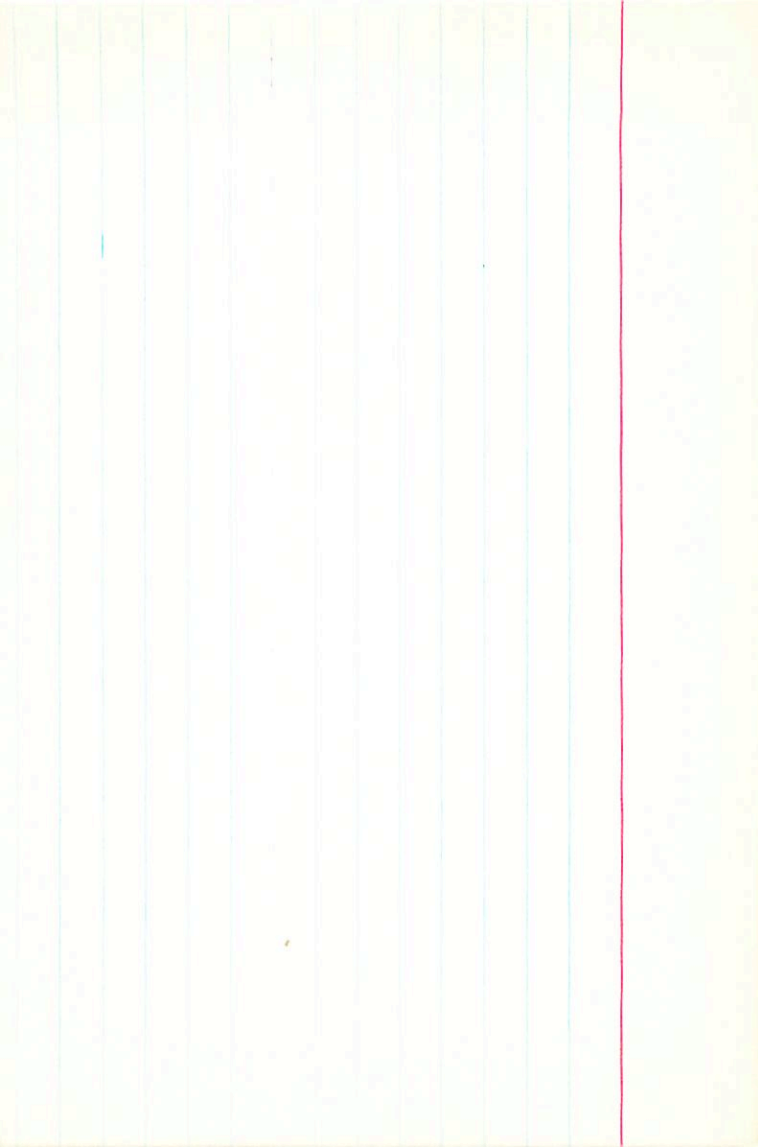
46569

5.25 +98 (2.04)0
5.24 +1.01 +0.65 ①

6c ±40
+0046 -0775

5th

4.86 +0.36 ②



27th Aug

2405

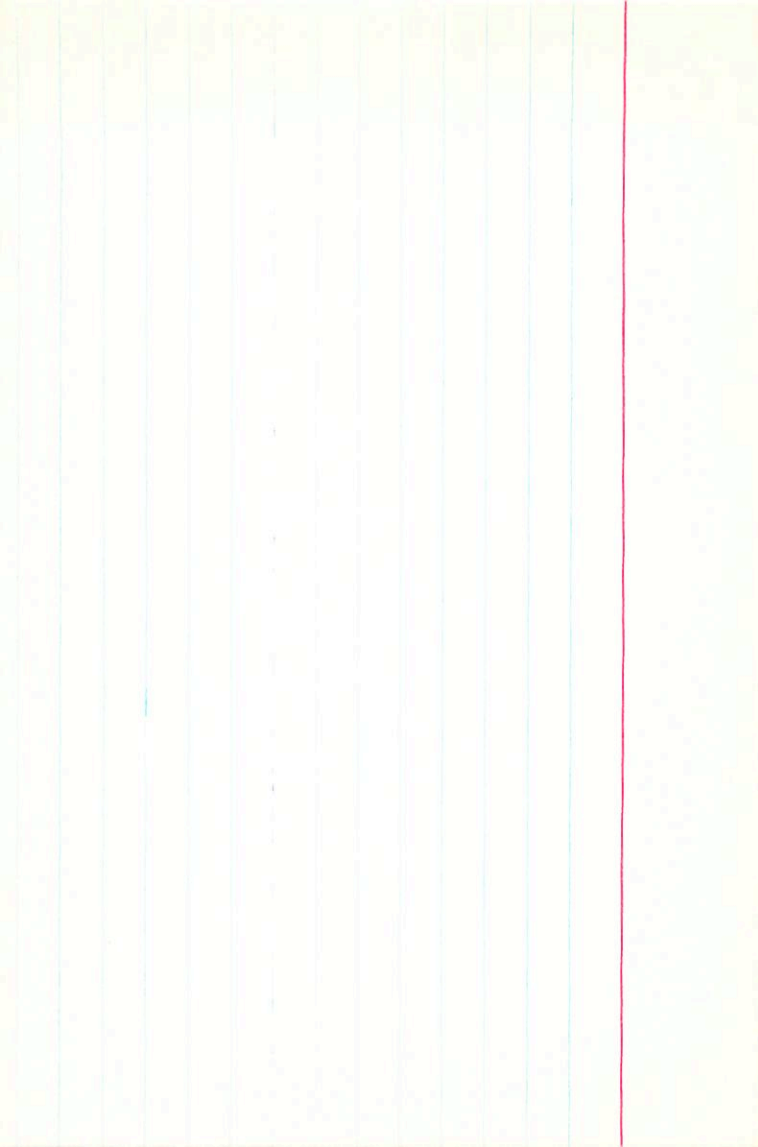
6 33.1

+38 30

C53

+12.07

46687



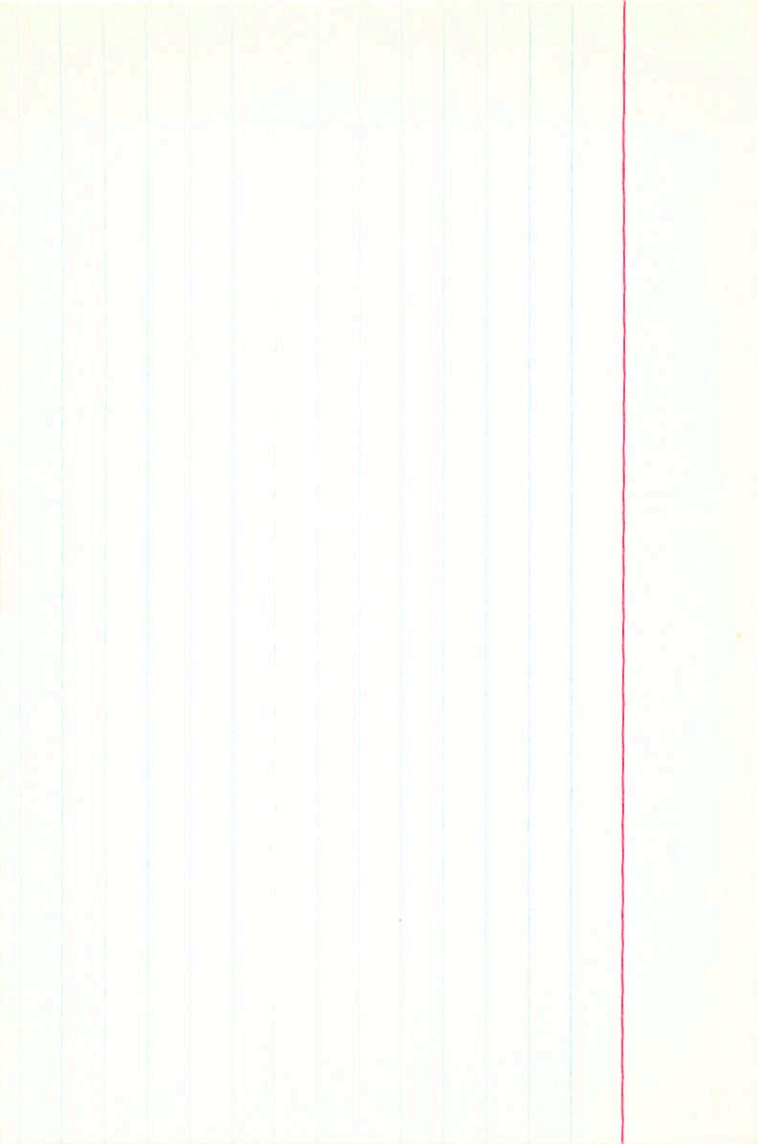
2406 6 32.5 +10 02 915 +38.66

46709

5.88 +1.51 +198 (3)

5.15 +0.54 (2)

66



4.08 7¹²

2411 4 32.1 -36 12 gmo +32.2 k

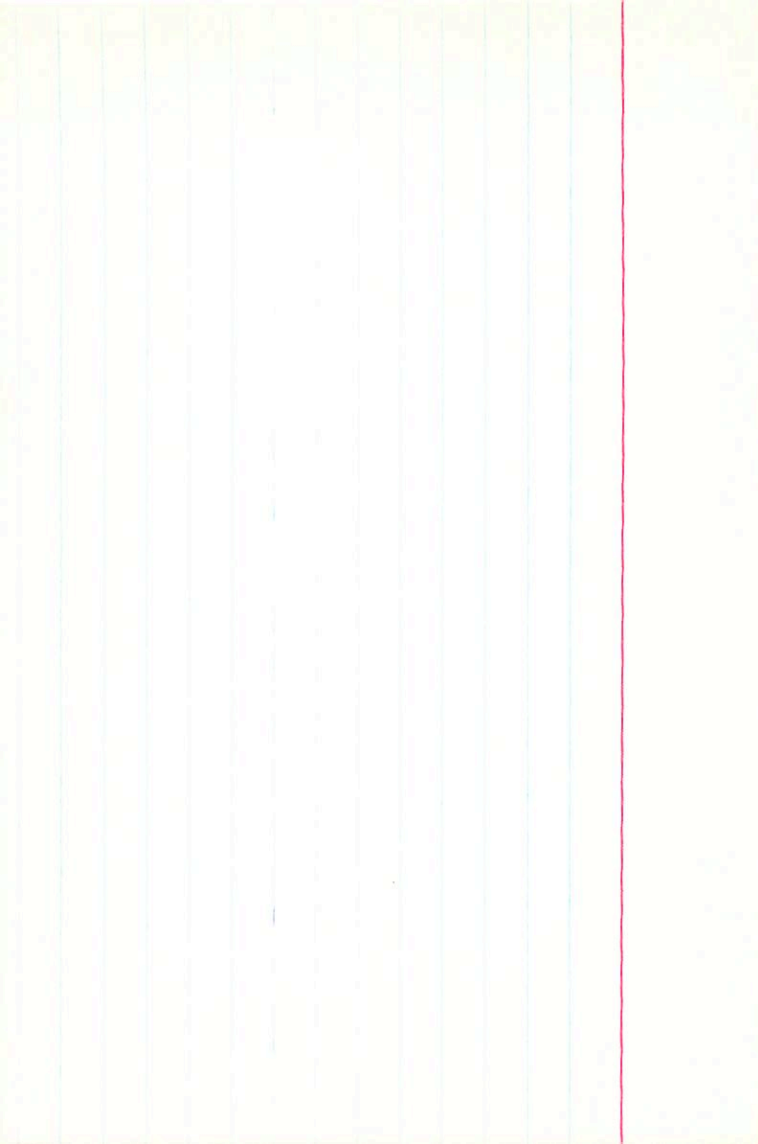
46815

5.41 + 1.44 - C

66 ± 3.5

-00155 + 0915

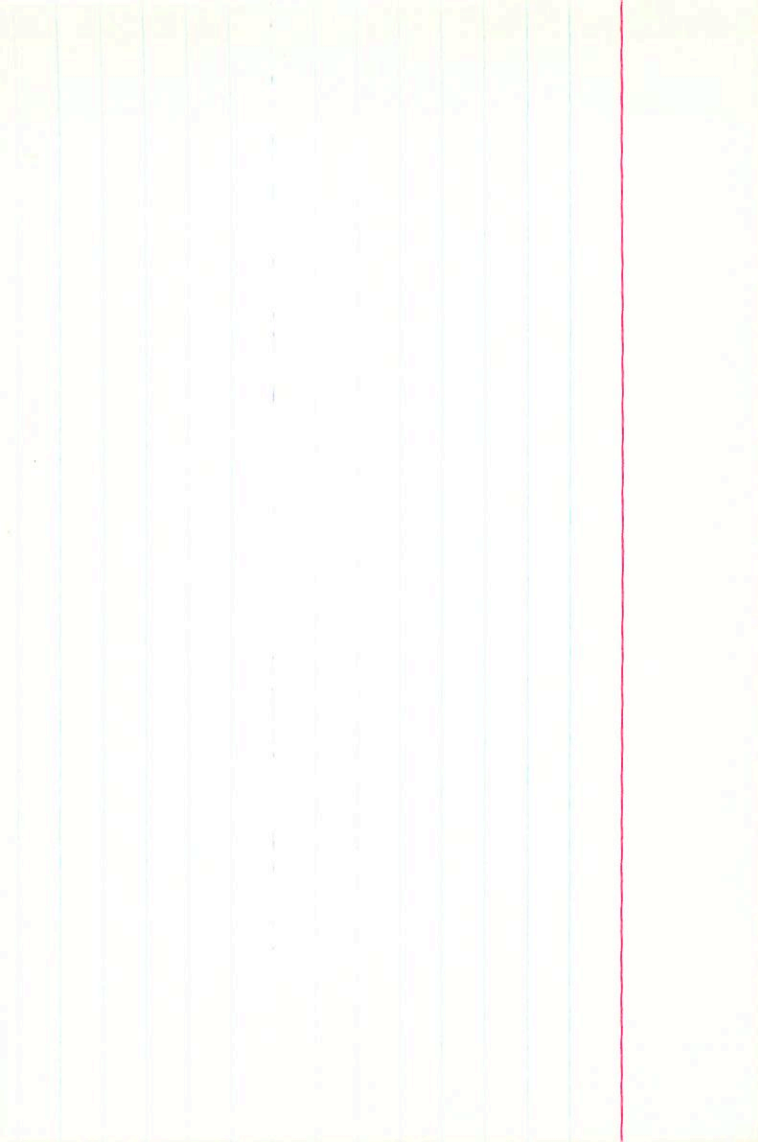
4.96 + 0.54 (2)



2476 6 32.3 -52 18 GS -

47001

6.17 + 1.09 (2.10) C GC



51 Ann

2414

6

35.2

+39

26

gms

+32.86

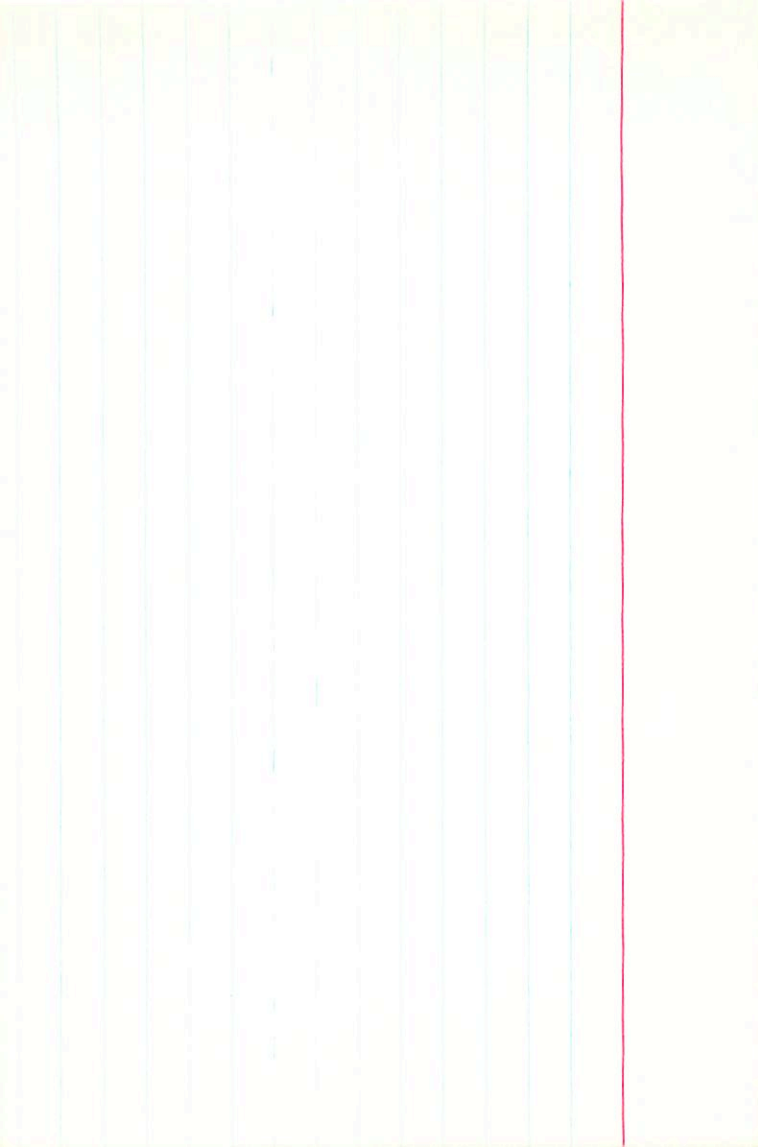
47070

5.68 +134 +1.56 ②

-00143

F114

-1107



+ F3.12-2

2423 6 34.2 -18 34 68711 +248 f

47184

1230 ± 2.0

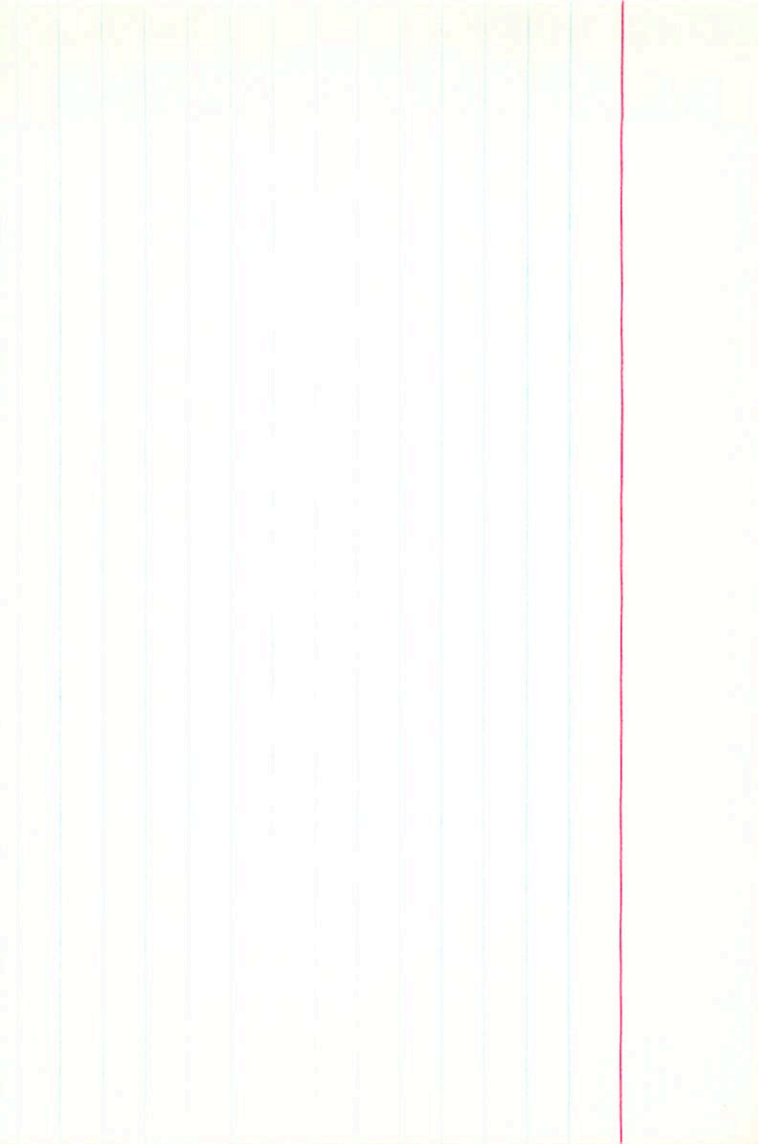
~~5.52 + 0.76 (1.84)~~

-00035 + 0.14

7.5 f6 14"

5.73 + 0.86 + 0.48 (3)

7.67 + 0.32 + 0.01 (3)



2426

6

348

+10

54

120

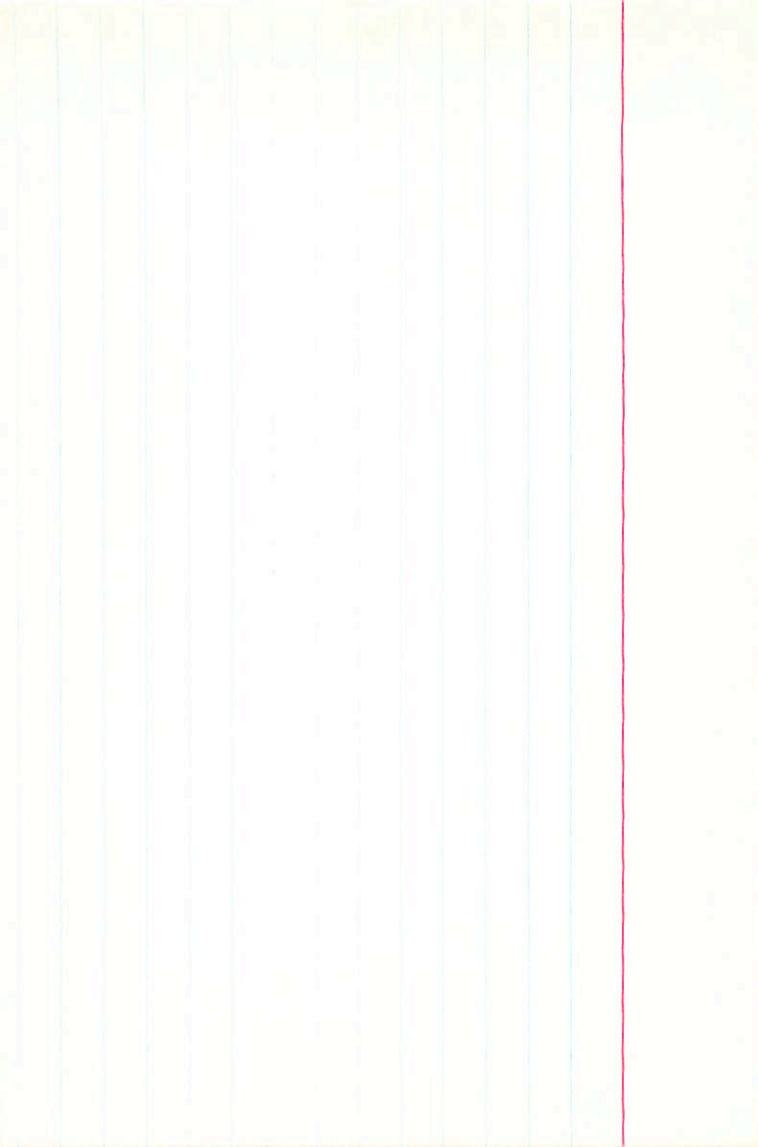
+1.56

47156

6.34 + 1.36 + 1.54 ①

5.71 + 0.495 ②

ac

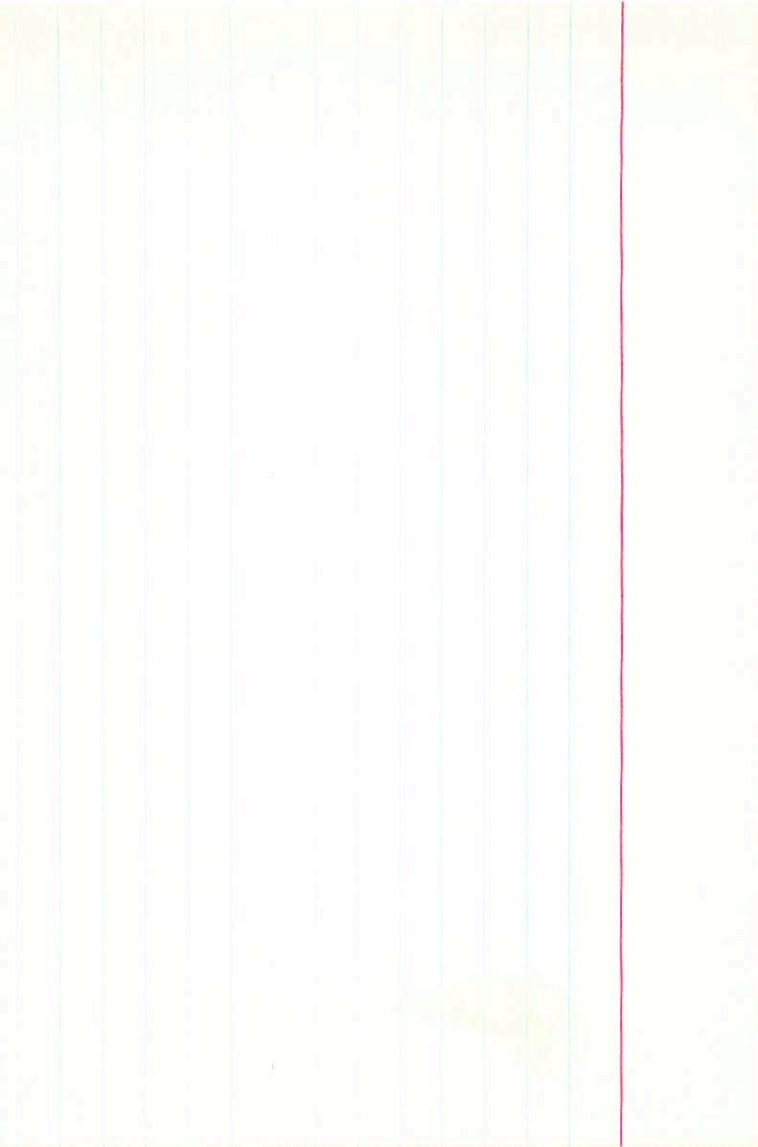


2429 6 345 -10 16 125 -

47182 5.56 + 1.56 (2.56) 6

5.95 + 1.62 + 1.42 (1)

5.00 + 0.64 (2)

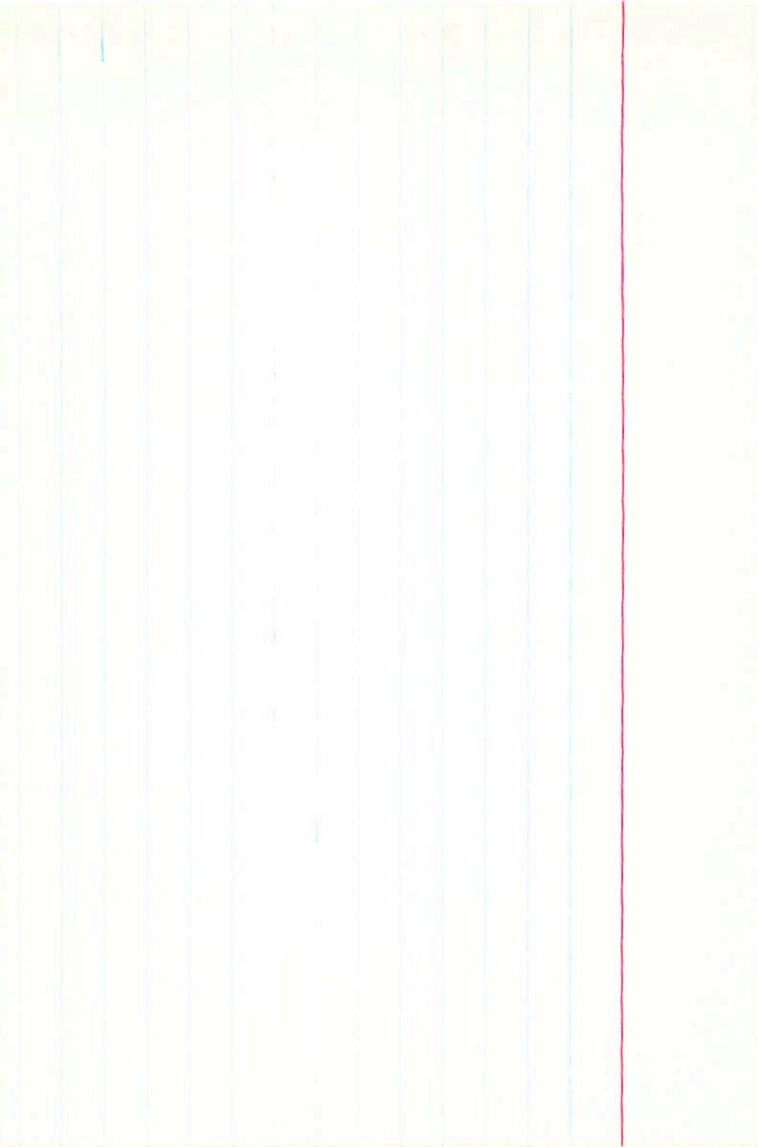


2430 6 351 +2 44 101 111 -2.6 f

47220

6.18 +1.08 +0.97 C

66

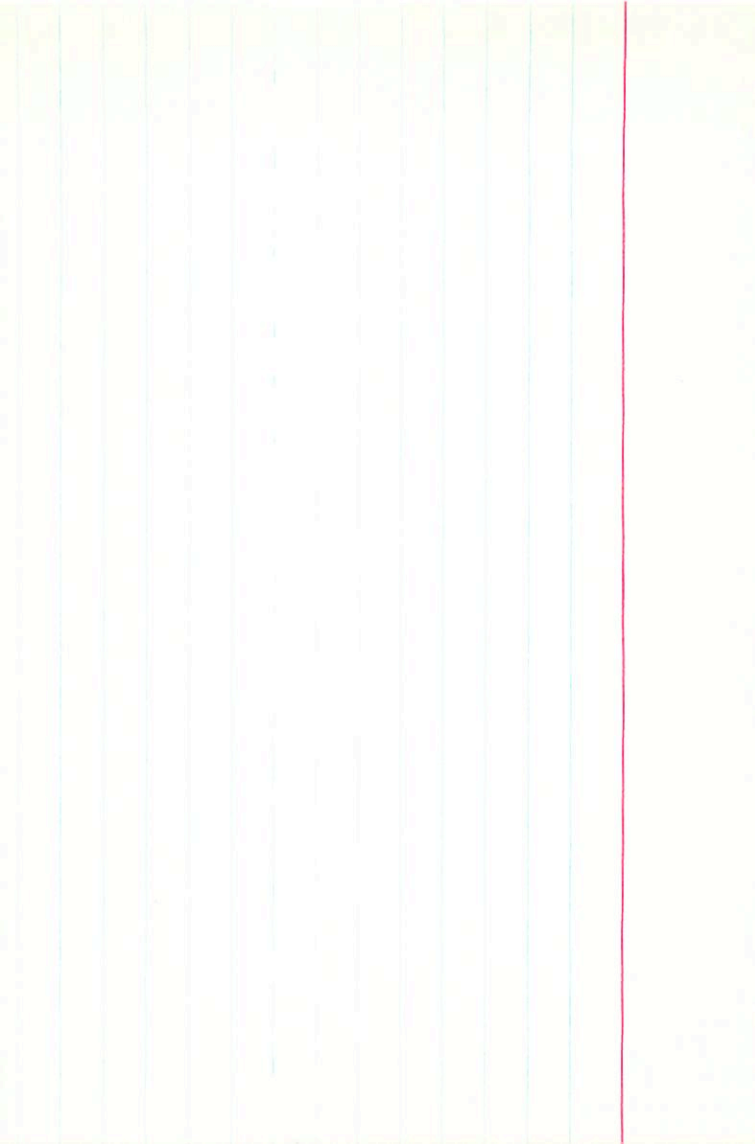


2436 6 361 +22 0Y 69 III -8.76

~~4737~~

47358

ac



2437

6

35.4

-12

56

140

—

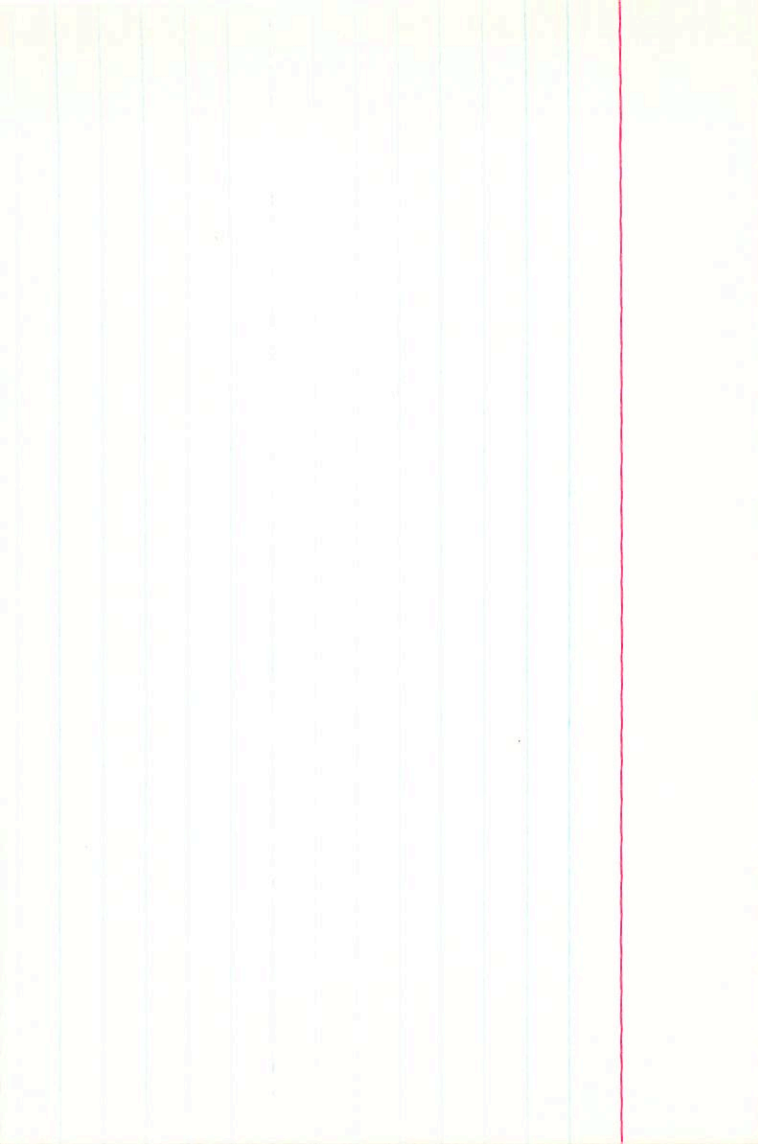
47366

6.11

+1.00

- C

BC



2440

6

35.8

-2

30

142

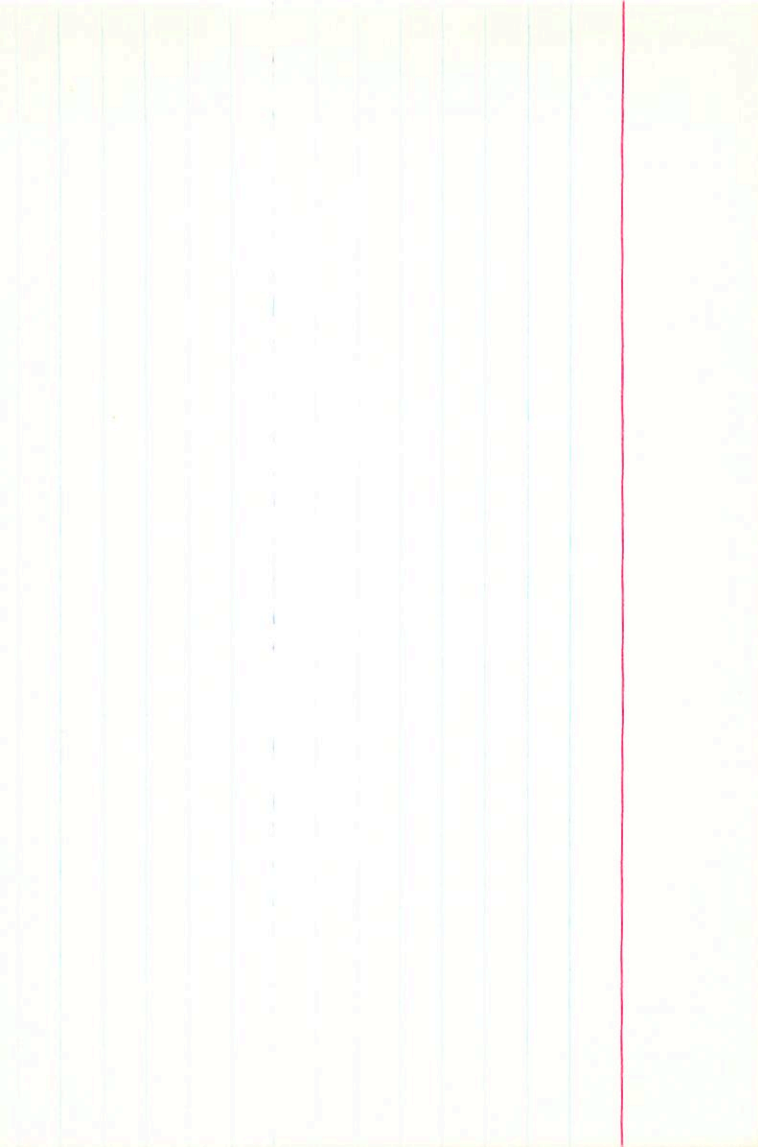
—

47420

$6.14 + 1.48 + 1.76 C$

60

$5.32 + 0.55 \textcircled{1}$



2444

6 35.3

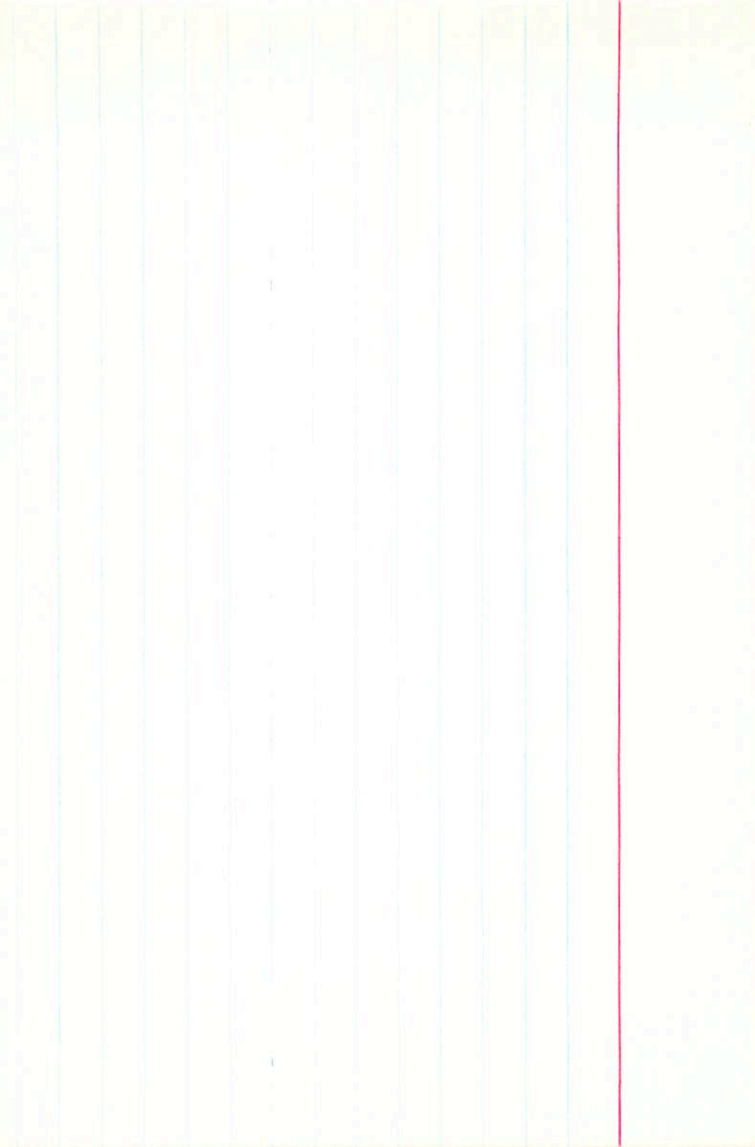
-88 06 65

—

47463

6.03 + 1.03

66



2447

6 360 -32 18 9 100 +78.8a

47536

5.23 +1.17 (2.22) C

GC ± 70

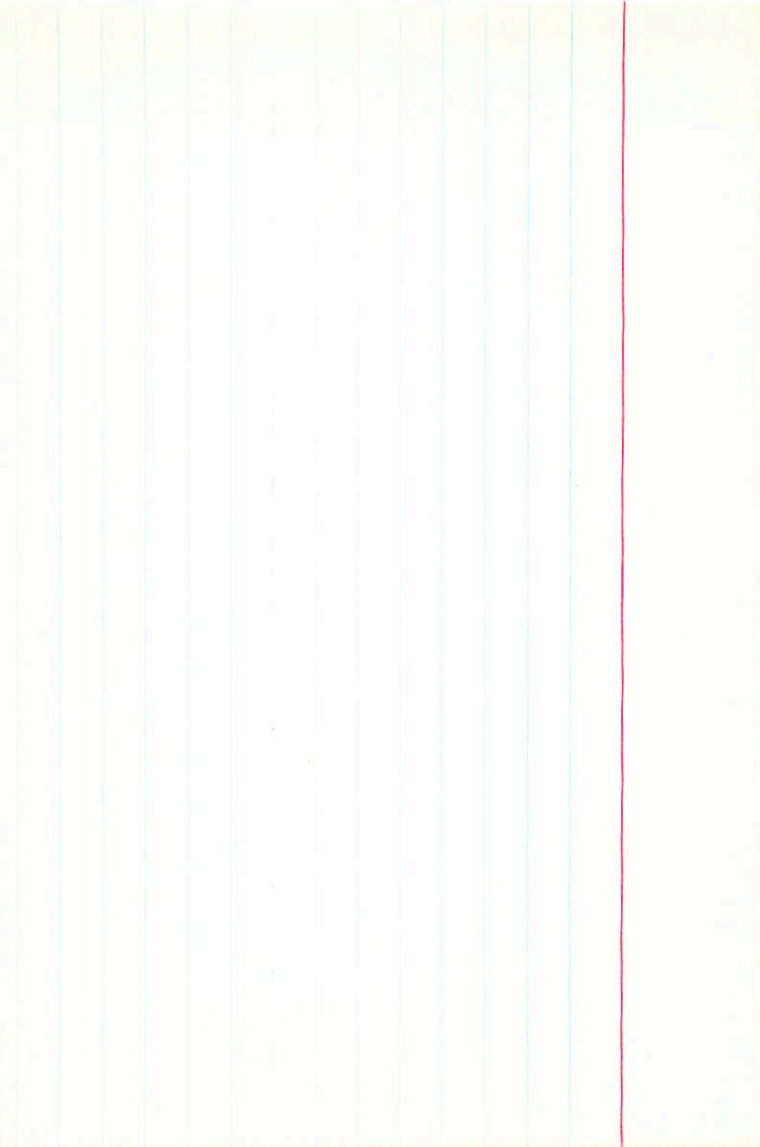
5.22 +1.20 +1.12 3BS

+00835 +6625

4.75 +0.47 ⊕

answer

4.58 428



2458

6 38.5 + 11 03 m1

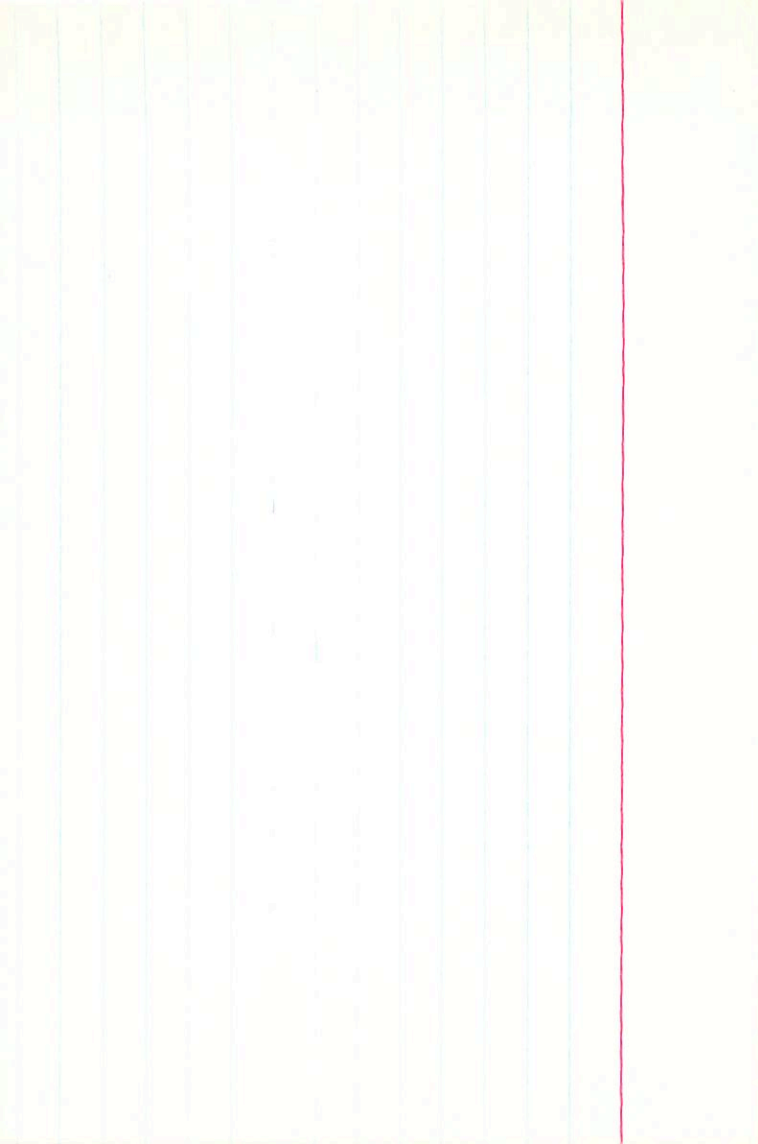
+ 15.96

47886

6.20 + 1.67 + 2.03 (4)

6.2

5.07 + 0.85 (2)



55 Ann

2459

6

39.4

+44

34

NS

$\sqrt{4}$

-23.14

47914

3.02

+1.48

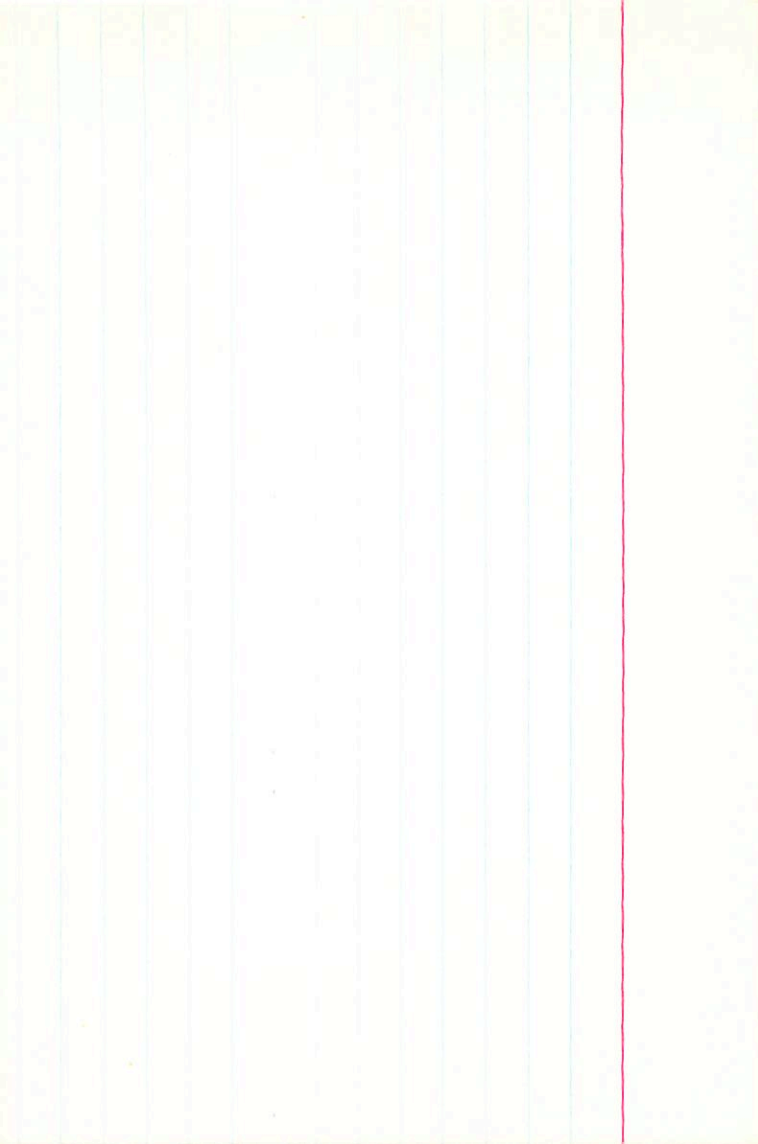
+1.83

2P

-042

-0311

SA4 = 2.0



5.20 488

2460

6 378 -30 25 100 —

47946

5.70 + 1.14 - C

02

5.28 + 0.40 (2)

